

STUDIES ON OPTIMUM SIZE AND SHAPE OF PLOTS AND BLOCKS FOR  
FIELD TRIALS ON RICE AND JUTE CROPS IN TERAJ AGROCLIMATIC  
ZONE OF NORTH BENGAL AND ON THE EFFICIENT MODELLING OF  
DATA THROUGH CONVENTIONAL AND SPATIAL METHODOLOGY

OFFICE OF THE  
DEAN POST GRADUATE  
STUDIES  
RECEIVED 23-08-2004.

*A Thesis*

*submitted to the*

*Bidhan Chandra Krishi Viswavidyalaya*

*in partial fulfillment of the requirements for the award of the Degree of*

*Doctor of Philosophy*

*in*

**AGRICULTURAL STATISTICS**

By

**Satyananda Basak**



DEPARTMENT OF AGRICULTURAL STATISTICS  
FACULTY OF AGRICULTURE  
BIDHAN CHANDRA KRISHI VISWAVIDYALAYA  
MOHONPUR, NADIA, WEST BENGAL  
2004

**Dedicated**

**to**

**my beloved little daughter**

**Sailee**

**and my beloved wife**

**Babita**



## CERTIFICATE OF APPROVAL

---

---

We, the undersigned, having been satisfied with the performance of Shri Satyananda Basak, in the Viva-Voce Examination, conducted today, the.....16/02/05....., 2004, recommended that the thesis be accepted for the award of the Degree of Doctor of Philosophy in Agricultural Statistics of Bidhan Chandra Krishi Viswavidyalaya.

| Name                          | Board of Research Studies<br>Examiners | Signature   |
|-------------------------------|--|---|
| 1. Prof. S. Pal               | Chairman, Advisory Committee           | .....    |
| 2. Dr.                        | External Examiner                      | .....    |
| 3. Dr. A. K. Pal              | Member, Advisory Committee             | .....  |
| 4. Dr. N. R. Majumdar         | Member, Advisory Committee             | .....  |
| 5. Dr. A. Majumdar            | Member, Advisory Committee             | .....   |
| 6. Dr. S.K.<br>Munishopadhyay | Departmental<br>Nominee                | .....  |

# *Bidhan Chandra Krishi Viswavidyalaya*

FACULTY OF AGRICULTURE  
DEPARTMENT OF AGRICULTURAL STATISTICS

Mohanpur, Nadia, West Bengal; Pin – 741252.

Phone (O): +91-3473-278605



## **Prof. Satyabrata Pal**

Ph.D., F.I.F.I., F.A.Sc.T., F.I.A.H., M. N. A. Sc.

Dean  
Post-Graduate Studies  
and Professor in Agricultural Statistics

Residence: 101/B Bakul Bagan Road  
Kolkata – 700025

Phone (Residence): 033-2485-2160  
033-2475-9048

E-mail: [satbrpal@vsnl.net](mailto:satbrpal@vsnl.net)

E-mail: [satyabratpal@hotmail.com](mailto:satyabratpal@hotmail.com)

*Ref. No.: Ag. Stat /*

*Date: ..23.../ 08 / 2004.*

### CERTIFICATE

This is to certify that the work, recorded in the thesis, entitled “Studies on optimum size and shape of plots and blocks for field trials on rice and jute crops in terai agroclimatic zone of North Bengal and on the efficient modeling of data through conventional and spatial methodology” submitted by Shri Satyananda Basak for the award of the degree of Doctor of Philosophy in Agricultural Statistics of the Bidhan Chandra Krishi Viswavidyalaya, is a record of faithful and bonafide research work carried out by Shri Basak under my direct supervision and guidance. The results of the investigation, reported in this thesis, have not so far been submitted for any other Degree or Diploma. The assistance and help received during the course of investigation have been duly acknowledged.

  
(SATYABRATA PAL)

Chairman, 23/08/04

Advisory Committee

## ACKNOWLEDGEMENT

---

I express my deep and profound sense of gratitude and indebtedness to Dr. S. Pal, Professor of the Department of Agricultural Statistics, Bidhan Chandra Krishi Viswavidyalaya, Mohonpur for his inspiring guidance, constant supervision, constructive criticisms, valuable suggestions, sustained interest and steady encouragement through the course of this research work. Words fall short to express my gratitude for his active involvement in spite of his heavy engagement as Dean, Post Graduate Studies.

I am grateful to Dr. A. K. Das, Head of the Department of Agricultural Statistics, Bidhan Chandra Krishi Viswavidyalaya, Mohonpur for providing me administrative support during my research work. I am grateful to the teachers Dr. S. R. Pal, Dr. R. M. Panda, Dr. A. Majumdar, Dr. S. Mukhopadhyaya, Dr. P. K. Sahu, Dr. M. K. Sanyal, Dr. (Mrs.) Banjul Bhattacharya of the Department of Agricultural Statistics, Bidhan Chandra Krishi Viswavidyalaya, for their encouragement in carrying out my research work.

This is also an opportunity to express my thanks due to all the non-teaching staff members of the Department for the love and affection extended by them during the tenure of my research.

I would confess that the hatching of the idea of conducting uniformity trial for the Terai Agro-climatic Region of North Bengal was originally due to Dr. A. K. Pal, Dr. N. R. Majumdar and Dr. Ananta Deb Das of the Uttar Banga Krishi Viswavidyalaya, Pundibari, Coochbehar. My acknowledgement is due to each one of them.

I acknowledge the help extended by my University, Uttar Banga Krishi Viswavidyalaya for granting me study leave to achieve the higher degree leading to Ph.D.

At last but not the least, it is my good fortune that my beloved wife, Babita, my little daughter, Sailee have taken much pain during my long absence and above all, shown their patience and in fact, bereft of their perseverance it could be too difficult to complete my research work. I don't find much suitable words of appreciation to express my indebtedness to them.

**Place:** Mohonpur

**Date:** 23/08/2004

*Satyananda Basak*  
( Satyananda Basak )

## INDEX

| CHAPTER<br>NUMBER | CHAPTERS   | PAGE    |
|-------------------|--|---------|
| <b>1.</b>         | <b>Introduction</b>  | 1-9     |
| 1.1               | Historical background  |         |
| 1.2               | Scope of the work  |         |
| 1.3               | Overview of the work   |         |
| <b>2.</b>         | <b>Smith's model and its developments</b>                        | 10-43   |
| 2.1               | Optimum plot size for isotropic field                            |         |
| 2.2               | Heterogeneity for non-isotropic field                            |         |
| 2.3               | Maximum curvature  |         |
| 2.4               | Block size   |         |
| <b>3.</b>         | <b>Two way spatial correlation study</b>                         | 44-65   |
| 3.1               | Introduction   |         |
| 3.2               | Material and method  |         |
| 3.3               | Optimum plot size  |         |
| 3.4               | Results and discussion   |         |
| <b>4.</b>         | <b>Modeling spatial variability</b>                              | 66-90   |
| 4.1               | Introduction   |         |
| 4.2               | Spatial model  |         |
| 4.3               | Spatial modeling of uniformity data                              |         |
| 4.4               | Results of variogram model fitting                               |         |
| 4.5               | Relating variogram parameters to plot and block size and shape   |         |
| <b>5.</b>         | <b>A new method for determination of plot size</b>               | 91-100  |
| 5.1               | Introduction   |         |
| 5.2               | Material and method  |         |
| 5.3               | Results  |         |
| <b>6.</b>         | <b>A case study of Mercer &amp; Hall wheat grain yield data.</b> | 101-117 |
| <b>7.</b>         | <b>Summary and conclusion</b>                                    | 118-119 |
|                   | <b>Bibliography</b>  | I-IV    |
|                   | <b>Appendix</b>  | IV-XV   |

## *Chapter 1*

### INTRODUCTION

#### 1.1 HISTORICAL BACKGROUND:

One of the chief difficulties in obtaining reliable results in field trials is the natural variability of the material with which we are dealing. Crops are living organisms with inherent tendencies to vary even though it was possible to make their environmental conditions identical. Further, variation is induced as a result of many environmental factors which are beyond the control and recognition of the experimenter. Lack of uniformity in both the physical and chemical characteristics of the soil is one of the foremost factors causing variation in productivity of plants. Apparently, uniform surface soils may be underlain with a heterogeneous subsoil. Differences also occur which are not evident on a careful inspection of both the soil and the crops, but which are easily measured by weighing the yields. In other words, the weighing machine is more sensitive than the eye and reveals differences that mere inspection can not detect. The past treatment of the soil brings in variables the significance of which may not be comprehended at the time a field trial is begun. The persistent effects left by the application of manure in some field plots can show how large a part is played by the past history of the field. Unequal prevalence of diseases and insects may bring about further errors in the results. Besides the above sources of variation and possibly outweighing them at times is the effect of season. No season is entirely normal.

Holtmark and Larsen (1906) are among the first to call attention to the errors of field trials. They recognize the inevitable variation of field results, and show how it may be estimated by the use of the standard deviation and the coefficient of variability. They also show that the coefficient of variability decreases as the plots are enlarged, but not proportionally to the size of the plot. The limitations of field experiments are discussed by Carleton (1909), who call the attention of experimenters to the various uses of control plots, and to the general precautions necessary to obtain reliable results. Hall (1909), Mercer and Hall (1911) and Hall and Russel (1911) record extensive studies of the soil variations in experimental grounds and the influence of size and repetition of plots upon accuracy. The above work was done largely with the yields of wheat, mangel and hay crops. The conclusions from the above work are that the error in field trials diminishes as the size of the plot increases, but that the reduction is small when the plot is enlarged to a size greater than one-fortieth of an acre. The error may be further diminished

by increasing the number of plots similarly treated and scattering them about the area under experiment; but there is not much to be gained by increasing the number of plots above five. Wood and Stratton (1910) sound notes of caution concerning the interpretation of experimental results. Frequency distribution is discussed from the point of view of its bearing on the reliability of averaging results. The applications of the probable-error methods to questions of sampling for analysis, to field experiments, and to feeding experiments are illustrated. The probable-error of field experiments is investigated by two independent methods and found to be about five percent of the mean yield. It is shown that more accurate results may be obtained by employing large numbers of small scattered plots than by using one large plot. The estimation of errors in field plot tests has been given considerable attention by Lyon (1912) and coworkers. It is shown that it is not possible to establish a schedule of relative yields for a series of plots, even after several years' comparison. Also, there seems to be little gain by using plots larger than one-fiftieth of an acre in size when the comparative yield of the crops is made the criterion. An area of one-twenty-fifth of an acre of land distributed in four widely separated plots, devoted to any one test, secures a much greater degree of accuracy than the same area of land in one body. The probable-error is reduced from 4.5 to 2.0 percent by such distribution. Pickering (1911), from studies on apples and pears, conclude that experimental plots should include 6 to 12 fruit trees. Precautionary advice is also given concerning the measurement of results by crop production, foliage and tree characteristics. In comparing the results on the treated plots with the controls, instead of taking the average of the controls, he prefers to plot these results out and to draw a smoothed curve through them, and then to compare the results of the experimental plots with readings taken at corresponding points of this curve. Wood (1911) shows how the degree of reliance can be determined for any set of experimental results by the use of the probable error. The use of this constant is demonstrated in interpreting laboratory analysis, as well as both plot and feeding experiments. Working with mangel yields, the author calculates the number and size of plots required to attain any desired precision, and working with the probable error of live weight increase of sheep, tables are given showing the number of animals required in an experiment to attain various degrees of reliability. Several papers by Harris (1912, 1913a, 1913b, and 1915) have drawn our attention to several phases of the experimental error in field tests. A measure of the variability of the soil productivity is obtained by determining the correlation between the yields of ultimate small plots and the yields of various groups of adjacent plots. The more nearly

this correlation approaches zero, the more homogeneous the soil. This method of measurement does not seem to provide as definite a means of obtaining a corrective term as the use of the coefficient of variability and the probable error as used by Wood, Wood and Straton, Mercer and Hall, etc., or the contingency method of correction as used by Surface and Pearl (1916). Montgomery (1912) has also discussed the comparative variability resulting from increasing the size of the plot and from distributing small ultimate plots over the area. The later method is found to be more accurate. In a subsequent paper (1913) the relative reliability of yields of wheat planted in rows and in square blocks is discussed. An exhaustive and discriminating discussion of the nature and magnitude of variability in the results of feeding experiments has been given by Mitchell and Grindley (1913). Much of their discussion is equally applicable to experimentation with plants. Olmstead (1914) applies the method of least squares in calculating the reliability of the yields of the mangel and wheat crop records of Mercer and Hall, the potato records of Lyon and the wheat yields of Montgomery. The author concludes that the estimation of the probable error of a large number of small duplicate plots well distributed in the area devoted to a field experiment indicates that the precision of agricultural experiments can be increased by replicating the experiment on small plots. Coombs and Grantham (1916) have studied the variation in the yields of rice and coconuts for one year, and discussed the range and interpretation of the probable error. They showed that the yields from any two single plots could only be significant when the difference amounted to 22.8 percent of the mean. They also introduced calculations to show the odds that any increase is a real increase and not a probable error. The use of controls and repeated plantings in varietals tests was studied by Pritchard (1916) in breeding work with sugar beets. His studies lead to the conclusion that the practice of dispensing with control rows and using the mean of all progeny rows as a standard of comparison appears to be less accurate than the employment of frequent controls. However, the employment of every alternate row as a control was not sufficient to offset the variability in yield arising from irregularities of soil. Stockberger (1916) discusses the value of a number of the common methods for determining the normal yield of treated plots based upon the yields of hops. Normal yields for various plots varied widely according to the method of computation, the values in some cases differing from the actual yield by as much as 40 percent. Repetition brought about a very marked reduction in variability, although with only five repetitions the error is still relatively large. The work of Surface and Pearl (1916) shows an advance in the refinement of methods of conducting field

trials. With the realization that the use of frequent control plots often produces results far from satisfactory, these workers have calculated by the contingency method the probable yield of each plot of ground in their grain testing series. This calculated yield represent the most probable yield of each plot on the supposition that they have all been planted with a hypothetical variety whose mean yield is the same as the observed mean of the field. This "calculated" yield may then be used as a basis for determining a correction factor, whereby each area must be given a handicap plus or minus the actual yield, depending upon whether the plot in question is calculated to be a low or a high producing area. This method of correcting the soil variation is combined with four systematically repeated plots of one-fortieth acre of each variety, and gives a high degree of accuracy. Batchelor and Reed (1918) study the nature and extent of the variability of the yields of fruit trees under field conditions and its bearing on the reliability of plot trials. The orchards studied are selected on account of uniformity of treatment and appearance, yet the variability in productivity was considerable. The effect upon variability of combining trees into plots of various sizes and shapes has been investigated. As the number of trees per plot is increased, the coefficient of variability decreases. However there is little gain in accuracy by increasing the plot to include more than eight adjacent trees. Greater reliability may be secured by a systematic repetition and distribution of plots through the experimental area. A 16 tree plot can be expected to give more reliable results if divided into four equal plots and repeated at four regularly placed intervals than can either two eight tree plots or 6 adjacent trees. The fact that marked soil variations occur which tend to make adjacent trees or adjacent plots yield alike, even on soils which are chosen because of their apparent uniformity, is well shown by applying the formula proposed by Harris (1915) for measuring the coefficient of correlation between neighboring plots of the field. Computations made on the yields of fruit trees for several consecutive years showed little annual fluctuation in their variability. Kalamkar (1932) studies the uniformity trial on potato. In his study the standard error in percent of the mean yield decreased slightly with increase in the widths up to plots 5 rows wide, but any further increase in the width of the plot results in the higher standard error. Given a piece of land of certain size, it is advantageous to have a greater replication of smaller plots than a smaller number of larger plots. Four-row plots proves to be the most efficient when the border rows are discarded. The superiority of long and narrow plots over shorter and wider ones is demonstrated.

For efficient conduct of Agricultural field trials knowledge of the proper size & shape of experimental plots and their arrangement in blocks is essential. One major problem encountered in experimental yield trials on field crops is that there exists variation in yield estimates regardless of how the trial is designed/ laid out taking the variety (or treatment). The usual method of finding out the heterogeneity structure of a piece of land is to construct a fertility contour map by conducting uniformity trial. The uniformity trial consists of growing the same crop under uniform treatment and management practices on a piece of land. When the crop is ready for harvest, the entire field is divided into suitable small units and the produce of each unit is recorded separately along with the row and column positions of the selected units. By combining these units suitably, different sizes and shapes of plots are obtained and their variability's for each size and shape can be worked out and compared efficiently.

The effect of inherent soil heterogeneity (without application of fertilizer) upon crop yield has been recognized since long ago. In an early study to determine experimental error of field trials, Mercer and Hall (1912), working with mangels used the concept of probable error to analyse variation in field experiments. They determined optimum plot size on the basis of a curve relating plot size and percent deviation. Under the procedure a field growing the crop under uniform treatment is harvested in small units of suitable size, usually 1m X 1m. The small units are then combined into various sizes. The sum of squares among the various plots are divided by the degrees of freedom to obtain the variances. The mean against various plot sizes are also computed together with the values of the coefficient of variation. These values of the coefficient of variation are plotted against the respective plot sizes. A free hand curve is drawn through the ordinates. It can be seen that the ordinates decrease with increase in plot size but after a particular plot size, the C.V. values do not decrease any further. The plot size above which the corresponding C.V. values become more or less steady and do not decrease further is called the optimum plot size.

## 1.2 SCOPE OF THE WORK:

One major problem encountered in experimental yield trials on field crops is that there exists variation in observed yields regardless of how the trial is designed/ laid out taking the variety (or treatment). The usual method of finding out the heterogeneity structure of a piece of land is to construct a fertility contour map by conducting uniformity trial. The uniformity trial consists of

growing the same crop under uniform treatment and management practices on a piece of land. When the crop is ready for harvest, the entire field is divided into suitable small units and the produce of each unit is recorded separately along with the row and column positions of the selected units. By combining these units suitably, different sizes and shapes of plots are obtained and variability with respect to each size and shape can be worked out and compared efficiently.

The particular experimental material under study determines the plot size to a large extent. Certain types of variabilities and cultural operations are associated with the kind of crop considered under experimentation. The optimum plot size for a variety yield trial for rice is different from that for jute. Hence, for efficient conduct of Agricultural field trials a knowledge of the proper size & shape of experimental plots and their arrangement in blocks is essential. The effect of inherent soil heterogeneity (without application of fertilizer) upon crop yield has been recognized since centuries ago. In an early study to determine experimental error of field trials, Mercer and Hall (1912), working with mangels used the concept of probable error to analyse variation in field experiments. They determined optimum plot size on the basis of a curve relating plot size and percent deviation. Under the procedure a field growing the crop under uniform treatment is harvested in small units of suitable size usually 1m X 1m. The small units are then combined into various sizes. The sum of squares among the various plots are divided by the degrees of freedom to obtain the variances. The mean against various plot sizes are also computed together with the values of the coefficient of variation. These values of the coefficient of variation are plotted against the respective plot sizes. A free hand curve is drawn through the ordinates. It can be seen that the ordinates decrease with increase in plot size but after a particular plot size, the C.V. values do not decrease any further. The plot size above which the corresponding C.V. values become more or less steady and do not decrease further is called the optimum plot size. Many workers used the above method to determine the optimum plot size. Federer (1955) however, pointed out that this method had a weakness in that the above method of determination of the point of optimum plot size was not independent of the smallest unit selected or of the scale of measurement used. Also this method did not consider the relative cost of various plot sizes.

An unscientific approach is again usually adopted when comparing the reduction of variability due to increasing the size of plot with the reduction which is to be expected if the fertilities of the adjacent areas/ plots of the land were uncorrelated or

which is attainable by random replication of unit plots. But since an hypothesis of zero correlation between adjacent areas/ plots can not be regarded as probable (as was demonstrated by Harris, 1915, 1920) it is misleading to speak of it as “theoretically expected”.

No satisfactory quantitative measure of soil heterogeneity was devised till the first decade of twentieth Century. Harris (1915) proposed using the intraclass correlation coefficient of yields from adjacent areas as a “coefficient of heterogeneity”. But although numerous workers have taken the trouble to evaluate such coefficients for their data it does not appear to serve any other purpose than to demonstrate that the fertilities of adjacent areas are correlated. Thereafter Smith (1938) suggested an empirical model relating variability to plot size and shape. He recognized the presence of association between adjacent plots and included a factor ‘*b*’ (called soil heterogeneity) in his proposed model. His model has been the basis for analysis of uniformity studies for many decades.

To the best of the knowledge, no uniformity studies have been reported for Terai agro-climatic zone of North Bengal in the literature. It is expected that this study will be the first of its kind. Keeping these facts in view, it has now become necessary to understand in detail the nature of variation, association, similarity and dissimilarity among data points in different directions and their relation in determining optimum plot and block size and shape. Thus the present studies will be carried out with the following objectives:

#### OBJECTIVES:

1. To find optimum plot size for rice and jute crops (by Smith’s and Sehti’s methods).
2. To find optimum plot shape for rice and jute crops.
3. To find optimum block size and shape for rice and jute crops.
4. To find optimum plot size by variogram analysis.

**1.3 Overview of results:** The works embodied under the research investigation have been carried out on the objectives mentioned as above. The chapters have been prepared keeping an eye to the important and latest reviews available in the literature concerned with optimum plot size. The findings obtained against the above objectives have been delineated precisely below.

#### Chapter 2

Chapter 2 presents an introduction pertaining to the works on optimum plot size and shape based on the Smith's model. Using the cost considerations optimum plot sizes for jute and rice crops are 12.42 sq.m. and 5.51 sq.m. respectively. By relating C.V. to the plot sizes the method of maximum curvature gives the plot sizes of 6.5 sq.m. (1.12m. X 5.76m.) and 15.86 sq.m. (7.84m. X 2.02 m.) for jute and rice crops respectively. For jute data it is observed that blocks should run row wise i.e., along E→W direction, and the larger dimension of the plot should be in the column i.e., along N→S direction. However, for rice data the plot and block orientation should be just the opposite i.e., the blocks should run column wise i.e., along N→S direction, and the larger dimension of the plot should be along the row direction i.e., along E→W direction.

### Chapter 3

The uniformity data are analysed to study the two way spatial correlations present in the field. In the Smith's model we have not considered the spatial covariance aspect while calculating the variance for different plot sizes and shapes. But in this chapter the covariance among plot observations both in the diagonal and off diagonal directions is considered (vide Modjeska and Rawlings, 1983). The optimum plot size is found by using the Smith's cost concept i.e. minimizing the cost per unit of information. However for finding suitable heterogeneity index  $b$  a few criteria like (i)symmetry of diagonal spatial correlation with the off diagonal one (ii) heterogeneity in the row and column directions (iii) plot of  $\ln(\text{STMSE}/\text{plot size})$  vs.  $\ln(\text{plot size})$  for the first and last row and first and last column of the STMSE matrix are considered. For both of my Jute and Rice data neither of Smith's one dimensional nor Smith's two dimensional model can be best fitted to the respective STMSE matrices so that a suitable heterogeneity index and thereby the optimum plot sizes can be found. However by studying the cost per unit of information for the minimum value it is found that optimum plot size is 15 sq.m. (3m. X 5m.) for jute data and 11 sq.m. (11m. X 1m.) for rice data.

### Chapter 4

Here uniformity data are studied in great detail to observe the nature and amount of spatial dependence present in the data. The variogram analysis has been done for different row and column lags at the diagonal and off diagonal directions. The change in spatial dependence with the increase in lag distance among observations is studied using the models, namely, spherical, exponential, Gaussian, Michaelis-Menton & VB. For both Jute and Rice data all of the above mentioned five models provides reasonably good fit ( $R^2 \cong 0.75$ ). However, the amount of

dependency among the estimated parameters is found to be least for exponential and VB models. From the fitted models we observe the values of the three parameters of the variogram model: the range, the sill, and the nugget effect. Here it is understood that the range is the separation distance beyond which two observations are independent of each other. The sill is the variogram value corresponding to the range. The discontinuity at the origin is called the nugget effect and arises from a combination of random errors and sources of variation at distances smaller than the shortest sampling interval (Goovaerts, 1998). Optimum plot size is studied using nugget to sill ratio of the fitted variogram model as one criterion indicating the extent to which the experimental errors between plots were randomly distributed in space (Bhatti *et al.*, 1991; Ersboll, 1996).

#### Chapter 5

Here we suggest a totally new method whereby we observe the amount of maximum curvature of variogram curves for each plot size and shape.

#### Chapter 6

In this chapter we study the historically renowned wheat grain yield uniformity data of Mercer and Hall (1911). Applying the method of maximum curvature to the data relating C.V. to plot sizes we find that optimum plot size is 19.14 sq.m. ( 1.33 m. X 14.39 m.).

#### Chapter 7

In this last chapter we summarise all of the methods studied.

## Chapter 2

### SMITH'S MODEL AND ITS DEVELOPMENT

**2.1 Optimum plot size for isotropic field:** Smith (1938) pointed out that the regression of variability on plot size can be more easily interpreted when the observations are plotted on double logarithmic paper. It becomes linear. Thus the relationship can be described by an equation of the form  $\log(V_x) = \log(V_1) - b \cdot \log(x)$  where  $V_x$  = variance of yield per unit area for plots of  $x$  units of area. Since the variances have been estimated from varying numbers of plots it is desirable that, when fitting a regression equation, each point should be weighted inversely by its variance.

But size of the field is purely arbitrary, and any given field may be considered as a single block of a larger field. Let the variance of the mean yield per unit area, of plots of  $x$  units of area over a block of  $m$  plots be  $(V_x)_m$ . Then the regression which has been empirically observed for a field having  $n$  plots is  $\log(V_x)_{n/x} = \log(V_1)_n - b' \log x$ . But the size of the field,  $n$ , is arbitrarily fixed, and if this regression is theoretically sound it should hold good for any alternative size of field which we may wish to consider as the area over which variances should be measured. But if  $n$  be varied the above regression becomes curved for any value other than that originally assigned. The regression is therefore inconsistent with the requirement that the law shall be unaffected by variation in the size of the field. This difficulty is overcome if we postulate an infinitely large field of which an observed field may represent a single block and suppose that the law be  $\log(V_x)_\infty = \log(V_1)_\infty - b \cdot \log x$ , or  $(V_x)_\infty = \frac{(V_1)_\infty}{x^b}$ . When  $b = 1$  this gives the ordinary formula for the variance of the mean of  $x$  independent units. Since a block is merely a large size plot the variance between blocks can be estimated from the same equation, and thence the variance of plots of  $x$  units within blocks of  $m$  plots is given by an analysis of variance, where  $\lambda$  tends to  $\infty$ , as follows:

|                | d. f.                   | M. S.                      |
|----------------|-------------------------|----------------------------|
| Between blocks | $(\lambda - 1)$         | $m \cdot (V_{xm})_\lambda$ |
| Within blocks  | $\lambda \cdot (m - 1)$ | $(V_x)_m$                  |
| Total          | $(\lambda \cdot m - 1)$ | $(V_x)_{\lambda m}$        |

Thus in the limit:  $(V_x)_m = \frac{m.(V_x)_\infty - m.(V_{xm})_\infty}{m-1} = \frac{m.(1-m^{-b})(V_x)_\infty}{m-1}$ . Here for given values of  $m$

and  $b$ ,  $(V_x)_m / (V_x)_\infty$  is a constant irrespective of  $x$ . Thus the association between neighboring plots is of such a type that the variance per plot within a block of  $m$  plots bears the same ratio to the total variance per plot in an infinite field whatever the plot size.

First we combine  $r \times c$  basic units to simulate plots of different sizes and shapes. Here we use only those combinations that fit exactly into the whole area. Now for each of simulated plots we compute yield total  $T$  as the sum of the  $x$  basic units combined to construct that plot. Now we compute between plot variance  $V_{(x)} = \Sigma T_i^2 / w - \bar{T}^2$  where  $w = (r.c / x)$  is the total number of simulated plots of size  $x$  basic units. For each plot size and shape, compute the variance per unit area as  $V_x = V_{(x)} / x^2$ . For each plot size having more than one shape, we test the homogeneity of between plot variances  $V_{(x)}$ , to determine the significance of plot orientation i.e. plot shape effect, by using F-test or the chi-square test. For each plot size whose plot shape effect is insignificant, we compute the average of  $V_x$  values over all plot shapes. However, when plot shape effect is significant we use the lowest  $V_x$  value.

Now using the values of variance per unit area  $V_x$  and plot size  $x$  we compute the regression coefficient  $b$ . As explained by Smith (1938) the relationship between  $V_x$  and  $x$  is not linear but log linear. As  $V_x = \frac{V_1}{x^b}$  the first step is to linearise the function into a linear form as  $Y = c.X$  where  $Y = \log V_x - \log V_1$ ,  $c = -b$  and  $X = \log x$ . Now minimizing weighted sum of square of residuals i.e.  $RSS = \sum_i w_i.(Y_i - c.X_i)^2$  with respect to  $c$  we get  $\frac{\partial RSS}{\partial c} = 0$  or,

$$2 \cdot \sum_i w_i.(Y_i - c.X_i).X_i = 0 \quad \text{or, } c = \frac{\sum_{i=1}^m w_i.X_i.Y_i}{\sum_{i=1}^m w_i.X_i^2}$$

Thus  $b = -c$ . Here  $w_i$  = the d.f. associated with a given variance. Here the weights are proportional to the reciprocal of the variances. As we have s.d. of  $s$  i.e.  $\partial s = \frac{s}{\sqrt{2n}}$  to a first approximation the variance of the logarithm of a variance may be taken as:

$\{\partial(\log_e s^2)\}^2 = \left\{ \frac{2 \cdot s \cdot \partial s}{s^2} \right\}^2 = \frac{2}{n}$  where  $n$  is the number of degrees of freedom upon which the estimate of variance is based.

The contribution of soil heterogeneity to experimental error stems from differences in soil fertility between plots within a block. The smaller this difference is, the smaller is the experimental error. The choice of suitable plot size and shape, therefore, should reduce the differences in soil productivity from plot to plot within a block and consequently reduce experimental error. Two major considerations are involved in choosing plot size, namely, practical considerations and the nature and size of variability. Practical considerations generally include ease of management in the field. The nature and size of variability is generally related to soil heterogeneity. From the empirical relationship between plot size and between plot variance, it can be seen that while variability becomes smaller as plot size becomes larger, the gain in precision decreases as plot size becomes increasingly large. Furthermore, higher costs are involved when large plots are used. Hence, the plot size that a researcher should aim for is one that balances precision and cost. This is conventionally referred to as *optimum plot size*.

To obtain optimum plot size we assume that cost per unit is known. Let the cost function be of the following linear form  $K_t = K_1 + K_2 \cdot x$ , where  $K_t$  = total cost for the experimental unit,  $K_1$  = part of the cost associated with the number of plots only.  $K_2$  = cost per unit area,  $x$  = size of plot. Then  $C$  = cost / unit of information is given by  $C = \frac{K_1 + K_2 \cdot x}{\frac{1}{V_x}} = \frac{V_x \cdot (K_1 + K_2 \cdot x)}{x^b}$ . Now the value of  $x$  which minimizes the cost ( $C$ ) is given by the

equation  $\frac{dC}{dx} = 0$ . Solving the equation for  $x$  we obtain  $x_{opt} = \frac{b \cdot K_1}{(1-b) \cdot K_2}$ , which gives the

optimum plot size. The value of  $b$  i.e., the index of soil heterogeneity, is used primarily to derive optimum plot size. The value of  $b$  indicates also the degree of correlation between adjacent experimental plots. Its value varies between unity and zero. The larger is the value of the index  $b$ , the lower is the correlation between adjacent plots, indicating that fertile spots are distributed randomly or in patches.

The value of 'b' in the range 0.3 to 0.7 does not greatly effect the increase in cost or in variance when plots of size ¼ to 4 times the optimum plot size are used. On the basis of

these results plot size of  $\frac{1}{2}$  to 2 times the optimum plot size can be taken without any loss in efficiency. However, for plot size  $\frac{1}{4}$  to 4 times the optimum size, a loss in efficiency of 20% results because of the increased variance.

**A UNIFORMITY TRIAL ON JUTE:** A uniformity trial with JRO 524 (Naveen, a variety of jute) was conducted (1999) at the Barokodali State Government Farm (approximately 7 Km from Tufanganj Subdivision of Cooch Behar District). The seeds were sown in continuous lines. The distance between line to line was kept 20 cm leaving a border on each side. Uniform management practices were undertaken throughout the field. The field was harvested in continuous units of 448 basic units. There was in total 32 rows each of which were along N – S direction and 14 columns each of which were along E – W direction. Yield of dried fiber was calculated from each basic unit of 1mt. X 1mt. The units were combined by taking 1 to 9 units along N → S with 1 to 9 units across E → W to form plots of different sizes & shapes.

**A UNIFORMITY TRIAL ON RICE:** A uniformity trial with MW10 (a variety of rice) as Aus paddy was conducted (1999) at the RRS, Terai zone, Pundibari. The seedlings were transplanted in lines with a hill to hill spacing of 20 c.m. The distance between line to line was kept 20 cm leaving a border on each side. Uniform management practices were undertaken throughout the field. There was in total 22 rows each of which were along N → S direction and 18 columns each of which were along E → W direction. The field was harvested in units of 1 mt x 1mt there being 22 mt x 18 mt i.e. 396 such units. The yields of these units were separately dried & weighed correct to the nearest gram.

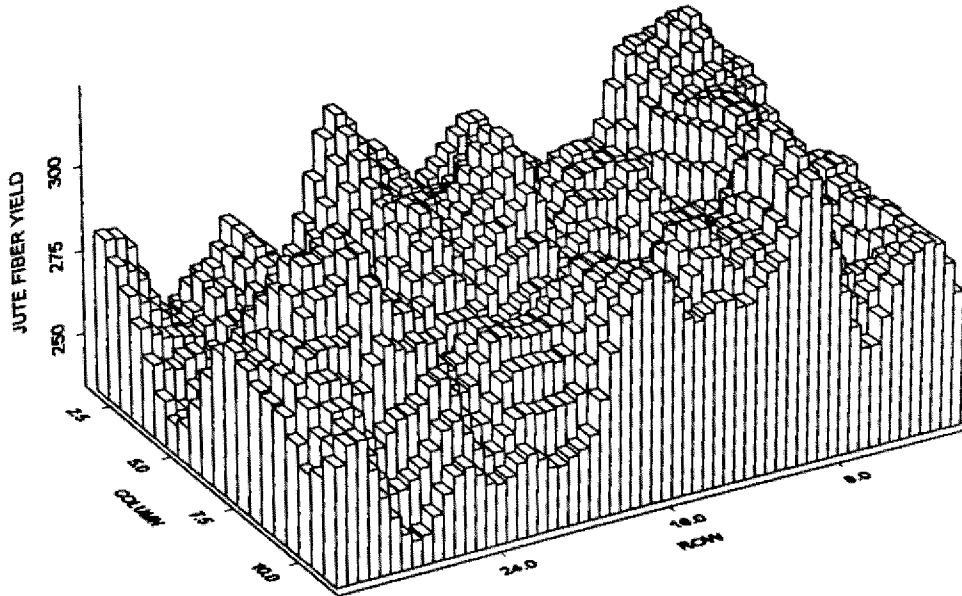


Fig.2.1.1 Jute field fertility contour surface based on moving average of 3X3 basic units.

On Eastern end of the field was dominated by very high yields, the middle region by a mixture of intermediate yields, and the Western end by low yield. Yield was not constant within any of these regions and appeared to change along both row and column.

The Jute uniformity data was analysed based on a two way ANOVA. The result shows that the Row mean square is 1.63 times higher than the Column mean square, indicating that the trend of soil fertility was slightly more pronounced along the row i.e. E->W direction than along the column i.e. N->S direction.

#### ANOVA FOR JUTE UNIFORMITY DATA

| S.O.V. | d.f. | M.S.     | Fcal.     |
|--------|------|----------|-----------|
| Row    | 31   | 218.4804 | 0.1735587 |
| Column | 11   | 133.1731 | 0.1057914 |
| Error  | 341  | 1258.827 |           |
| Total  | 383  | 1610.48  |           |

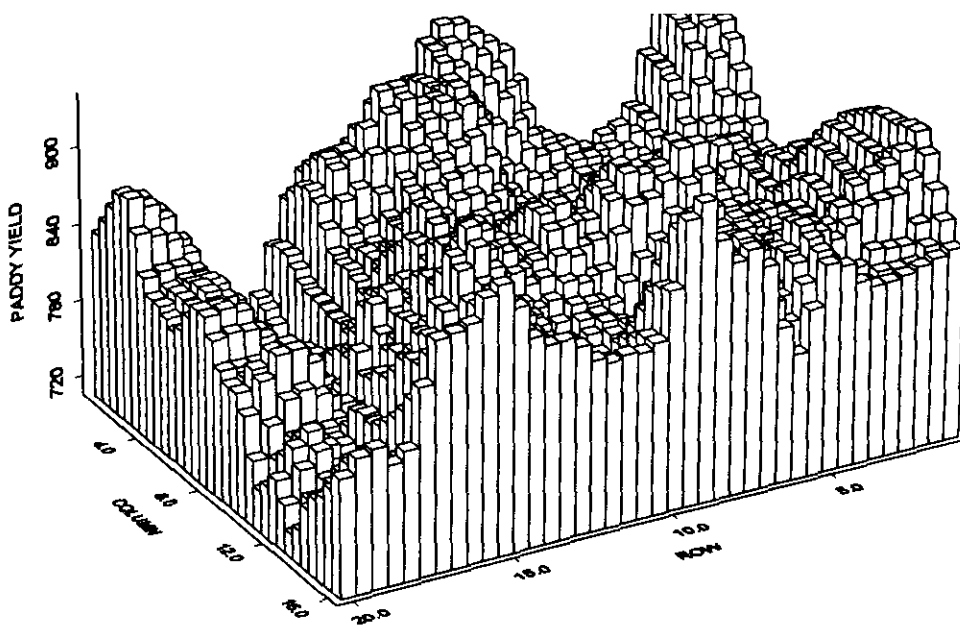


Fig. 2.1.2 Rice field fertility contour surface based on moving averages of 3X3 basic units.

On the borders of Eastern, Northern & Southern ends of the Rice field are dominated by very high yields, the middle region by a mixture of high and intermediate yields and Western borders by low yields. Yield was not constant within any of these regions and appeared to change along both row and column.

The Rice uniformity data was analysed based on a two way ANOVA. The result shows that the Row mean square is more than four times higher than the Column mean square, indicating that the trend of soil fertility was more pronounced along the row i.e. E->W direction than along the column i.e. N->S direction.

ANOVA FOR RICE UNIFORMITY DATA

| S.O.V. | d.f. | M.S.     | Fcal.      |
|--------|------|----------|------------|
| Row    | 21   | 1978.732 | 0.1717749  |
| Column | 17   | 490.308  | 0.04256392 |
| Error  | 357  | 11519.33 |            |
| Total  | 395  | 13988.38 |            |

Smith's optimum: The basic units were combined by taking 1 to 9 units along N→S with 1 to 9 units across E→W to form plots of different sizes & shapes for rice and jute data individually. Based on this between plot variance  $V_{(x)}$ , Variance per unit area  $V_x$  and coefficient of variability C.V. are calculated for plots of various size and shapes. These are shown in the following tables:

TABLE:2.1.1(Jute data)

| PLOT SIZE | Wid-th | Len-gth | No.of Plots | PLOT MEAN | VARIANCE | VARIANCE /SQ.MT | C.V.     |
|-----------|--------|---------|-------------|-----------|----------|-----------------|----------|
| 1         | 1      | 1       | 384         | 276.2578  | 1610.48  | 1610.48         | 14.52657 |
| 2         | 2      | 1       | 192         | 552.5156  | 3850.241 | 962.5602        | 11.23051 |
| 2         | 1      | 2       | 192         | 552.5156  | 3683.476 | 920.8691        | 10.9846  |
| 3         | 3      | 1       | 120         | 829.7584  | 6892.605 | 765.845         | 10.00553 |
| 3         | 1      | 3       | 128         | 828.7734  | 6039.638 | 671.0709        | 9.377122 |
| 4         | 4      | 1       | 96          | 1105.031  | 9688.674 | 605.5421        | 8.907537 |
| 4         | 2      | 2       | 96          | 1105.031  | 9145.685 | 571.6053        | 8.654332 |
| 4         | 1      | 4       | 96          | 1105.031  | 7038.905 | 439.9316        | 7.592381 |
| 5         | 5      | 1       | 72          | 1382.931  | 14923.21 | 596.9285        | 8.833459 |
| 5         | 1      | 5       | 64          | 1396.563  | 10267.3  | 410.6921        | 7.255507 |
| 6         | 6      | 1       | 60          | 1659.517  | 20687.05 | 574.6403        | 8.666978 |
| 6         | 3      | 2       | 60          | 1659.517  | 18360.54 | 510.0151        | 8.165094 |
| 6         | 2      | 3       | 64          | 1657.547  | 13024.32 | 361.7866        | 6.885124 |
| 6         | 1      | 6       | 64          | 1657.547  | 13992.95 | 388.6931        | 7.136559 |
| 7         | 7      | 1       | 48          | 1940.917  | 27332.13 | 557.7985        | 8.517846 |
| 7         | 1      | 7       | 32          | 1935.281  | 22072.06 | 450.4503        | 7.67675  |
| 8         | 8      | 1       | 48          | 2210.063  | 28331.91 | 442.6862        | 7.616113 |
| 8         | 4      | 2       | 48          | 2210.063  | 25416.85 | 397.1383        | 7.213671 |
| 8         | 2      | 4       | 48          | 2210.063  | 13128.51 | 205.133         | 5.184456 |
| 8         | 1      | 8       | 32          | 2211.531  | 20612.64 | 322.0726        | 6.491929 |
| 9         | 9      | 1       | 36          | 2496.556  | 35958.69 | 443.9344        | 7.595576 |
| 9         | 3      | 3       | 40          | 2489.275  | 26544.72 | 327.7126        | 6.545098 |
| 9         | 1      | 9       | 32          | 2492.063  | 21952.26 | 271.0155        | 5.945395 |
| 10        | 5      | 2       | 36          | 2765.861  | 42883.43 | 428.8343        | 7.487113 |
| 10        | 2      | 5       | 32          | 2793.125  | 17482.84 | 174.8284        | 4.733862 |
| 12        | 6      | 2       | 30          | 3319.033  | 59150.9  | 410.7701        | 7.327724 |
| 12        | 4      | 3       | 32          | 3315.094  | 33146.07 | 230.181         | 5.491868 |
| 12        | 3      | 4       | 30          | 3319.033  | 28774.07 | 199.8199        | 5.110801 |
| 12        | 2      | 6       | 32          | 3315.094  | 32910.71 | 228.5466        | 5.472336 |
| 14        | 7      | 2       | 24          | 3881.833  | 76620.7  | 390.9219        | 7.130765 |
| 14        | 2      | 7       | 16          | 3870.563  | 41125.6  | 209.8245        | 5.239406 |
| 15        | 5      | 3       | 24          | 4148.792  | 54537.22 | 242.3876        | 5.628918 |
| 15        | 3      | 5       | 20          | 4195.6    | 43627.47 | 193.8999        | 4.978356 |
| 16        | 8      | 2       | 24          | 4420.125  | 80681.74 | 315.1631        | 6.426183 |
| 16        | 4      | 4       | 24          | 4420.125  | 27894.26 | 108.962         | 3.77853  |
| 16        | 2      | 8       | 16          | 4423.063  | 34289.07 | 133.9417        | 4.186535 |
| 18        | 9      | 2       | 18          | 4993.111  | 93382.82 | 288.2186        | 6.120153 |
| 18        | 6      | 3       | 20          | 4978.55   | 81695.58 | 252.1469        | 5.741117 |
| 18        | 3      | 6       | 20          | 4978.55   | 76373.48 | 235.7206        | 5.550964 |

| PLOT SIZE | Wid-th | Len-gth | No.of Plots | PLOT MEAN | VARIANCE | VARIANCE /SQ.MT | C.V.     |
|-----------|--------|---------|-------------|-----------|----------|-----------------|----------|
| 20        | 4      | 5       | 16          | 5586.25   | 46513.07 | 116.2827        | 3.860709 |
| 21        | 7      | 3       | 16          | 5822.75   | 100332.1 | 227.5105        | 5.439911 |
| 21        | 3      | 7       | 10          | 5807.4    | 127643.8 | 289.4417        | 6.152025 |
| 24        | 8      | 3       | 16          | 6630.188  | 109432.5 | 189.987         | 4.98939  |
| 24        | 6      | 4       | 15          | 6638.067  | 80592    | 139.9167        | 4.276657 |
| 24        | 4      | 6       | 16          | 6630.188  | 75986.13 | 131.9204        | 4.157587 |
| 24        | 3      | 8       | 10          | 6630      | 111061.3 | 192.8148        | 5.026526 |
| 25        | 5      | 5       | 12          | 6992.667  | 100211.5 | 160.3383        | 4.527056 |
| 27        | 9      | 3       | 12          | 7489.667  | 104260.2 | 143.0181        | 4.311186 |
| 27        | 3      | 9       | 10          | 7478.3    | 91430.22 | 125.4187        | 4.043356 |
| 28        | 7      | 4       | 12          | 7763.667  | 113961.5 | 145.359         | 4.348226 |
| 28        | 4      | 7       | 8           | 7741.125  | 112005.7 | 142.8644        | 4.323306 |
| 30        | 6      | 5       | 10          | 8391.2    | 132592.4 | 147.3249        | 4.339457 |
| 30        | 5      | 6       | 12          | 8297.583  | 157490.2 | 174.9891        | 4.782722 |
| 32        | 8      | 4       | 12          | 8840.25   | 84834.91 | 82.84659        | 3.294752 |
| 32        | 4      | 8       | 8           | 8846.125  | 100269.7 | 97.91964        | 3.579578 |
| 35        | 7      | 5       | 8           | 9824.75   | 166125.1 | 135.6124        | 4.148549 |
| 35        | 5      | 7       | 6           | 9679      | 249047.6 | 203.3042        | 5.155973 |
| 36        | 9      | 4       | 9           | 9986.223  | 139181   | 107.3927        | 3.735844 |
| 36        | 6      | 6       | 10          | 9957.1    | 231927.1 | 178.9561        | 4.83663  |
| 36        | 4      | 9       | 8           | 9968.25   | 77691.43 | 59.94709        | 2.796196 |
| 40        | 8      | 5       | 8           | 11172.5   | 148498.3 | 92.81142        | 3.449136 |
| 40        | 5      | 8       | 6           | 11050     | 236774.4 | 147.984         | 4.403572 |
| 42        | 7      | 6       | 8           | 11645.5   | 293894.3 | 166.6067        | 4.65519  |
| 42        | 6      | 7       | 5           | 11614.8   | 339805   | 192.6332        | 5.018838 |
| 45        | 9      | 5       | 6           | 12620.67  | 150843.2 | 74.49047        | 3.077376 |
| 45        | 5      | 9       | 6           | 12463.83  | 171169.6 | 84.5282         | 3.319416 |
| 48        | 8      | 6       | 8           | 13260.38  | 252347.4 | 109.5258        | 3.788294 |
| 48        | 6      | 8       | 5           | 13260     | 316752   | 137.4792        | 4.244399 |
| 49        | 7      | 7       | 4           | 13620.25  | 582604   | 242.6506        | 5.604045 |
| 54        | 9      | 6       | 6           | 14979.33  | 311084   | 106.6818        | 3.723457 |
| 54        | 6      | 9       | 5           | 14956.6   | 217356   | 74.53909        | 3.117116 |
| 56        | 8      | 7       | 4           | 15482.25  | 341125.3 | 108.7772        | 3.772445 |
| 56        | 7      | 8       | 4           | 15534.75  | 546352   | 174.2194        | 4.758083 |
| 63        | 9      | 7       | 3           | 17502.33  | 529995   | 133.5336        | 4.159488 |
| 63        | 7      | 9       | 4           | 17513.5   | 437853.3 | 110.3183        | 3.778256 |
| 64        | 8      | 8       | 4           | 17692.25  | 286378.7 | 69.91666        | 3.024734 |
| 72        | 9      | 8       | 3           | 19942.33  | 639336   | 123.3287        | 4.009485 |
| 72        | 8      | 9       | 4           | 19936.5   | 233408   | 45.02469        | 2.42331  |
| 81        | 9      | 9       | 3           | 22465.67  | 477797   | 72.82381        | 3.076822 |

TABLE:2.1.1A(Jute data) average values for same plot sizes but different shapes.

| PLOT<br>SIZE | No.of<br>Plots | PLOT     |          | VARIANCE |          |
|--------------|----------------|----------|----------|----------|----------|
|              |                | MEAN     | VARIANCE | /SQ.MT   | C.V.     |
| 1            | 384            | 276.2578 | 1610.48  | 1610.48  | 14.52657 |
| 2            | 192            | 552.5156 | 3766.859 | 941.7147 | 11.10756 |
| 3            | 124            | 829.2659 | 6466.122 | 718.458  | 9.691326 |
| 4            | 96             | 1105.031 | 8624.421 | 539.0263 | 8.38475  |
| 5            | 68             | 1389.747 | 12595.26 | 503.8103 | 8.044483 |
| 6            | 62             | 1658.532 | 16516.22 | 458.7838 | 7.713439 |
| 7            | 40             | 1938.099 | 24702.1  | 504.1244 | 8.097298 |
| 8            | 44             | 2210.43  | 21872.48 | 341.7575 | 6.626542 |
| 9            | 36             | 2492.631 | 28151.89 | 347.5542 | 6.695356 |
| 10           | 34             | 2779.493 | 30183.14 | 301.8314 | 6.110488 |
| 12           | 31             | 3317.064 | 38495.44 | 267.3294 | 5.850682 |
| 14           | 20             | 3876.198 | 58873.15 | 300.3732 | 6.185086 |
| 15           | 22             | 4172.196 | 49082.35 | 218.1438 | 5.303637 |
| 16           | 21.33          | 4421.104 | 47621.69 | 186.0223 | 4.797083 |
| 18           | 18.5           | 4983.584 | 69286.7  | 213.8479 | 5.157093 |
| 20           | 17             | 5558.986 | 51886.65 | 129.7167 | 4.093254 |
| 21           | 13             | 5815.075 | 113988   | 258.4761 | 5.795968 |
| 24           | 14.25          | 6632.111 | 94267.98 | 163.6597 | 4.61254  |
| 25           | 12             | 6992.667 | 100211.5 | 160.3383 | 4.527056 |
| 27           | 11             | 7483.984 | 97845.21 | 134.2184 | 4.177271 |
| 28           | 10             | 7752.396 | 112983.6 | 144.1117 | 4.335766 |
| 30           | 11             | 8344.392 | 145041.3 | 161.157  | 4.56109  |
| 32           | 10             | 8843.188 | 92552.31 | 90.38312 | 3.437165 |
| 35           | 7              | 9751.875 | 207586.4 | 169.4583 | 4.652261 |
| 36           | 9              | 9970.524 | 149599.8 | 115.432  | 3.789557 |
| 40           | 7              | 11111.25 | 192636.4 | 120.3977 | 3.926354 |
| 42           | 6.5            | 11630.15 | 316849.7 | 179.62   | 4.837014 |
| 45           | 6              | 12542.25 | 161006.4 | 79.50934 | 3.198396 |
| 48           | 6.5            | 13260.19 | 284549.7 | 123.5025 | 4.016347 |
| 49           | 4              | 13620.25 | 582604   | 242.6506 | 5.604045 |
| 54           | 5.5            | 14967.97 | 264220   | 90.61045 | 3.420287 |
| 56           | 4              | 15508.5  | 443738.7 | 141.4983 | 4.265264 |
| 63           | 3.5            | 17507.92 | 483924.2 | 121.926  | 3.968872 |
| 64           | 4              | 17692.25 | 286378.7 | 69.91666 | 3.024734 |
| 72           | 3.5            | 19939.42 | 436372   | 84.1767  | 3.216398 |
| 81           | 3              | 22465.67 | 477797   | 72.82381 | 3.076822 |

TABLE 2.1.2: Rice data

| Plot<br>Size | Wid-<br>th | Len-<br>gth | No.of<br>Plots | Plot<br>MEAN | VARIANCE | Variance<br>/sq.mt. | C.V.     |
|--------------|------------|-------------|----------------|--------------|----------|---------------------|----------|
| 1            | 1          | 1           | 396            | 835.1843     | 13988.38 | 13988.38            | 14.16124 |
| 2            | 2          | 1           | 198            | 1670.369     | 27349.12 | 6837.279            | 9.90055  |
| 2            | 1          | 2           | 198            | 1670.369     | 35538.84 | 8884.711            | 11.28598 |
| 3            | 3          | 1           | 126            | 2515.262     | 39960.83 | 4440.092            | 7.947564 |
| 3            | 1          | 3           | 132            | 2505.553     | 60863.75 | 6762.639            | 9.846361 |

| Plot Size | Width | Length | No. of Plots | Plot MEAN | VARIANCE | Variance /sq.mt. | C.V.     |
|-----------|-------|--------|--------------|-----------|----------|------------------|----------|
| 4         | 4     | 1      | 90           | 3357.145  | 53770.79 | 3360.674         | 6.907218 |
| 4         | 2     | 2      | 99           | 3340.737  | 80709.23 | 5044.327         | 8.503922 |
| 4         | 1     | 4      | 88           | 3333.386  | 95908.78 | 5994.299         | 9.290595 |
| 5         | 5     | 1      | 72           | 4196.431  | 62910.65 | 2516.426         | 5.976983 |
| 5         | 1     | 5      | 66           | 4157.091  | 123822.5 | 4952.901         | 8.464675 |
| 6         | 6     | 1      | 54           | 5050.056  | 79760.91 | 2215.581         | 5.592408 |
| 6         | 3     | 2      | 63           | 5030.524  | 106220.4 | 2950.566         | 6.478743 |
| 6         | 2     | 3      | 66           | 5011.106  | 136336.7 | 3787.132         | 7.368395 |
| 6         | 1     | 6      | 66           | 5011.106  | 153177.6 | 4254.933         | 7.810233 |
| 7         | 7     | 1      | 54           | 5868.944  | 107111.2 | 2185.944         | 5.576447 |
| 7         | 1     | 7      | 44           | 5813.364  | 193632.8 | 3951.689         | 7.569408 |
| 8         | 8     | 1      | 36           | 6807.583  | 89870.63 | 1404.229         | 4.403682 |
| 8         | 4     | 2      | 45           | 6714.289  | 170132.4 | 2658.318         | 6.143183 |
| 8         | 2     | 4      | 44           | 6666.773  | 236410   | 3693.907         | 7.293186 |
| 8         | 1     | 8      | 44           | 6666.773  | 269960.9 | 4218.14          | 7.79354  |
| 9         | 9     | 1      | 36           | 7575.083  | 92057.6  | 1136.514         | 4.005367 |
| 9         | 3     | 3      | 42           | 7545.786  | 187989.1 | 2320.853         | 5.74595  |
| 9         | 1     | 9      | 44           | 7516.659  | 292946.6 | 3616.625         | 7.200611 |
| 10        | 5     | 2      | 36           | 8392.861  | 169155.7 | 1691.557         | 4.900419 |
| 10        | 2     | 5      | 33           | 8314.182  | 334565   | 3345.65          | 6.956979 |
| 12        | 6     | 2      | 27           | 10100.11  | 240029.5 | 1666.872         | 4.85072  |
| 12        | 4     | 3      | 30           | 10071.43  | 287783.7 | 1998.498         | 5.326499 |
| 12        | 3     | 4      | 28           | 10034.93  | 334312.3 | 2321.613         | 5.761849 |
| 12        | 2     | 6      | 33           | 10022.21  | 376188   | 2612.417         | 6.119823 |
| 14        | 7     | 2      | 27           | 11737.89  | 306715.1 | 1564.873         | 4.718213 |
| 14        | 2     | 7      | 22           | 11626.73  | 534253.7 | 2725.784         | 6.286607 |
| 15        | 5     | 3      | 24           | 12589.29  | 263770.4 | 1172.313         | 4.079545 |
| 15        | 3     | 5      | 21           | 12519.9   | 481429.6 | 2139.687         | 5.541985 |
| 16        | 8     | 2      | 18           | 13615.17  | 286930.8 | 1120.823         | 3.934283 |
| 16        | 4     | 4      | 20           | 13403.4   | 520879.2 | 2034.684         | 5.384601 |
| 16        | 2     | 8      | 22           | 13333.55  | 707925.3 | 2765.333         | 6.310272 |
| 18        | 9     | 2      | 18           | 15150.17  | 257340.2 | 794.26           | 3.348393 |
| 18        | 6     | 3      | 18           | 15150.17  | 373504   | 1152.79          | 4.033947 |
| 18        | 3     | 6      | 21           | 15091.57  | 535516.8 | 1652.83          | 4.849    |
| 18        | 2     | 9      | 22           | 15033.32  | 761731.1 | 2351.022         | 5.805585 |
| 20        | 5     | 4      | 16           | 16754.25  | 513668.3 | 1284.171         | 4.27776  |
| 20        | 4     | 5      | 15           | 16709.2   | 757961.1 | 1894.903         | 5.210361 |
| 21        | 7     | 3      | 18           | 17606.83  | 508176.9 | 1152.329         | 4.048799 |
| 21        | 3     | 7      | 14           | 17494.86  | 787478.1 | 1785.665         | 5.072346 |
| 24        | 8     | 3      | 12           | 20422.75  | 332171.6 | 576.6868         | 2.822066 |
| 24        | 6     | 4      | 12           | 20164.83  | 699194.2 | 1213.879         | 4.146715 |
| 24        | 4     | 6      | 15           | 20142.87  | 727899.4 | 1263.714         | 4.235595 |
| 24        | 3     | 8      | 14           | 20069.86  | 1052416  | 1827.111         | 5.111513 |
| 25        | 5     | 5      | 12           | 20886.5   | 611211.6 | 977.9386         | 3.743089 |
| 27        | 9     | 3      | 12           | 22725.25  | 366964.4 | 503.3805         | 2.665651 |
| 27        | 3     | 9      | 14           | 22637.36  | 1224071  | 1679.11          | 4.887397 |

| Plot Size | Wid-th | Len-gth | No.of Plots | Plot MEAN | VARIANCE | Variance /sq.mt. | C.V.     |
|-----------|--------|---------|-------------|-----------|----------|------------------|----------|
| 28        | 7      | 4       | 12          | 23414.83  | 1006976  | 1284.408         | 4.285667 |
| 28        | 4      | 7       | 10          | 23345.8   | 1167239  | 1488.825         | 4.627764 |
| 30        | 6      | 5       | 9           | 25112     | 910596   | 1011.773         | 3.799982 |
| 30        | 5      | 6       | 12          | 25178.58  | 589410.9 | 654.9011         | 3.049143 |
| 32        | 8      | 4       | 8           | 27253.5   | 597357.7 | 583.3571         | 2.835926 |
| 32        | 4      | 8       | 10          | 26806.8   | 1635726  | 1597.389         | 4.77101  |
| 35        | 7      | 5       | 9           | 29213.11  | 1497438  | 1222.398         | 4.188868 |
| 35        | 5      | 7       | 8           | 29182.25  | 905826.3 | 739.4501         | 3.261397 |
| 36        | 9      | 4       | 8           | 30247.25  | 569828.6 | 439.6825         | 2.495665 |
| 36        | 6      | 6       | 9           | 30300.33  | 886656   | 684.1481         | 3.107636 |
| 36        | 4      | 9       | 10          | 30214.3   | 1573305  | 1213.97          | 4.151393 |
| 40        | 8      | 5       | 6           | 33976.33  | 673126.4 | 420.704          | 2.414748 |
| 40        | 5      | 8       | 8           | 33508.5   | 1586304  | 991.44           | 3.758705 |
| 42        | 7      | 6       | 9           | 35213.67  | 1250952  | 709.1564         | 3.176209 |
| 42        | 6      | 7       | 6           | 35068     | 1140448  | 646.5125         | 3.045276 |
| 45        | 9      | 5       | 6           | 37668     | 554096   | 273.6277         | 1.97615  |
| 45        | 5      | 9       | 8           | 37767.88  | 1761659  | 869.9553         | 3.514297 |
| 48        | 8      | 6       | 6           | 40845.5   | 107212.8 | 46.53333         | 0.80164  |
| 48        | 6      | 8       | 6           | 40329.67  | 1812224  | 786.5555         | 3.337961 |
| 49        | 7      | 7       | 6           | 40821.33  | 1871699  | 779.5499         | 3.351435 |
| 54        | 9      | 6       | 6           | 45450.5   | 279961.6 | 96.00877         | 1.164154 |
| 54        | 6      | 9       | 6           | 45450.5   | 2289459  | 785.1369         | 3.329107 |
| 56        | 8      | 7       | 4           | 47494.5   | 256170.7 | 81.68707         | 1.065667 |
| 56        | 7      | 8       | 6           | 46829.67  | 3119360  | 994.6938         | 3.771479 |
| 63        | 9      | 7       | 4           | 52602     | 149552   | 37.68002         | 0.73518  |
| 63        | 7      | 9       | 6           | 52820.5   | 3264122  | 822.404          | 3.420429 |
| 64        | 8      | 8       | 4           | 54507     | 1319936  | 322.25           | 2.107774 |
| 72        | 9      | 8       | 4           | 60494.5   | 1730773  | 333.8683         | 2.174724 |
| 72        | 8      | 9       | 4           | 61268.25  | 736341.3 | 142.0412         | 1.400568 |
| 81        | 9      | 9       | 4           | 68175.75  | 2025472  | 308.7139         | 2.087532 |

TABLE 2.1.2A: (Rice data) average values for same plot sizes but different shapes.

| Plot Size | No.of Plots | Plot MEAN | VARIANCE  | Variance /sq.mt. | C.V.     |
|-----------|-------------|-----------|-----------|------------------|----------|
| 1         | 396         | 835.1843  | 13988.38  | 13988.38         | 14.16124 |
| 2         | 198         | 1670.369  | 31443.98  | 7860.995         | 10.59327 |
| 3         | 129         | 2510.408  | 50412.29  | 5601.366         | 8.896963 |
| 4         | 92.3        | 3343.756  | 76796.267 | 4799.767         | 8.233912 |
| 5         | 69          | 4176.761  | 93366.575 | 3734.664         | 7.220829 |
| 6         | 62.3        | 5025.698  | 118873.9  | 3302.053         | 6.812445 |
| 7         | 49          | 5841.154  | 150372    | 3068.817         | 6.572928 |
| 8         | 42.3        | 6713.855  | 191593.48 | 2993.649         | 6.408398 |
| 9         | 40.7        | 7545.843  | 190997.77 | 2357.997         | 5.650643 |
| 10        | 34.5        | 8353.522  | 251860.35 | 2518.604         | 5.928699 |
| 12        | 29.5        | 10057.17  | 309578.38 | 2149.85          | 5.514723 |
| 14        | 24.5        | 11682.31  | 420484.4  | 2145.329         | 5.50241  |

| Plot Size | No.of Plots | Plot MEAN | VARIANCE  | Variance /sq.mt. | C.V.     |
|-----------|-------------|-----------|-----------|------------------|----------|
| 15        | 22.5        | 12554.6   | 372600    | 1656             | 4.810765 |
| 16        | 20          | 13450.71  | 505245.1  | 1973.613         | 5.209719 |
| 18        | 19.8        | 15106.31  | 482023.03 | 1487.726         | 4.509231 |
| 20        | 15.5        | 16731.73  | 635814.7  | 1589.537         | 4.744061 |
| 21        | 16          | 17550.85  | 647827.5  | 1468.997         | 4.560573 |
| 24        | 13.3        | 20200.08  | 702920.3  | 1220.348         | 4.078972 |
| 25        | 12          | 20886.5   | 611211.6  | 977.9386         | 3.743089 |
| 27        | 13          | 22681.31  | 795517.7  | 1091.245         | 3.776524 |
| 28        | 11          | 23380.32  | 1087107.5 | 1386.617         | 4.456716 |
| 30        | 10.5        | 25145.29  | 750003.45 | 833.3371         | 3.424563 |
| 32        | 9           | 27030.15  | 1116541.9 | 1090.373         | 3.803468 |
| 35        | 8.5         | 29197.68  | 1201632.2 | 980.9241         | 3.725133 |
| 36        | 9           | 30253.96  | 1009929.9 | 779.2669         | 3.251565 |
| 40        | 7           | 33742.42  | 1129715.2 | 706.072          | 3.086727 |
| 42        | 7.5         | 35140.84  | 1195700   | 677.8345         | 3.110743 |
| 45        | 7           | 37717.94  | 1157877.5 | 571.7915         | 2.745224 |
| 48        | 6           | 40587.59  | 959718.4  | 416.5444         | 2.0698   |
| 49        | 6           | 40821.33  | 1871699   | 779.5499         | 3.351435 |
| 54        | 6           | 45450.5   | 1284710.3 | 440.5728         | 2.246631 |
| 56        | 5           | 47162.09  | 1687765.4 | 538.1904         | 2.418573 |
| 63        | 5           | 52711.25  | 1706837   | 430.042          | 2.077805 |
| 64        | 4           | 54507     | 1319936   | 322.25           | 2.107774 |
| 72        | 4           | 60881.38  | 1233557.2 | 237.9548         | 1.787646 |
| 81        | 4           | 68175.75  | 2025472   | 308.7139         | 2.087532 |

From the above table it is observed that both variance per unit area and C.V. decrease with the increase in size of plot. For calculating Smith's heterogeneity coefficient  $b$  we consider only those plot shapes which fit exactly into the whole field. For Jute data the Smith's coefficient is 0.715 and its corresponding optimum plot size is 12.42 sq.mt. However for rice data Smith's coefficient is 0.54 and its corresponding optimum plot size is 5.51 sq.mt. The relatively high value of heterogeneity index for jute data indicate that the jute data are relatively random than rice field data.

**2.2 Heterogeneity for non-isotropic field:** Smith's empirical law relating the variance of crop yields per unit area to plot size is  $V_n = V_1 / n^b$  where  $V_n$  is the variance among plots with an area of  $n$  units and  $V_1$  is the variance among plots of unit size. The factor  $b$  is an index of heterogeneity. If the plots are spatially uncorrelated, then  $b$  will be 1. It can approach a limiting value of zero if no heterogeneity exists. If  $n$  corresponds to an area  $W$  and the size of the basic

plot is  $w$  we can rewrite the above equation as  $V_w = V_w.[w/W]^b$  where  $V_w$  and  $V_w$  are the two corresponding variances. Smith's empirical law is applicable only under the broad assumption of an isotropic field. However, in field it is often encountered that the fertility pattern shows a directional trend. To take anisotropy into account, a general variance relationship similar to Smith's law may be written as  $V_{n,s} = V_1/(n_1^{b_1}.n_2^{b_2}) \dots\dots(i)$  where  $n_1, n_2$  are the numbers of basic plots taken along the row, column directions respectively.  $V_1$  is the variance of the basic plots,  $V_{n,s}$  is the variance of plots each of which has  $n = n_1.n_2$  basic plots.  $b_1$  and  $b_2$  are the indices which characterize the heterogeneity in the  $X, Y$  directions of a 2-D field, respectively. Such anisotropic models are used by Modjeska and Rawlings (1983), Sethi (1985), Zhang *et al.* (1994) etc. For an isotropic field,  $b_1 = b_2$  resulting in  $V_{n,s} = V_1/(n_1.n_2)^{b_1}$  which is essentially the same as given by Smith. For a completely uniform field  $b_1 = b_2 = 0$ ; and for a field with no spatial correlation,  $b_1 = b_2 = 1$ . In a logarithmic form we can write  $\log(V_{n,s}/V_1) = -b_1 \log(n_1) - b_2 \log(n_2) \dots\dots(ii)$  which will be used to compute the indices of heterogeneity, i.e.  $b_1$  and  $b_2$  from available data.  $V_1$  is calculated from the basic units (the original data) while  $V_{n,s}$  is estimated from reconstructed plots each of which consists of  $n = n_1.n_2$  basic units. During the reconstruction of the plots, if  $n_2$  is fixed (e.g.  $n_2 = 1$ ) and  $n_1$  is varied i.e.  $n_1 = 1, 2, 3, \dots\dots$ ,  $V_{n,s}$  is a function of  $n_1$  only. Therefore, the second term i.e.  $b_2 \log(n_2)$  is constant and we can compute  $b_1$  from the  $\log(V_{n,s}/V_1)$  vs.  $\log(n_1)$  relationship. Similarly, if  $n_1$  is fixed and  $n_2$  is varied,  $b_2$  can be computed from the relationship of  $\log(V_{n,s}/V_1)$  vs.  $\log(n_2)$ . If the same number of units are taken in the  $X$  and  $Y$  directions, or  $n_1 = n_2$ , we have  $\log(V_{n,s}/V_1) = -(b_1 + b_2). \log(n_1) = -b_s. \log(n_1) \dots\dots(iii)$  Thus  $b_s$  can be obtained from the linear regression of  $\log(V_{n,s}/V_1)$  on  $\log(n_1)$ . Now to verify whether the equation  $V_{n,s} = V_1/(n_1^{b_1}.n_2^{b_2})$  is a reasonable mathematical form to characterize heterogeneity in two directions, the sum of  $b_1$  and  $b_2$  computed from equation (ii) should be close to  $b_s$  independently computed from equation (iii). To study the effect of plot shapes on variances Zhang *et al.* (1994) have used an index called relative difference of variance i.e.  $RV = 100.(V_{n,s} - V_n)/V_n$  where  $V_{n,s}$  is computed using

equation (i) and  $V_n = V_1 / (n_1 \cdot n_2)^{0.5(b_1 + b_2)}$  which represents the variance assuming that the field is isotropic. Less RV value will indicate a more efficient plot. Earlier optimum plot size has been defined as the size which balances between precision and sampling cost. The cost per plot is given by a linear relation (Smith, 1938; Weber and Horner, 1957)  $K_1 + K_2 \cdot n$ . Thus an objective function accounting for both cost and variance in an isotropic field can be expressed by  $C = (K_1 + K_2 \cdot n) \cdot \frac{V_1}{n^b}$  where  $n$  is the number of units in the chosen plot and  $K_1, K_2$  are the cost

components as defined earlier. This objective function is minimized when  $n_0 = \frac{K_1 \cdot b}{K_2 \cdot (1 - b)}$  where

$n_0$  is the optimum plot size in terms of the number of basic units. Let,  $K = \frac{K_2}{K_1}$ , we have

$n_0 \cdot K = \frac{b}{1 - b}$ . Again let,  $z = \frac{n}{n_0}$  (i.e. the ratio of plot size of  $n$  units to the most efficient size of

$n_0$  units), then the objective function can be rewritten as  $C = K_1 \left[ 1 + \frac{b}{1 - b} \cdot z \right] \cdot \frac{V_1}{n^b}$ . Now if  $C$  is the

cost related to variance for a specified plot size  $n$  and  $C_{\min}$  is the cost related to variance for the optimum plot size  $n_0$  then using Smith's (1938) definition the relative cost is

$y = \frac{C}{C_{\min}} = b \cdot z^{(1-b)} + (1 - b) \cdot z^{-b}$ . In non-isotropic fields, the cost per plot may be given by

$K_1 + K_2 \cdot n_1 \cdot n_2$  (Zhang *et al.*, 1994). Here the objective function accounting for both cost and

variance is  $C_s = (K_1 + K_2 \cdot n_1 \cdot n_2) \cdot \frac{V_1}{n_1^{b_1} \cdot n_2^{b_2}}$  where  $n_1 \cdot n_2$  is the number of basic units in a chosen

plot. When  $b_1 \leq 0.5$  and  $b_2 \leq 0.5$ ,  $C_s$  is a monotone increasing function of  $n_1$  and  $n_2$ . When  $b_1$  or / and  $b_2$  are greater than 0.5, the minimum value of  $C_s$  depends on the larger value of the

heterogeneity indices. If  $b_1 > b_2$ ,  $C_s$  has a minimum value when  $n_1 = \frac{K_1 \cdot b_1}{[k_2 \cdot (1 - b_1)]}$  and  $n_2 = 1$ .

Similarly, if  $b_2 > b_1$ ,  $C_s$  is minimum when  $n_2 = \frac{K_1 \cdot b_2}{[k_2 \cdot (1 - b_2)]}$  and  $n_1 = 1$ .

TABLE 2.2.1 : Indices of heterogeneity  $b_1$ ,  $b_2$  and  $b_s$  for the Jute data.

| Jute data<br>Variance<br>per |            |            |                      | JUTE DATA<br>VARIANCE<br>PER |             |            |            |
|------------------------------|------------|------------|----------------------|------------------------------|-------------|------------|------------|
| Shape                        | Unit area  | LOG(VAR)   | Plot<br>size         | SHAPE                        | UNIT AREA   | LOG(SIZE)  | LOG(VAR)   |
| 1X1                          | 1610.48    | 0          | 1                    | 1X1                          | 1610.48     | 0          | 0          |
| 1X2                          | 920.8691   | -0.55897   | 2                    | 2X1                          | 962.5602    | 0.6931472  | -0.5146909 |
| 1X3                          | 671.0709   | -0.87541   | 3                    | 3X1                          | 765.845     | 1.0986123  | -0.7433078 |
| 1X4                          | 439.9316   | -1.29767   | 4                    | 4X1                          | 605.5421    | 1.3862944  | -0.9781635 |
| 1X5                          | 410.6921   | -1.36644   | 5                    | 5X1                          | 596.9285    | 1.6094379  | -0.9924902 |
| 1X6                          | 388.6931   | -1.4215    | 6                    | 6X1                          | 574.6403    | 1.7917595  | -1.0305433 |
| 1X7                          | 450.4503   | -1.27404   | 7                    | 7X1                          | 557.7985    | 1.9459102  | -1.0602898 |
| 1X8                          | 322.0726   | -1.60951   | 8                    | 8X1                          | 442.6862    | 2.0794416  | -1.2914264 |
| 1X9                          | 271.0155   | -1.78211   | 9                    | 9X1                          | 443.9344    | 2.1972246  | -1.2886108 |
| Intercept=                   | -0.0498954 |            |                      | Intercept=                   | -0.08147225 |            |            |
| Slope=                       | -0.7605628 | $b_2=0.76$ |                      | Slope=                       | -0.55978509 | $b_1=0.56$ |            |
| Corr.<br>Coeff.              | -0.9761098 |            |                      | Corr.<br>Coeff.              | -0.98372046 |            |            |
|                              |            |            | Jute<br>Plot<br>size | Variance per                 |             |            |            |
|                              |            |            | SHAPE                | Unit area                    | LOG(SIZE)   | LOG(VAR)   |            |
|                              |            |            | 1                    | 1X1                          | 1610.48     | 0          | 0          |
|                              |            |            | 2                    | 2X2                          | 571.6053    | 0.6931472  | -1.0358388 |
|                              |            |            | 3                    | 3X3                          | 327.7126    | 1.0986123  | -1.5921506 |
|                              |            |            | 4                    | 4X4                          | 108.962     | 1.3862944  | -2.6932884 |
|                              |            |            | 5                    | 5X5                          | 160.3383    | 1.6094379  | -2.3070016 |
|                              |            |            | 6                    | 6X6                          | 178.9561    | 1.7917595  | -2.197147  |
|                              |            |            | 7                    | 7X7                          | 242.6505    | 1.9459102  | -1.8926654 |
|                              |            |            | 8                    | 8X8                          | 69.91666    | 2.0794416  | -3.1369836 |
|                              |            |            | 9                    | 9X9                          | 72.82381    | 2.1972246  | -3.0962446 |
|                              |            |            |                      | Intercept=                   | -0.16429954 |            |            |
|                              |            |            |                      | Slope=                       | -1.28674004 | $b_s=1.28$ |            |
|                              |            |            |                      | Corr.<br>Coeff.              | -0.91328668 |            |            |

TABLE 2.2.2 : Indices of heterogeneity  $b_1$ ,  $b_2$  and  $b_s$  for the rice data.

| Rice data    |              |            |           | Rice data    |              |            |          |
|--------------|--------------|------------|-----------|--------------|--------------|------------|----------|
| Shape        | Variance per |            | Plot size | Shape        | Variance per |            | Log(var) |
|              | Unit area    | Log(var)   |           |              | Unit area    | Log(size)  |          |
| 1X1          | 13988.38     | 2.161695   | 1         | 1X1          | 13988.38     | 0          | 2.161695 |
| 1X2          | 8884.711     | 1.7078     | 2         | 2X1          | 6837.279     | 0.693147   | 1.445858 |
| 1X3          | 6762.639     | 1.434881   | 3         | 3X1          | 4440.092     | 1.098612   | 1.014143 |
| 1X4          | 5994.299     | 1.314277   | 4         | 4X1          | 3360.674     | 1.386294   | 0.735609 |
| 1X5          | 4952.901     | 1.123441   | 5         | 5X1          | 2516.426     | 1.609438   | 0.446307 |
| 1X6          | 4254.933     | 0.971547   | 6         | 6X1          | 2215.581     | 1.791759   | 0.318982 |
| 1X7          | 3951.689     | 0.897611   | 7         | 7X1          | 2185.944     | 1.94591    | 0.305516 |
| 1X8          | 4218.14      | 0.962862   | 8         | 8X1          | 1404.229     | 2.079442   | -0.13704 |
| 1X9          | 3616.625     | 0.809009   | 9         | 9X1          | 1136.514     | 2.197225   | -0.34857 |
| Intercept=   | 2.1357619    |            |           | Intercept=   | 2.2010865    |            |          |
| Slope=       | -0.6123138   | $b_2=0.61$ |           | Slope=       | -1.0832265   | $b_1=1.08$ |          |
| Corr. Coeff. | -0.9936021   |            |           | Corr. Coeff. | -0.9910984   |            |          |
|              |              |            |           | Variance per |              |            |          |
|              |              |            | PLOT SIZE | SHAPE        | Unit area    | LOG(SIZE)  | LOG(VAR) |
|              |              |            | 1         | 1X1          | 13988.38     | 0          | 2.161695 |
|              |              |            | 2         | 2X2          | 5044.327     | 0.693147   | 1.141732 |
|              |              |            | 3         | 3X3          | 2320.853     | 1.098612   | 0.365403 |
|              |              |            | 4         | 4X4          | 2034.684     | 1.386294   | 0.233808 |
|              |              |            | 5         | 5X5          | 977.9386     | 1.609438   | -0.49884 |
|              |              |            | 6         | 6X6          | 684.1481     | 1.791759   | -0.85611 |
|              |              |            | 7         | 7X7          | 779.5499     | 1.94591    | -0.72557 |
|              |              |            | 8         | 8X8          | 322.25       | 2.079442   | -1.60896 |
|              |              |            | 9         | 9X9          | 308.7139     | 2.197225   | -1.65187 |
|              |              |            |           | Intercept=   | 2.3011417    |            |          |
|              |              |            |           | Slope=       | -1.730143    | $b_s=1.73$ |          |
|              |              |            |           | Corr. Coeff. | -0.985333    |            |          |

The above tables show the values of  $b_1$ ,  $b_2$  and  $b_s$  for the jute and rice data. The index heterogeneity is more pronounced along column than along row in case of Jute data. In Rice field the heterogeneity is nearly double along row than along column direction. The sum of  $b_1$  and  $b_2$  is close to  $b_s$  for both rice and jute data. Smith's  $b$  found for both rice and jute data is some sort average of  $b_1$  and  $b_2$ .

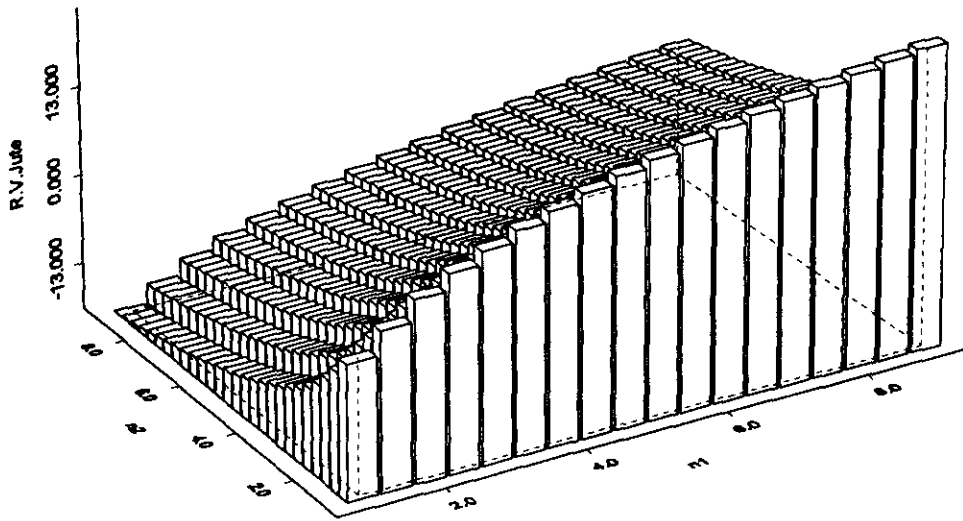


Fig. 2.2.1: Relative difference of variances R.V. as a function of plot shapes i.e. units along row and column directions  $n_1$  and  $n_2$  respectively for jute data.

The effect of plot shapes on the variance is shown in the fig.2.2.1 For Jute data the relative difference in variance increases i.e. efficiency decreases considerably as the number of units taken along row increases as compared to the number units taken along the column direction. In case of Rice data the efficiency decreases considerably as we increase the number of units along column direction as compared to the number units taken along the row direction.

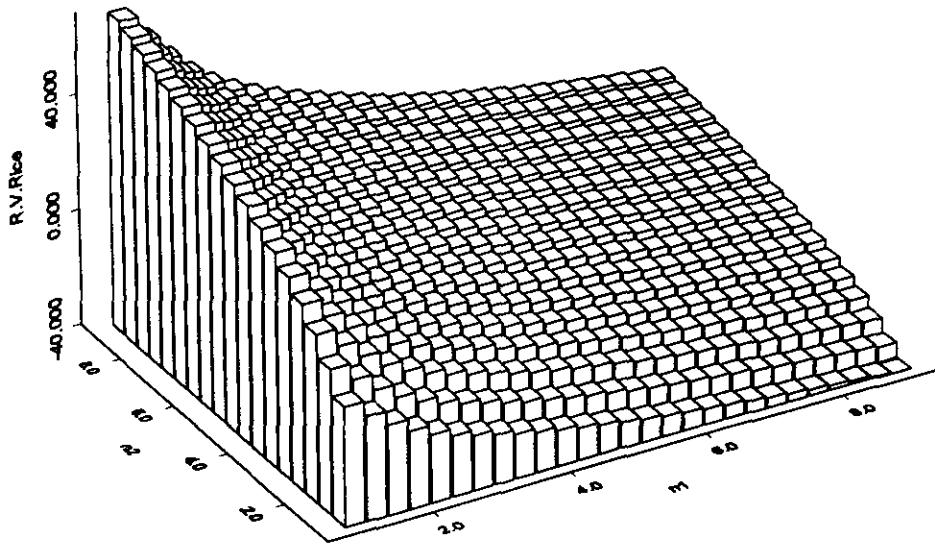
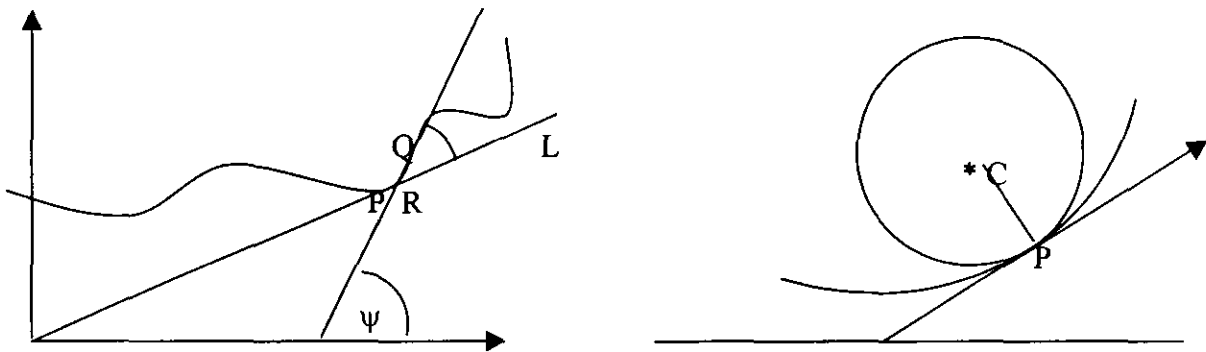


Fig. 2.2.2: Relative difference of variances R.V. as a function of plot shapes i.e. units along row and column directions  $n_1$  and  $n_2$  respectively for Rice data.

**2.3 Maximum curvature:** The method of maximum curvature is useful for determining optimum size and shape of plots in field experiments. Sethi (1985) suggested that Smith's law can be employed to relate C.V.(y) of a plot to its size(x) as  $y = a.x^{-b}$ . Now method of maximum curvature uses the general result of curvature of any curve. Let there be any curve AB on which PQ is any arch. We draw two tangent lines at P & Q respectively. Let  $\angle QRL = \Delta\psi$  where  $\Delta\psi$  is the



change in the inclination of the tangent line as the point of contact of the tangent line describes the arc  $PQ = \Delta S$ . Here,  $\frac{\Delta\Psi}{\Delta S}$  is called the average curvature of the arch PQ. When  $Q \rightarrow P$  (from

either side) along the curve, as a limiting position curvature at P is  $\lim_{\Delta S \rightarrow 0} \frac{\Delta\Psi}{\Delta S} = \frac{d\Psi}{dS}$ . Thus

curvature is the rate of change of direction of the curve with respect to the arc or roughly the curvature is the “rate at which the curve curves”. The reciprocal of the curvature at any point P is called the radius of curvature at P and it is denoted as  $\frac{dS}{d\Psi}$ . If a length PC is measured from P

along the positive direction of the normal, the point C is called the centre of curvature at P and the circle with centre C and radius CP (i.e.  $\rho$ ) is called the circle of curvature at P. Any chord of this circle through the point of contact is called a chord of curvature. The line PC which makes an angle  $+90^\circ$  with the positive direction of the tangent (i.e. the direction in which S increases) is called the positive direction of the normal at P.  $\rho$  is +ve or -ve according to C is on the +ve or -

ve side of the normal. For  $y = f(x)$   $\frac{dy}{dx} = \tan(\Psi)$  and

$$\frac{d^2 y}{dx^2} = \text{Sec}^2 \Psi \cdot \frac{d\Psi}{dx} = \text{Sec}^2 \Psi \cdot \frac{d\Psi}{ds} \cdot \frac{ds}{dx} = \text{Sec}^3 \Psi \cdot \frac{d\Psi}{ds}. \text{ As we see that } \left[ \frac{ds}{dx} = \text{Sec} \Psi \right]. \text{ Hence } \rho =$$

$$\frac{ds}{d\Psi} = \frac{\text{Sec}^3 \Psi}{\frac{d^2 y}{dx^2}}. \text{ Since } \text{Sec} \Psi = (1 + \tan^2 \Psi)^{1/2} \text{ we can write that } \text{Sec} \Psi = \left\{ 1 + \left( \frac{dy}{dx} \right)^2 \right\}^{1/2}. \text{ Finally}$$

$$\rho = \frac{\left\{ 1 + \left( \frac{dy}{dx} \right)^2 \right\}^{3/2}}{\frac{d^2 y}{dx^2}} = \frac{(1 + y_1^2)^{3/2}}{y_2}. \rho \text{ is +ve or -ve accordingly as } y_2 \text{ is +ve or -ve. If we denote it}$$

by  $\rho$  then  $\rho = \frac{(1 + y_1^2)^{3/2}}{y_2}$  where  $y_1 = \frac{dy}{dx}$  and  $y_2 = \frac{d^2 y}{dx^2}$ . Now using the property of maxima

minima we have  $\frac{d\rho}{dx} = 0$  or,  $\frac{d}{dx} \left\{ \frac{(1 + y_1^2)^{3/2}}{y_2} \right\} = 0$  which gives rise to the following equation:-

$$3 \cdot y_1 \cdot y_2^2 - y_1^2 \cdot y_3 - y_3 = 0 \quad \text{where} \quad y_1 = -a \cdot b \cdot x^{-(1+b)}, \quad y_2 = a \cdot b \cdot (1+b) \cdot x^{-(2+b)},$$

$y_3 = -a.b.(1+b).(2+b).x^{-(3+b)}$ . Putting the values and solving for x gives

$$x_{opt} = \left\{ \frac{a^2.b^2.(1+2.b)}{(2+b)} \right\}^{\frac{1}{2.(1+b)}}$$

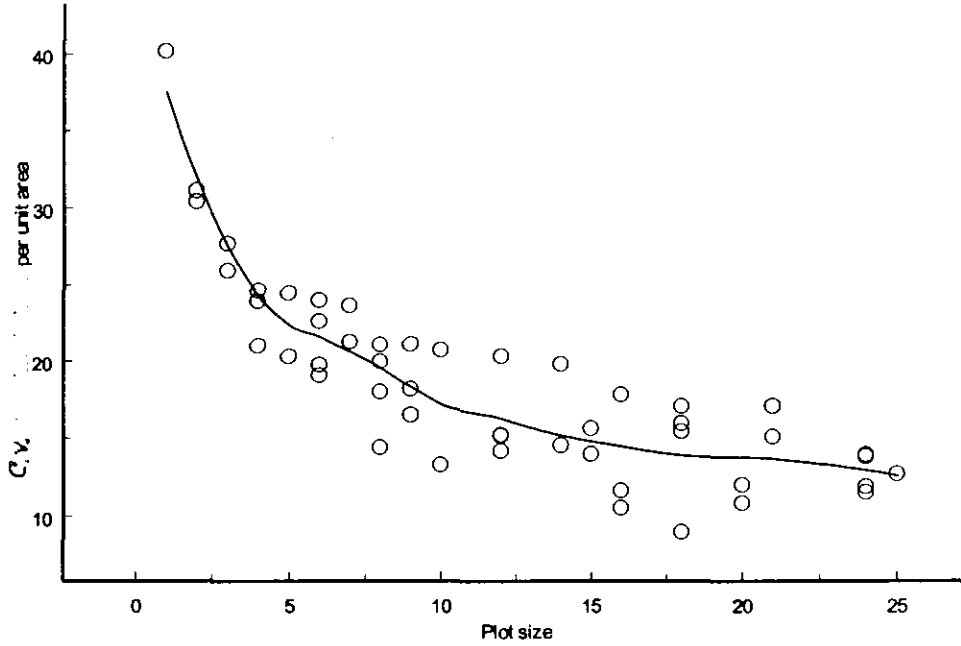


Fig.2.3.1: Smoothing Loess plot of C.V. as a function of plot size for Jute data.

Once the optimum plot size is determined, the choice of *plot shape* is governed by the following considerations. Long and narrow plots should be used for areas with distinct fertility gradient, with the length of the plot parallel to the fertility gradient of the field. When the fertility pattern of the field is spotty or not known plots should be as square as possible. For determining optimum shape of plots  $y$  was further related to  $x$  as  $y = a'.x_1^{-b_1}.x_2^{-b_2}$  where  $x_1$  and  $x_2$  denote the number of units combined in row (E →W) and column (N→S) directions respectively, to make a plot of size  $x$ . Now the value of  $x_2$  (say  $x_{02}$ ) which conditionally

maximizes curvature of  $y$  at a fixed  $x_1$  is given by  $x_{02} = \left\{ \frac{b_2^2.c_1^2.(1+2.b_2)}{(2+b_2)} \right\}^{\frac{1}{2.(1+b_2)}}$  where

$c_1 = a'.x_1^{-b_1}$ . The conditional maxima of  $x_1$  at a fixed  $x_2$  was similarly obtained. Now  $x_{02}$  was expressed as a function of  $x_1$  as  $x_{02} = d.x_1^{-e}$ . The above function was solved for the values

of  $x_1$  (say  $x_{1opt}$ ) and  $x_2$  (say  $x_{2opt}$ ) under the constraint  $x_{opt} = x_{1opt} \cdot x_{2opt}$  thereby providing optimum dimensions of the plot of size  $x_{opt}$ . The unknown parameters  $a$ ,  $b$  are estimated through regression analysis. The goodness of a fitted function is indicated by the closeness of a statistic  $\phi$ ,

given by  $\phi = 1 - \frac{\sum_{i=1}^n (y_i - \hat{y}_i)^2}{\sum_{i=1}^n (y_i - \bar{y})^2}$  to 1, where  $\hat{y}_i$  is the estimate of an observed  $y_i$  from the function

$$\text{and } \bar{y} = \frac{1}{n} \sum_{i=1}^n y_i .$$

**Maximum curvature: Jute data:** The pooled values of C.V. decreases with an increases in plot size. The relation  $y = a x^{-b}$  in estimated form was  $y = 40.2 x^{-0.38}$  with  $\phi = 0.98$ , thus indicating a good fit. From relation 2 it was found that  $x_{opt} = 6.5$  units i.e.  $X_{opt} = 7$  sq. m. when units plots were 1 m. x 1 m. Model 3 i.e.  $y = a' \cdot x_1^{b_1} \cdot x_2^{b_2}$  applied to C. V. data resulted in  $y = 40.2 x_1^{-0.31} \cdot x_2^{-0.45}$ , which too was a good fit since  $\phi = 0.987$ . The relative magnitude of  $b_1$  and  $b_2$  again indicate the C.V values to expectedly fall at a higher rate as the plot size was increased along length along width of the Jute field. For attaining  $x_2 > x_1$  with  $x_1 x_2 = 6.5$  it is sufficient to evaluate conditional maxima of  $x_2$  at different  $x_1$  ,s which be possibly due to  $b_2 > b_1$ . The equation  $x_{02} = 6.75 x_1^{-0.21}$  gave an excellent fit to the underlying relationship between  $x_{02}$  &  $x_1$ . its solution provided  $x_{1opt} = 1.122$  m.,  $x_{2opt} = 5.762$  m. meaning thereby that the optimum plot size was 7 sq. m. with 1.12 m. along the width and 5.76 m. along the length of the Jute field.

**Rice data:** The pooled values of C.V. decreases with an increases in plot size. The relation  $y = a x^{-b}$  in estimated form was  $y = 139.86 x^{-0.48}$  with  $\phi = 0.96$ , thus indicating a good fit. From relation 2 it was found that  $x_{opt} = 15.86$  mt.<sup>2</sup> when units plots were 1 mt x 1 mt. model 3 i.e.  $y = a' \cdot x_1^{b_1} \cdot x_2^{b_2}$  applied to C. V. data resulted in  $y = 139.87 x_1^{-0.63} x_2^{-0.32}$  which too was a good fit since  $\phi = 0.96$  the relative magnitude of  $b_1$  and  $b_2$  again indicate the C.V values to expectedly fall at a higher rate as the plot size was increased along width than along length of the Rice field. For attaining  $x_1 > x_2$  with  $x_1 \cdot x_2 = 15.86$ . it is sufficient to evaluate conditional maxima of  $x_1$  at different  $x_2$ 's which be possibly due to  $b_1 > b_2$ . The equation  $x_{01} = 14.87 \cdot x_2^{-0.196}$  gave an excellent fit to the underlying relationship between  $x_{01}$  &  $x_2$ . Its solution provided  $x_{1opt} = 7.842$

mt.  $x_{2opt} = 2.022$  mt. meaning thereby that the optimum plot size was 15.86 sq. mt. with 7.842 mt. along width and 2.022 mt. along length of the Rice field.

**2.4 Block size:** Block size is governed by the plot size chosen, the number of treatments tested and the experimental design used. The primary objective in choosing the shape of blocks is to reduce the differences in productivity levels among plots within a block so that most of the soil variability in the experimental area is accounted for by variability between blocks. Information on the pattern of soil heterogeneity in the area is helpful in making this choice. When the fertility pattern of the area is known, orient the blocks so that soil differences between blocks are maximized and those within the same block are minimized. For example, in an area with a unidirectional fertility gradient, the length of the block should be oriented perpendicular to the direction of the fertility gradient. In an area with bidirectional fertility gradient a row-column design is appropriate. On the other hand, when the fertility pattern of the area is spotty or is not known to the researcher blocks should be kept as compact or as nearly square as possible. Again block size, for most experimental designs, increases proportionately with the number of treatments and because it is difficult to maintain homogeneity in large blocks, a researcher must also be concerned with the number of treatments. If the number of treatments is so large that uniform area within a block can not be attained, incomplete block designs may be used.

To find out the size and shape of plots and blocks that will give the maximum accuracy for the mean with a given amount of experimental area, it is necessary to have a knowledge of the probable magnitude of the coefficient of variation for different sizes and shapes of the plots and blocks. This information is generally obtained from the data of a uniformity trial. In India earlier such studies have been made by Hutchinson and Panse (1935) for cotton, Ghose and Sanyal (1945) for jute and by a large number of workers for sugarcane and wheat. Similar work on rice has been done by Bose et al (1936), Narasinga Rao (1937), Abraham et al (1964).

In our work both the crops (rice and jute) are harvested in contiguous units of 1mt. X 1mt. Plots of various sizes are obtained by combining the units along North-South and West-East directions. The plots are grouped into blocks of 2 to 12 plots as found feasible for our data. Plots are grouped both in North-South and West-East directions separately. The coefficient

of variation (C.V.) for each arrangement is calculated separately and the optimum size and shape of the plots and their arrangement in blocks are found out on the basis of observed C.V.

RESULT: *Optimum block size and shape:* For Jute data Table 2.4.1 & 2.4.2 give the C.V. for the different size and shapes of plots after arranging them into blocks of 3 to 12 plots some of the combinations of the plot sizes and blocks are not possible. The blanks in Table correspond to such combinations.

For Jute data C.V. in general decreased with increase in plot size in either direction, the decrease being greater when the larger dimension is in N→S direction and when the blocks run E→W direction. The reduction in C.V. with increased plot size is comparatively less when the increase in plot size was beyond 6 units or 6 mt. along E→W direction. For optimum plot size of 2mt.X5mt. the 9 plot blocks give lowest C.V. than 3 plot blocks and 6 plot and 12 plot blocks. However when blocks run in N→S direction the decrease in C.V. with increase in plot size is more or less equal in both directions. The 12 plot blocks gave a higher C.V. than the 6 plot blocks with larger plots. The decrease in C.V. is reasonably greater when blocks run E→W direction than when blocks run N→S direction.

EFFECT OF PLOT SHAPE ON VARIABILITY: In general plots elongated along N→S direction showed less variability than plots elongated along E→W direction. Compact or square plots in general showed slightly less or approximately equal variability than plots elongated in N→S direction. However, plots elongated along E→W direction are more variable than square plots.

TABLE 2.4.1: (Jute data) Within block C.V. for different plot sizes when blocks run row (E→W) direction

3 plot blocks:

| row | no. of units along column(N→S) direction |      |      |      |             |      |      |             |             |
|-----|--|------|------|------|-------------|------|------|-------------|-------------|
| E→W | 1  | 2    | 3    | 4    | 5           | 6    | 7    | 8           | 9           |
| 1   | 10.62                                    | 7.50 | 6.91 | 5.67 | 5.52        | 4.86 | 5.16 | 4.55        | 4.67        |
| 2   | 7.35                                     | 4.92 | 4.05 | 3.10 | 2.41        | 3.08 | 2.70 | <b>1.75</b> | <b>1.60</b> |
| 3   | 6.62                                     | 5.41 | 4.52 | 3.59 | 3.65        | 4.16 | 4.89 | 3.71        | 3.13        |
| 4   | 6.14                                     | 4.71 | 3.15 | 2.98 | 2.29        | 2.53 | 2.78 | 2.64        | <b>2.12</b> |
| 5   | 6.68                                     | 5.72 | 4.69 | 3.37 | 3.59        | 3.83 | 3.81 | 3.11        | 2.30        |
| 6   | 5.26                                     | 4.40 | 2.75 | 2.89 | 2.26        | 2.30 |      |             |             |
| 7   | 5.26                                     | 4.18 | 2.87 | 2.39 | 2.17        | 2.19 |      |             |             |
| 8   | 5.04                                     | 4.14 | 2.87 | 2.53 | <b>1.52</b> | 2.29 |      |             |             |
| 9   | 5.81                                     | 4.51 | 3.99 | 3.52 | 2.69        | 3.31 |      |             |             |

of variation (C.V.) for each arrangement is calculated separately and the optimum size and shape of the plots and their arrangement in blocks are found out on the basis of observed C.V.

RESULT: *Optimum block size and shape:* For Jute data Table 2.4.1 & 2.4.2 give the C.V. for the different size and shapes of plots after arranging them into blocks of 3 to 12 plots some of the combinations of the plot sizes and blocks are not possible. The blanks in Table correspond to such combinations.

For Jute data C.V. in general decreased with increase in plot size in either direction, the decrease being greater when the larger dimension is in N→S direction and when the blocks run E→W direction. The reduction in C.V. with increased plot size is comparatively less when the increase in plot size was beyond 6 units or 6 mt. along E→W direction. For optimum plot size of 2mt.X5mt. the 9 plot blocks give lowest C.V. than 3 plot blocks and 6 plot and 12 plot blocks. However when blocks run in N→S direction the decrease in C.V. with increase in plot size is more or less equal in both directions. The 12 plot blocks gave a higher C.V. than the 6 plot blocks with larger plots. The decrease in C.V. is reasonably greater when blocks run E→W direction than when blocks run N→S direction.

EFFECT OF PLOT SHAPE ON VARIABILITY: In general plots elongated along N→S direction showed less variability than plots elongated along E→W direction. Compact or square plots in general showed slightly less or approximately equal variability than plots elongated in N→S direction. However, plots elongated along E→W direction are more variable than square plots.

TABLE 2.4.1: (Jute data) Within block C.V. for different plot sizes when blocks run row (E→W) direction

*3 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |             |      |      |             |             |
|-----|--|------|------|------|-------------|------|------|-------------|-------------|
| E→W | 1  | 2    | 3    | 4    | 5           | 6    | 7    | 8           | 9           |
| 1   | 10.62                                    | 7.50 | 6.91 | 5.67 | 5.52        | 4.86 | 5.16 | 4.55        | 4.67        |
| 2   | 7.35                                     | 4.92 | 4.05 | 3.10 | 2.41        | 3.08 | 2.70 | <b>1.75</b> | <b>1.60</b> |
| 3   | 6.62                                     | 5.41 | 4.52 | 3.59 | 3.65        | 4.16 | 4.89 | 3.71        | 3.13        |
| 4   | 6.14                                     | 4.71 | 3.15 | 2.98 | 2.29        | 2.53 | 2.78 | 2.64        | <b>2.12</b> |
| 5   | 6.68                                     | 5.72 | 4.69 | 3.37 | 3.59        | 3.83 | 3.81 | 3.11        | 2.30        |
| 6   | 5.26                                     | 4.40 | 2.75 | 2.89 | 2.26        | 2.30 |      |             |             |
| 7   | 5.26                                     | 4.18 | 2.87 | 2.39 | 2.17        | 2.19 |      |             |             |
| 8   | 5.04                                     | 4.14 | 2.87 | 2.53 | <b>1.52</b> | 2.29 |      |             |             |
| 9   | 5.81                                     | 4.51 | 3.99 | 3.52 | 2.69        | 3.31 |      |             |             |

*4 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |             |
|-----|--|------|------|------|------|------|------|------|-------------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9           |
| 1   | 11.49                                    | 8.31 | 7.62 | 6.58 | 6.15 | 5.83 | 6.38 | 5.44 | 5.23        |
| 2   | 8.29                                     | 5.88 | 4.83 | 4.05 | 3.36 | 4.06 | 3.88 | 3.09 | 2.30        |
| 3   | 7.76                                     | 5.84 | 4.85 | 4.37 | 3.73 | 4.32 | 4.92 | 4.05 | 3.40        |
| 4   | 6.83                                     | 5.47 | 4.33 | 2.69 | 2.96 | 3.15 | 3.18 | 2.49 | <b>1.94</b> |
| 5   | 6.00                                     | 4.79 | 3.17 | 2.90 | 2.58 | 2.86 |      |      |             |
| 6   | 6.42                                     | 5.15 | 3.94 | 3.73 | 2.91 | 3.56 |      |      |             |
| 7   | 7.04                                     | 5.75 | 5.20 | 4.16 | 3.77 | 4.28 |      |      |             |
| 8   | 6.27                                     | 5.30 | 4.76 | 3.13 | 2.95 | 3.53 |      |      |             |

*5 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |             |             |      |      |             |
|-----|--|------|------|------|-------------|-------------|------|------|-------------|
| E→W | 1  | 2    | 3    | 4    | 5           | 6           | 7    | 8    | 9           |
| 1   | 11.63                                    | 8.21 | 7.69 | 6.30 | 5.94        | 5.65        | 6.20 | 5.23 | 5.23        |
| 2   | 8.82                                     | 6.45 | 5.20 | 4.01 | 3.42        | 4.08        | 3.23 | 2.29 | <b>1.79</b> |
| 3   | 8.18                                     | 6.62 | 5.78 | 4.35 | 4.20        | 4.79        | 5.14 | 4.03 | 3.29        |
| 4   | 6.01                                     | 4.80 | 2.90 | 2.43 | <b>1.99</b> | <b>2.18</b> |      |      |             |
| 5   | 6.92                                     | 5.52 | 4.27 | 4.08 | 3.54        | 3.93        |      |      |             |
| 6   | 7.40                                     | 6.21 | 5.57 | 4.11 | 3.89        | 4.58        |      |      |             |

*6 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |             |             |      |      |      |
|-----|--|------|------|------|-------------|-------------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5           | 6           | 7    | 8    | 9    |
| 1   | 11.76                                    | 8.36 | 7.63 | 6.35 | 6.09        | 5.65        | 6.36 | 5.39 | 5.36 |
| 2   | 9.33                                     | 6.77 | 5.33 | 4.63 | 3.63        | 4.42        | 4.22 | 3.44 | 2.70 |
| 3   | 7.06                                     | 5.09 | 3.64 | 3.32 | <b>2.62</b> | <b>2.89</b> |      |      |      |
| 4   | 6.74                                     | 5.29 | 3.62 | 3.28 | <b>2.64</b> | 3.09        |      |      |      |
| 5   | 7.61                                     | 6.41 | 5.48 | 4.19 | 4.12        | 4.57        |      |      |      |

*7 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |             |             |
|-----|--|------|------|------|------|------|------|-------------|-------------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8           | 9           |
| 1   | 11.79                                    | 8.53 | 7.62 | 6.33 | 5.89 | 5.65 | 5.91 | 5.02        | 4.93        |
| 2   | 9.64                                     | 7.28 | 6.16 | 4.64 | 3.86 | 4.72 | 4.48 | <b>3.40</b> | <b>2.52</b> |
| 3   | 7.51                                     | 5.65 | 4.29 | 3.54 | 2.83 | 3.66 |      |             |             |
| 4   | 7.63                                     | 6.10 | 5.15 | 3.75 | 3.27 | 3.90 |      |             |             |

*8 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |             |             |
|-----|--|------|------|------|------|------|------|-------------|-------------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8           | 9           |
| 1   | 12.40                                    | 8.97 | 7.99 | 6.86 | 6.44 | 6.13 | 6.81 | 5.83        | 5.46        |
| 2   | 9.68                                     | 7.29 | 6.02 | 4.46 | 4.06 | 4.77 | 4.42 | <b>3.38</b> | <b>2.57</b> |
| 3   | 8.25                                     | 6.31 | 5.17 | 4.59 | 3.95 | 4.67 |      |             |             |
| 4   | 7.81                                     | 6.28 | 5.34 | 3.68 | 3.50 | 4.02 |      |             |             |

*9 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 12.16                                    | 9.15 | 7.87 | 6.57 | 6.57 | 6.41 | 7.01 | 5.70 | 5.36 |
| 2   | 9.13                                     | 6.69 | 4.95 | 4.23 | 3.30 | 3.87 |      |      |      |
| 3   | 8.81                                     | 7.04 | 6.03 | 5.03 | 4.53 | 5.32 |      |      |      |

*10 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 12.73                                    | 9.35 | 8.30 | 6.84 | 6.56 | 6.25 | 6.60 | 5.59 | 5.42 |
| 2   | 9.28                                     | 6.88 | 5.42 | 4.51 | 3.55 | 4.44 |      |      |      |
| 3   | 8.95                                     | 7.23 | 6.44 | 5.01 | 4.66 | 5.41 |      |      |      |

*11 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 12.03                                    | 8.88 | 7.66 | 6.58 | 5.97 | 6.07 | 6.16 | 4.91 | 4.71 |
| 2   | 9.29                                     | 7.01 | 5.46 | 4.57 | 3.54 | 4.52 |      |      |      |

*12 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 12.56                                    | 9.19 | 7.93 | 6.75 | 6.20 | 6.32 | 6.68 | 5.44 | 5.06 |
| 2   | 9.74                                     | 7.19 | 5.62 | 4.83 | 3.86 | 4.76 |      |      |      |

TABLE 2.4.2: (Jute data) Within block C.V. for different plots when blocks run column (N→S) direction.

*3 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |
|-----|--|------|------|------|
| E→W | 1  | 2    | 3    | 4    |
| 1   | 11.10                                    | 8.36 | 6.98 | 5.33 |
| 2   | 8.88                                     | 6.72 | 5.42 | 3.68 |
| 3   | 7.58                                     | 6.02 | 5.18 | 3.20 |
| 4   | 7.02                                     | 5.89 | 4.36 | 2.07 |
| 5   | 6.83                                     | 5.79 | 4.81 | 2.66 |
| 6   | 6.52                                     | 5.55 | 4.52 | 2.50 |
| 7   | 6.58                                     | 5.46 | 3.57 | 2.10 |
| 8   | 5.78                                     | 5.20 | 4.09 | 1.73 |
| 9   | 6.25                                     | 4.88 | 2.23 | 1.25 |

*4 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |
|-----|--|------|------|
| E→W | 1  | 2    | 3    |
| 1   | 12.39                                    | 8.35 | 7.66 |
| 2   | 9.96                                     | 6.65 | 5.82 |
| 3   | 8.60                                     | 6.49 | 5.17 |
| 4   | 8.05                                     | 5.57 | 4.45 |
| 5   | 7.70                                     | 6.04 | 4.44 |
| 6   | 7.54                                     | 5.60 | 4.53 |
| 7   | 7.33                                     | 5.01 | 3.85 |
| 8   | 6.84                                     | 5.21 | 4.05 |
| 9   | 6.61                                     | 3.74 | 2.49 |

| row | <i>5 plot</i>                            |      | <i>6 plot blocks</i> |      |
|-----|--|------|----------------------|------|
|     | no. of units along column(N→S) direction |      |                      |      |
| E→W | 1  | 2    | 1                    | 2    |
| 1   | 12.28                                    | 8.95 | 12.66                | 9.56 |
| 2   | 9.52                                     | 7.14 | 9.82                 | 7.83 |
| 3   | 8.4                                      | 6.95 | 8.37                 | 7.11 |
| 4   | 7.49                                     | 5.95 | 7.89                 | 6.45 |
| 5   | 7.14                                     | 6.49 | 7.48                 | 6.62 |
| 6   | 7.01                                     | 6.18 | 7.27                 | 6.41 |
| 7   | 6.82                                     | 5.59 | 7.22                 | 5.98 |
| 8   | 6.28                                     | 5.26 | 6.65                 | 5.71 |
| 9   | 6.14                                     | 4.37 | 6.67                 | 4.95 |

| row | <i>7 plot</i>                           | <i>8 plot</i> | <i>9 plot</i> | <i>10 plot</i> | <i>11 plot</i> | <i>12 plot blocks</i> |
|-----|---|---------------|---------------|----------------|----------------|-----------------------|
|     | single unit along column(N→S) direction |               |               |                |                |                       |
| 1   | 11.83                                   | 12.21         | 12.2          | 13.07          | 13.18          | 13.48                 |
| 2   | 9.07                                    | 9.52          | 9.61          | 10.11          | 10.35          | 10.61                 |
| 3   | 7.94                                    | 8.39          | 8.51          | 9              | 9              | 9.18                  |
| 4   | 7.21                                    | 7.33          | 7.41          | 7.93           | 8.01           | 8.31                  |
| 5   | 6.87                                    | 7.23          | 7.44          | 7.85           | 7.86           | 8.14                  |
| 6   | 6.61                                    | 6.71          | 6.97          | 7.64           | 7.73           | 7.94                  |
| 7   | 6.09                                    | 6.14          | 6.3           | 7.18           | 7.29           | 7.62                  |
| 8   | 6.11                                    | 6.3           | 6.14          | 6.7            | 6.82           | 7.06                  |
| 9   | 5.34                                    | 5.17          | 5.36          | 6.22           | 6.39           | 6.73                  |

**BLOCK EFFICIENCY:** For investigating the influence of size and shape of plots and blocks on block efficiency 24 units along E→W and 18 units along N→S are taken to have as many convenient combinations as possible.

If  $V_B$  denotes variance with blocks &  $V$  the variance without block restriction, the efficiency of block is defined as  $\frac{V}{V_B}$ . For selected plot sizes & shapes, block efficiencies for various number of

plots per block are given in Table 5 & 6

From the following Table 2.4.3 for Jute data we see that with blocks of same size but different shapes formed from plots of the same size, there was detectable change in blocking efficiency. As in general for all plot sizes & shapes blocks running E→W showed higher blocking efficiency than the blocks running in N→S direction. The highest blocking efficiency value 5.71 was found for 3 plot blocks containing plots of size 16 sq. mt. & shape 2 x 8 (i.e. 2 mt. in E→W & 8 mt in N→S direction). For the same B.E. block size was 48 sq. mt. & shape was 3 : 4 (i.e. 6 mt. in E→W direction & 8 mt. in N→S direction). The second highest blocking efficiency was 4.05 was found for 3 plot blocks containing plot of size 18 sq. mt. & shape 2 :9 (i.e. 2 mt. in E→W direction & 9 mt. in N→S direction). For the same B.E. block size was 54 sq. mt. & block shape was 2 : 3 (i.e. 6 mt. in E→W direction & 9 mt. in N→S direction).

TABLE 2.4.3: (Jute data) Blocking Efficiencies when blocks run row(E->W) direction

*3 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |             |             |
|-----|--|------|------|------|------|------|------|-------------|-------------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8           | 9           |
| 1   | 1.88                                     | 2.16 | 1.87 | 1.79 | 1.77 | 2.24 | 2.28 | 2.10        | 1.68        |
| 2   | 2.37                                     | 3.14 | 2.91 | 2.78 | 3.93 | 3.21 | 3.77 | <b>5.71</b> | <b>4.05</b> |
| 3   | 2.28                                     | 2.21 | 1.83 | 1.96 | 1.59 | 1.67 | 1.48 | 1.78        | 1.64        |
| 4   | 1.89                                     | 2.00 | 1.65 | 1.22 | 1.35 | 1.79 | 1.10 | 1.20        | 1.23        |
| 5   | 1.72                                     | 1.66 | 1.38 | 1.56 | 1.46 | 1.43 | 1.53 | 1.67        | 1.73        |
| 6   | 1.87                                     | 1.46 | 1.40 | 1.04 | 1.18 | 1.06 |      |             |             |
| 7   | 2.00                                     | 1.90 | 1.51 | 1.01 | 1.03 | 1.49 |      |             |             |
| 8   | 2.02                                     | 1.96 | 1.39 | 1.00 | 1.05 | 1.37 |      |             |             |
| 9   | 1.66                                     | 1.74 | 1.07 | 1.00 | 1.09 | 1.06 |      |             |             |

*4 plot blocks:*

| row | no. of units along column(N→S) direction |             |      |      |      |      |      |      |      |
|-----|--|-------------|------|------|------|------|------|------|------|
| E→W | 1  | 2           | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.60                                     | 1.74        | 1.50 | 1.32 | 1.37 | 1.48 | 1.40 | 1.38 | 1.25 |
| 2   | 1.83                                     | <b>2.15</b> | 2.00 | 1.61 | 1.92 | 1.76 | 1.71 | 1.72 | 1.83 |
| 3   | 1.56                                     | 1.65        | 1.27 | 1.10 | 1.13 | 1.27 | 1.03 | 1.08 | 1.09 |
| 4   | 1.68                                     | 1.70        | 1.56 | 1.89 | 1.60 | 1.63 | 1.62 | 1.81 | 1.82 |
| 5   | 1.65                                     | 1.51        | 1.34 | 1.01 | 1.03 | 1.20 |      |      |      |
| 6   | 1.63                                     | 1.62        | 1.21 | 1.00 | 1.01 | 1.15 |      |      |      |
| 7   | 1.43                                     | 1.48        | 1.02 | 1.00 | 1.06 | 1.03 |      |      |      |
| 8   | 1.44                                     | 1.41        | 1.03 | 1.01 | 1.20 | 1.01 |      |      |      |

*5 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.57                                     | 1.81 | 1.51 | 1.45 | 1.53 | 1.66 | 1.58 | 1.59 | 1.34 |
| 2   | 1.64                                     | 1.83 | 1.77 | 1.65 | 1.94 | 1.83 | 2.63 | 3.32 | 3.22 |
| 3   | 1.48                                     | 1.50 | 1.25 | 1.34 | 1.34 | 1.28 | 1.29 | 1.40 | 1.36 |
| 4   | 1.65                                     | 1.50 | 1.40 | 1.02 | 1.05 | 1.34 |      |      |      |
| 5   | 1.48                                     | 1.52 | 1.14 | 1.00 | 1.01 | 1.10 |      |      |      |
| 6   | 1.35                                     | 1.35 | 1.01 | 1.01 | 1.12 | 1.00 |      |      |      |

*6 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.53                                     | 1.74 | 1.54 | 1.42 | 1.46 | 1.66 | 1.50 | 1.50 | 1.27 |
| 2   | 1.39                                     | 1.49 | 1.23 | 1.09 | 1.14 | 1.26 | 1.04 | 1.12 | 1.14 |
| 3   | 1.49                                     | 1.35 | 1.23 | 1.03 | 1.13 | 1.04 |      |      |      |
| 4   | 1.57                                     | 1.59 | 1.25 | 1.00 | 1.02 | 1.20 |      |      |      |
| 5   | 1.33                                     | 1.32 | 1.01 | 1.01 | 1.11 | 1.00 |      |      |      |

*7 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.51                                     | 1.67 | 1.48 | 1.43 | 1.43 | 1.59 | 1.67 | 1.67 | 1.44 |
| 2   | 1.36                                     | 1.42 | 1.16 | 1.22 | 1.25 | 1.24 | 1.25 | 1.38 | 1.42 |
| 3   | 1.49                                     | 1.49 | 1.23 | 1.00 | 1.02 | 1.18 |      |      |      |
| 4   | 1.37                                     | 1.42 | 1.03 | 1.00 | 1.08 | 1.04 |      |      |      |

*8 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.37                                     | 1.49 | 1.37 | 1.21 | 1.25 | 1.33 | 1.23 | 1.20 | 1.15 |
| 2   | 1.34                                     | 1.39 | 1.29 | 1.32 | 1.32 | 1.28 | 1.32 | 1.44 | 1.47 |
| 3   | 1.38                                     | 1.41 | 1.12 | 1.00 | 1.01 | 1.09 |      |      |      |
| 4   | 1.29                                     | 1.29 | 1.03 | 1.01 | 1.14 | 1.00 |      |      |      |

*9 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.38                                     | 1.42 | 1.27 | 1.29 | 1.18 | 1.28 | 1.23 | 1.33 | 1.22 |
| 2   | 1.29                                     | 1.20 | 1.12 | 1.02 | 1.08 | 1.02 |      |      |      |
| 3   | 1.29                                     | 1.30 | 1.03 | 1.00 | 1.03 | 1.02 |      |      |      |

*10 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.31                                     | 1.40 | 1.30 | 1.23 | 1.26 | 1.36 | 1.39 | 1.39 | 1.24 |
| 2   | 1.27                                     | 1.24 | 1.12 | 1.00 | 1.02 | 1.08 |      |      |      |
| 3   | 1.24                                     | 1.26 | 1.01 | 1.01 | 1.08 | 1.00 |      |      |      |

11 plot blocks:

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.27                                     | 1.31 | 1.13 | 1.01 | 1.02 | 1.12 | 1.00 | 1.01 | 1.01 |
| 2   | 1.33                                     | 1.32 | 1.12 | 1.00 | 1.02 | 1.10 |      |      |      |

12 plot blocks:

| row | no. of units along column(N→S) direction |      |      |      |      |      |      |      |      |
|-----|--|------|------|------|------|------|------|------|------|
| E→W | 1  | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1   | 1.21                                     | 1.26 | 1.10 | 1.04 | 1.05 | 1.13 | 1.02 | 1.05 | 1.04 |
| 2   | 1.27                                     | 1.32 | 1.10 | 1.00 | 1.01 | 1.08 |      |      |      |

For Rice data C.V.(TABLE 2.4.4 & 2.4.5) in general decreased with increase in plot size in either direction, the decrease being greater when the larger plot dimension is in E→W direction and when the blocks run N→S direction. The reduction in C.V. with increased plot size is comparatively less when the increase in plot size was beyond 6 units or 6 mt. along E→W direction. For optimum plot size of 8mt. X 2mt. the 5 plot blocks give lowest C.V. than 3 plot blocks and 6 plot and 12 plot blocks. However when blocks run in E→W direction the decrease in C.V. with increase in plot size is more in E→W directions. The decrease in C.V. is reasonably greater when blocks run N→S direction than when blocks run E→W direction.

EFFECT OF PLOT SHAPE ON VARIABILITY: Plots elongated along N→S direction showed less variability than plots elongated along E→W direction. Compact or square plots in general showed slightly less variability than plots elongated in N→S direction. However, plots elongated along E→W direction are more variable than square plots.

TABLE 2.4.4: (Rice data) C.V. for different plots when blocks run row(E->W) direction

3 plot blocks:

| row  | no. of units along column(N->S) direction |      |      |      |      |      |      |      |      |
|------|---|------|------|------|------|------|------|------|------|
| E->W | 1   | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 11.70                                     | 9.21 | 7.92 | 7.31 | 6.26 | 6.01 | 5.64 | 5.85 | 5.11 |
| 2    | 8.25                                      | 7.12 | 6.38 | 6.17 | 6.03 | 5.45 | 5.81 | 5.38 | 4.87 |
| 3    | 6.96                                      | 5.63 | 5.28 | 5.12 | 5.30 | 4.74 | 5.10 | 4.56 | 4.55 |
| 4    | 5.94                                      | 5.25 | 4.41 | 4.29 | 4.36 | 3.19 | 3.15 | 3.53 | 2.72 |
| 5    | 4.62                                      | 3.61 | 2.25 | 2.67 | 2.20 | 1.42 | 1.12 | 2.16 | 1.64 |
| 6    | 4.67                                      | 4.03 | 3.20 | 3.42 | 3.36 | 2.79 | 2.75 | 2.62 | 2.52 |
| 7    | 4.79                                      | 4.10 | 3.38 | 3.80 | 3.86 | 2.97 | 3.06 | 3.34 | 2.89 |

row 4 plot blocks: no. of units along column(N->S) direction

| E->W | 1     | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
|------|-------|------|------|------|------|------|------|------|------|
| 1    | 12.20 | 9.36 | 8.37 | 7.63 | 6.70 | 6.62 | 6.13 | 6.16 | 5.86 |
| 2    | 7.97  | 6.59 | 5.63 | 5.37 | 5.16 | 4.49 | 4.52 | 4.28 | 3.94 |
| 3    | 7.14  | 5.48 | 4.78 | 4.42 | 4.83 | 3.96 | 4.37 | 3.84 | 3.75 |
| 4    | 5.50  | 4.89 | 3.97 | 3.83 | 3.93 | 2.87 | 2.89 | 3.09 | 2.38 |
| 5    | 5.26  | 4.29 | 3.37 | 3.77 | 3.47 | 2.87 | 3.04 | 3.31 | 2.98 |

*5 plot blocks:*

| row  | no. of units along column(N->S) direction |       |      |      |      |      |      |      |      |
|------|---|-------|------|------|------|------|------|------|------|
| E->W | 1   | 2     | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 12.68                                     | 10.06 | 9.03 | 8.28 | 7.58 | 7.21 | 6.90 | 6.79 | 6.25 |
| 2    | 8.85                                      | 7.55  | 6.65 | 6.48 | 6.33 | 5.75 | 5.90 | 5.48 | 5.09 |
| 3    | 6.82                                      | 5.23  | 4.38 | 4.06 | 4.39 | 3.57 | 3.93 | 3.52 | 3.39 |
| 4    | 6.30                                      | 5.65  | 4.78 | 4.96 | 4.95 | 4.05 | 4.38 | 4.37 | 3.68 |

*6 plot blocks:*

| row  | no. of units along column(N->S) direction |       |      |      |      |      |      |      |      |
|------|---|-------|------|------|------|------|------|------|------|
| E->W | 1   | 2     | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 13.22                                     | 10.36 | 9.42 | 8.67 | 7.89 | 7.45 | 7.40 | 7.32 | 6.68 |
| 2    | 9.10                                      | 7.64  | 6.46 | 6.06 | 5.85 | 4.99 | 5.00 | 4.82 | 4.31 |
| 3    | 7.42                                      | 5.99  | 5.41 | 5.25 | 5.45 | 4.78 | 5.12 | 4.68 | 4.59 |

*7 plot blocks:*

| row  | no. of units along column(N->S) direction |       |      |      |      |      |      |      |      |
|------|---|-------|------|------|------|------|------|------|------|
| E->W | 1   | 2     | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 13.00                                     | 10.24 | 8.91 | 8.28 | 7.27 | 7.04 | 6.81 | 6.83 | 6.21 |
| 2    | 8.89                                      | 7.45  | 6.11 | 5.78 | 5.53 | 4.66 | 4.63 | 4.55 | 4.06 |
| 3    | 7.42                                      | 6.05  | 5.31 | 5.44 | 5.34 | 4.72 | 4.89 | 4.86 | 4.56 |

*8 plot blocks:*

| row  | no. of units along column(N->S) direction |      |      |      |      |      |      |      |      |
|------|---|------|------|------|------|------|------|------|------|
| E->W | 1   | 2    | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 12.83                                     | 9.77 | 8.81 | 7.80 | 7.22 | 6.45 | 6.22 | 6.30 | 5.77 |
| 2    | 8.57                                      | 7.16 | 5.92 | 5.63 | 5.49 | 4.55 | 4.61 | 4.54 | 4.03 |

*9 plot blocks:*

| row  | no. of units along column(N->S) direction |       |      |      |      |      |      |      |      |
|------|---|-------|------|------|------|------|------|------|------|
| E->W | 1   | 2     | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 13.78                                     | 10.93 | 9.88 | 9.25 | 8.48 | 7.93 | 7.88 | 7.71 | 7.11 |
| 2    | 9.48                                      | 8.18  | 7.14 | 7.05 | 6.90 | 6.12 | 6.43 | 5.98 | 5.49 |

*10 plot blocks:*

| row  | no. of units along column(N->S) direction |       |      |      |      |      |      |      |      |
|------|---|-------|------|------|------|------|------|------|------|
| E->W | 1   | 2     | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 13.42                                     | 10.60 | 9.43 | 8.78 | 8.04 | 7.57 | 7.35 | 7.25 | 6.71 |
| 2    | 9.31                                      | 8.01  | 6.94 | 6.91 | 6.70 | 5.99 | 6.14 | 5.87 | 5.37 |

*11 plot blocks:*

| row  | no. of units along column(N->S) direction |       |      |      |      |      |      |      |      |
|------|---|-------|------|------|------|------|------|------|------|
| E->W | 1   | 2     | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 13.51                                     | 10.64 | 9.31 | 8.65 | 7.94 | 7.41 | 7.15 | 7.19 | 6.70 |
| 2    | 9.51                                      | 8.21  | 7.08 | 7.07 | 6.80 | 6.02 | 6.14 | 6.13 | 5.60 |

*12 plot blocks:*

| row  | no. of units along column(N->S) direction |       |      |      |      |      |      |      |      |
|------|---|-------|------|------|------|------|------|------|------|
| E->W | 1   | 2     | 3    | 4    | 5    | 6    | 7    | 8    | 9    |
| 1    | 13.99                                     | 10.75 | 9.64 | 8.36 | 8.03 | 7.00 | 6.79 | 6.85 | 6.36 |

TABLE 2.4.5: (Rice data) Within block C.V. when blocks run col.(N → S) direction

| row | <i>3 plot blocks:</i> no. of units along column(N→S) direction |             |      |      |      |      |
|-----|--|-------------|------|------|------|------|
| E→W | 1  | 2           | 3    | 4    | 5    | 6    |
| 1   | 10.19  | 8.16        | 6.75 | 5.80 | 5.55 | 5.63 |
| 2   | 6.64   | 5.94        | 4.61 | 4.39 | 4.42 | 4.11 |
| 3   | 5.52   | 4.35        | 3.17 | 3.32 | 3.85 | 3.56 |
| 4   | 4.44   | 4.49        | 3.45 | 3.42 | 3.24 | 2.40 |
| 5   | 4.39   | 3.85        | 2.27 | 2.87 | 2.39 | 1.85 |
| 6   | 3.92   | 3.75        | 2.48 | 2.75 | 2.93 | 2.43 |
| 7   | 3.88   | 3.53        | 2.39 | 2.18 | 3.02 | 2.11 |
| 8   | 3.40   | 3.75        | 2.41 | 2.59 | 2.20 | 0.67 |
| 9   | 3.01   | 3.08        | 1.80 | 2.25 | 1.66 | 0.91 |
| row | <i>4 plot blocks:</i> no. of units along column(N→S) direction |             |      |      |      |      |
| E→W | 1  | 2           | 3    | 4    |      |      |
| 1   | 10.68  | 8.19        | 6.95 | 6.98 |      |      |
| 2   | 6.60   | 5.83        | 4.73 | 5.14 |      |      |
| 3   | 5.61   | 4.45        | 4.13 | 4.37 |      |      |
| 4   | 4.31   | 4.04        | 3.73 | 3.51 |      |      |
| 5   | 4.28   | 3.48        | 3.25 | 3.02 |      |      |
| 6   | 3.67   | 3.76        | 3.02 | 3.41 |      |      |
| 7   | 3.76   | 3.23        | 2.53 | 3.07 |      |      |
| 8   | 3.04   | 3.01        | 2.62 | 2.63 |      |      |
| 9   | 3.20   | 2.75        | 2.63 | 2.15 |      |      |
| row | <i>5 plot blocks:</i> no. of units along column(N→S) direction |             |      |      |      |      |
| E→W | 1  | 2           | 3    |      |      |      |
| 1   | 11.36  | 8.94        | 7.68 |      |      |      |
| 2   | 7.07   | 6.35        | 5.29 |      |      |      |
| 3   | 5.67   | 4.24        | 4.66 |      |      |      |
| 4   | 4.55   | 4.33        | 3.85 |      |      |      |
| 5   | 4.59   | 3.60        | 3.27 |      |      |      |
| 6   | 3.87   | 3.51        | 3.51 |      |      |      |
| 7   | 3.77   | 2.51        | 3.33 |      |      |      |
| 8   | 3.26   | <b>2.63</b> | 2.68 |      |      |      |
| 9   | 3.22   | 2.21        | 2.36 |      |      |      |
| row | <i>6 plot blocks:</i> no. of units along column(N→S) direction |             |      |      |      |      |
| E→W | 1  | 2           | 3    |      |      |      |
| 1   | 11.83  | 8.90        | 8.24 |      |      |      |
| 2   | 7.82   | 6.39        | 5.83 |      |      |      |
| 3   | 6.35   | 4.62        | 4.75 |      |      |      |
| 4   | 5.52   | 4.52        | 4.06 |      |      |      |
| 5   | 5.17   | 3.74        | 3.29 |      |      |      |
| 6   | 4.70   | 3.72        | 3.57 |      |      |      |
| 7   | 4.64   | 3.03        | 3.31 |      |      |      |
| 8   | 4.28   | 3.21        | 2.69 |      |      |      |
| 9   | 3.80   | 2.80        | 2.49 |      |      |      |

| row | <i>7 plot</i>                            |      | <i>8 plot</i> |      | <i>9 plot blocks</i> |      |
|-----|--|------|---------------|------|----------------------|------|
|     | no. of units along column(N→S) direction |      |               |      |                      |      |
| E→W | 1  | 2    | 1             | 2    | 1                    | 2    |
| 1   | 12.17                                    | 9.24 | 11.83         | 9.47 | 12.22                | 9.92 |
| 2   | 7.77                                     | 6.54 | 7.58          | 6.82 | 8.08                 | 7.22 |
| 3   | 6.24                                     | 5.04 | 6.26          | 5.58 | 6.36                 | 5.62 |
| 4   | 5.23                                     | 4.58 | 5.06          | 4.65 | 5.63                 | 5.09 |
| 5   | 4.9                                      | 3.72 | 4.81          | 4.06 | 4.94                 | 4.27 |
| 6   | 4.47                                     | 4.04 | 4.47          | 4.4  | 4.63                 | 4.47 |
| 7   | 4.44                                     | 3.58 | 4.37          | 3.86 | 4.56                 | 4.11 |
| 8   | 3.71                                     | 3.22 | 3.6           | 3.5  | 4.17                 | 3.81 |
| 9   | 3.46                                     | 2.66 | 3.49          | 3.21 | 3.51                 | 3.21 |

| Row | Single unit along column(N→S) direction |                |                       |
|-----|---|----------------|-----------------------|
| E→W | <i>10 plot</i>                          | <i>11 plot</i> | <i>12 plot blocks</i> |
| 1   | 12.89                                   | 12.65          | 12.54                 |
| 2   | 8.03                                    | 7.95           | 8.07                  |
| 3   | 6.31                                    | 6.32           | 6.54                  |
| 4   | 5.45                                    | 5.35           | 5.55                  |
| 5   | 5.12                                    | 4.96           | 5.22                  |
| 6   | 4.27                                    | 4.21           | 4.38                  |
| 7   | 3.77                                    | 3.73           | 4.29                  |
| 8   | 3.34                                    | 3.36           | 3.84                  |
| 9   | 3.18                                    | 3.25           | 3.52                  |

From the following Table 2.4.6 for Rice data we see that with blocks of same size but different shapes formed from plots of the same size, there was detectable change in blocking efficiency. As in general for all plot sizes & shapes blocks running N→S showed higher blocking efficiency than the blocks running in E→W direction. The highest blocking efficiency value 3.21 was found for 3 plot blocks containing plots of size 9 sq. mt. & shape 3 x 3 (i.e. 3 mt. in E→W & 3 mt in N→S direction). For the same B.E. block size was 27 sq. mt. & shape was 1 : 3 (i.e. 3 mt. in E→W direction & 9 mt. in N→S direction). The second highest blocking efficiency was 3.10 was found for 3 plot blocks containing plot of size 15 sq. mt. & shape 5 : 3 (i.e. 5 mt. in E→W direction & 3 mt. in N→S direction). For the same B.E. block size was 45 sq. mt. & block shape was 5 : 9 (i.e. 5 mt. in E→W direction & 9 mt. in N→S direction). For 5 plot block highest blocking efficiency was 2.73 for plot of size 14 sq. mt. & shape 7 : 2 (i.e. 7 mt. in E→W direction & 2 mt. in N→S direction). For the same B.E. block size was 70 sq. mt. & block shape was 7 : 10 (i.e. 7 mt. in E→W direction & 10 mt. in N→S direction).

TABLE 2.4.6: (Rice data) Within block Blocking Efficiencies for different plot sizes when blocks run col.(N→S) direction

*3 plot blocks:*

| row | no. of units along column(N→S) direction |      |             |      |      |      |
|-----|--|------|-------------|------|------|------|
| E→W | 1  | 2    | 3           | 4    | 5    | 6    |
| 1   | 1.93                                     | 1.90 | 2.11        | 2.43 | 2.29 | 1.89 |
| 2   | 2.21                                     | 2.03 | 2.51        | 2.75 | 2.40 | 2.15 |
| 3   | 2.06                                     | 2.18 | <b>3.21</b> | 2.81 | 1.98 | 1.76 |
| 4   | 2.39                                     | 1.83 | 2.30        | 2.44 | 2.42 | 2.90 |
| 5   | 1.83                                     | 1.58 | <b>3.10</b> | 2.07 | 2.25 | 2.50 |
| 6   | 2.00                                     | 1.61 | 2.51        | 2.17 | 1.50 | 1.45 |
| 7   | 2.03                                     | 1.72 | 2.70        | 2.91 | 1.71 | 2.01 |
| 8   | 1.63                                     | 1.04 | 1.25        | 1.03 | 1.01 | 1.19 |
| 9   | 1.72                                     | 1.12 | 2.01        | 1.07 | 1.18 | 1.38 |

*4 plot blocks:*

| row | no. of units along column(N→S) direction |      |      |      |
|-----|--|------|------|------|
| E→W | 1  | 2    | 3    | 4    |
| 1   | 1.75                                     | 1.89 | 2.00 | 1.75 |
| 2   | 2.19                                     | 2.12 | 2.51 | 1.96 |
| 3   | 2.02                                     | 2.22 | 2.17 | 1.68 |
| 4   | 2.48                                     | 2.25 | 2.21 | 2.24 |
| 5   | 1.93                                     | 2.02 | 1.83 | 1.88 |
| 6   | 2.17                                     | 1.66 | 1.98 | 1.35 |
| 7   | 2.19                                     | 2.13 | 2.42 | 1.79 |
| 8   | 1.76                                     | 1.37 | 1.02 | 1.02 |
| 9   | 1.53                                     | 1.47 | 1.05 | 1.17 |

*5 plot blocks:*

| row | no. of units along column(N→S) direction |             |      |
|-----|--|-------------|------|
| E→W | 1  | 2           | 3    |
| 1   | 1.55                                     | 1.66        | 1.68 |
| 2   | 1.94                                     | 1.88        | 1.98 |
| 3   | 1.91                                     | 2.50        | 1.67 |
| 4   | 2.22                                     | 1.89        | 2.00 |
| 5   | 1.61                                     | 1.73        | 1.67 |
| 6   | 1.86                                     | 1.89        | 1.35 |
| 7   | 2.10                                     | <b>2.73</b> | 1.58 |
| 8   | 1.46                                     | 1.19        | 1.00 |
| 9   | 1.31                                     | 1.00        | 1.09 |

*6 plot blocks:*

| row   | no. of units along column(N → S) direction |      |      |
|-------|--|------|------|
| E → W | 1  | 2    | 3    |
| 1     | 1.43                                       | 1.61 | 1.42 |
| 2     | 1.59                                       | 1.83 | 1.57 |
| 3     | 1.56                                       | 1.94 | 1.43 |
| 4     | 1.55                                       | 1.82 | 1.67 |
| 5     | 1.32                                       | 1.63 | 1.47 |
| 6     | 1.39                                       | 1.64 | 1.21 |
| 7     | 1.42                                       | 1.99 | 1.41 |
| 8     | 1.03                                       | 1.02 | 1.01 |
| 9     | 1.08                                       | 1.04 | 1.05 |

| row   | no. of units along column(N → S) direction |      |               |      |                      |      |
|-------|--|------|---------------|------|----------------------|------|
|       | <i>7 plot</i>                              |      | <i>8 plot</i> |      | <i>9 plot blocks</i> |      |
| E → W | 1  | 2    | 1             | 2    | 1                    | 2    |
| 1     | 1.38                                       | 1.5  | 1.42          | 1.41 | 1.34                 | 1.29 |
| 2     | 1.63                                       | 1.69 | 1.66          | 1.55 | 1.49                 | 1.37 |
| 3     | 1.61                                       | 1.65 | 1.62          | 1.41 | 1.55                 | 1.31 |
| 4     | 1.71                                       | 1.73 | 1.8           | 1.7  | 1.49                 | 1.42 |
| 5     | 1.39                                       | 1.52 | 1.53          | 1.49 | 1.44                 | 1.28 |
| 6     | 1.39                                       | 1.3  | 1.47          | 1.21 | 1.43                 | 1.13 |
| 7     | 1.47                                       | 1.53 | 1.62          | 1.5  | 1.47                 | 1.27 |
| 8     | 1.06                                       | 1    | 1.26          | 1.01 | 1.08                 | 1.01 |
| 9     | 1.03                                       | 1.03 | 1.29          | 1.08 | 1.27                 | 1.03 |

| Row   | Single unit along column(N → S) direction |                |                       |
|-------|---|----------------|-----------------------|
| E → W | <i>10 plot</i>                            | <i>11 plot</i> | <i>12 plot blocks</i> |
| 1     | 1.32                                      | 1.31           | 1.31                  |
| 2     | 1.55                                      | 1.57           | 1.52                  |
| 3     | 1.68                                      | 1.62           | 1.47                  |
| 4     | 1.56                                      | 1.63           | 1.55                  |
| 5     | 1.36                                      | 1.43           | 1.32                  |
| 6     | 1.6                                       | 1.56           | 1.46                  |
| 7     | 1.77                                      | 1.85           | 1.5                   |
| 8     | 1.11                                      | 1.08           | 1.01                  |
| 9     | 1   | 1.01           | 1.03                  |

### Chapter 3

#### TWO WAY SPATIAL CORRELATION STUDY:

**3.1 Introduction:** The empirical model developed by Smith (1938) gives a measure of correlation between adjacent units in terms of a soil heterogeneity index 'b'. Here  $b = 0$  indicates perfect positive correlation and  $b = 1$  indicates no correlation between adjacent units. An alternative approach to the analysis based on Smith's model is a direct study of the correlation structure among experimental units. Li and Keller (1951) estimated lag-one serial correlations to obtain information on the randomness of a set of uniformity data and to compare relative efficiencies of different sizes and shapes of plots. However, a more complete analysis of the correlation structure would include the estimation of two dimensional spatial correlations of various lags. Whittle (1954) computed the spatial correlations for several uniformity studies as a model fitting and testing exercise on the nature of the two dimensional autoregressive models operating in the field, but he did not attempt to use the correlation structure to infer on the optimum plot size and shape. In 1983 Modjeska and Rawlings presented the spatial correlation analysis of uniformity data as an alternative to the conventional method of analysis based on Smith's model. Here the spatial correlation model permits arbitrary patterns of behavior of the correlations, in contrast to the strict monotonic decrease required in Smith's model. It also provides more information about the nature of the variation in the uniformity trial.

**3.2 Material and method:** Let  $Y = \{ Y_{ij} \}$  be a matrix of crop yield from a uniformity trial of  $R \times C$  units in size where  $i = 1, 2, \dots, R$  and  $j = 1, 2, \dots, C$  designate row and column numbers. Here the spatial correlation model assumes that all pairs of observations having same spatial relationship have the same correlation. Thus  $Y_{ij} = \mu + \varepsilon_{ij}$  and

$$\frac{E(\varepsilon_{ij}, \varepsilon_{i'j'})}{\sigma^2} = \rho(l, k) \quad \text{where } l = i' - i \text{ and } k = j' - j \text{ define the two dimensional lags or the}$$

number of unit plots from plot  $(i, j)$  across rows and across columns respectively, to plot  $(i', j')$ . Because of symmetry of correlation  $\rho(l, k) = \rho(-l, -k)$  and  $\rho(l, -k) = \rho(-l, k)$ . Three spatial correlation matrices of dimension  $m \times n$  are defined as  $\rho^+ = \{\rho(l, k)\}$   $\rho^- = \{\rho(l, -k)\}$

and  $\bar{\rho} = \frac{1}{2}(\rho^+ + \rho^-)$  where  $0 \leq l \leq m-1$  and  $0 \leq k \leq n-1$ . Here  $m \times n$  is the maximum plot size to be considered. For  $l, k > 0$ ,  $\rho^+$  and  $\rho^-$  contain spatial correlations for lags in

different diagonal directions. The first row and first column ( $l = 0$  or  $k = 0$ ) of  $\rho^+$  and  $\rho^-$  will be identical. No constraints are imposed on the manner in which  $\rho(l, k)$  changes with  $l$  and  $k$ ; in particular  $\rho(l, k)$  can be negative and need not be monotonic function of  $l$  and  $k$ . If the field consists of regular cycles of fertility with axes coinciding with the axes of the field,  $\rho^+ = \rho^-$  and the spatial correlations will cycle between +1 and -1 with a frequency corresponding to the frequency of the fertility cycles. That is, the spatial correlations reproduce the soil fertility patterns. If the axes of the fertility cycles are not parallel to the field axes,  $\rho^+ \neq \rho^-$ . If the fertility cycles are not regular, the cycle length of the spatial correlations will reflect an averaging of the lengths of the fertility cycles and the spatial correlations will not approach  $\pm 1$ . If the field is uniform with random error attached to all unit plots, the true spatial correlations will be zero. The spatial covariances,  $\text{cov}(l, k)$ , are defined similarly as the three  $m \times n$  spatial covariance matrices,  $\text{cov}^+$ ,  $\text{cov}^-$  and  $\overline{\text{cov}}$ . The variance among plots  $r \times c$  units in size in a field of size  $R \times C$  is:

$$\text{MSE}(rc/RC) = \frac{\left\{ r c \overline{\text{cov}}(0,0) + 2r \sum_{k=1}^c (c-k) \overline{\text{cov}}(0,k) + 2c \sum_{l=1}^r (r-l) \overline{\text{cov}}(l,0) + 4 \sum_{l=1}^r \sum_{k=1}^c (c-k) \cdot (r-l) \overline{\text{cov}}(l,k) \right\}}{r \cdot c}$$

Here  $\text{MSE}(RC) = \{\text{MSE}(rc / RC)\}$  is the  $m \times n$  matrix of variances among plots of size  $r \times c$ , where  $r$  and  $c$  designate the row and column positions in the  $\text{MSE}$  matrix as well as the plot size and can be expressed in terms of  $\overline{\text{cov}}$  as  $\text{MSE}(RC) = k_m * \overline{\text{cov}} * k_n'$ , where,  $k_m = (L_m^2 * D_m) \# / (L_m * J_m)$ ,  $L_m = m \times m$  lower triangular matrix of 1's,  $D_m = \text{diag}(1, 2, \dots, 2)$  of dimension  $m \times m$ ,  $J_m = m \times m$  matrix of 1's and '#' denotes element wise division. The spatial covariances and correlations are computed for  $0 \leq l \leq \frac{1}{2} \cdot R - 1$ ,

$0 \leq |k| \leq \frac{1}{2} \cdot C - 1$ . The estimate  $\hat{\text{cov}}^+$  is computed as the  $\frac{1}{2} \cdot R \times \frac{1}{2} \cdot C$  matrix whose elements are :

$$\hat{\text{cov}}^+(l, k) = \frac{\sum_i \sum_j Y_{ij} \cdot Y_{i+l, j+k} - (\sum_i \sum_j Y_{ij}) \cdot (\sum_i \sum_j Y_{i+l, j+k})}{\{(R-l) \cdot (C-k) - 1\}}$$

with summations over all combinations of  $1 \leq i \leq R-l$  and  $1 \leq j \leq C-k$ ,  $k \geq 0$ . Similarly

$\widehat{cov}^-$  is computed as the  $\frac{1}{2}R \times \frac{1}{2}C$  matrix whose elements are:

$$\widehat{cov}^-(l, k) = \frac{\sum_i \sum_j Y_{i,j-k} \cdot Y_{i+l,j} - (\sum_i \sum_j Y_{i,j-k}) \cdot (\sum_i \sum_j Y_{i+l,j})}{\{(R-l) \cdot (C+k) - 1\}}$$

with summations over  $1 \leq i \leq R-l$  and  $1 \leq j \leq C+k$ ,  $k \leq 0$ . Then  $\overline{cov} = \frac{1}{2}(\widehat{cov}^+ + \widehat{cov}^-)$ . The

spatial correlations are computed by dividing each  $\widehat{cov}(l, k)$  by the geometric mean of covariances of the two subsets of  $Y_{ij}$  involved, rather than by  $\widehat{cov}(0, 0)$ . This procedure appears to give more stability to  $\widehat{\rho}(l, k)$  as  $l$  and  $k$  become large.

Comparison of the elements of **MSE(RC)** gives the relative efficiencies of plots of  $r \times c$  within blocks of  $R \times C$ . Thus the matrix of variances among plots of all possible sizes up to  $\frac{1}{2}R \times \frac{1}{2}C$  is

computed as  $M\widehat{SE}(RC) = K_m * \widehat{cov} * K_n'$ , where  $m = \frac{1}{2}R$  and  $n = \frac{1}{2}C$ , and is standardized by

dividing all elements by the variance among unit plots. Thus,  $\widehat{STMSE}(RC) = M\widehat{SE}(RC) / M\widehat{SE}(11/RC)$ . The quantity  $M\widehat{SE}(rc/RC)/rc$  is equal to  $(V_{rc})_{RC}$  in Smith's notation. Behavior of the MSE is shown by plotting  $\ln\{M\widehat{SE}(rc/RC)/rc\}$  against  $\ln(rc)$ . If Smith's original model holds, a linear relationship is obtained; because of the density of points, a graphical estimate of  $b$  appears adequate. If the two dimensional model holds, the graph would be a parallelogram with the slopes for all columns being  $-b_1$  and those for all rows being  $-b_2$ .

**A two dimensional version of Smith's model and its implications for the spatial correlation structure:** Smith (1938) recognized that the index of soil heterogeneity need not be the same for plots oriented in different directions in the field and that the longer axis of the plots should cover the greatest variability. In Smith's analysis this can be taken into account by computing variances and estimating  $b$  separately for different plot orientations. For our purposes it is more convenient to define a two-dimensional version of Smith's model for variances of plots of size  $r \times c$  as

$V_{rc} = \frac{V_1}{r^{b_1} c^{b_2}}$ , where  $b_1$  and  $b_2$  are indices of soil heterogeneity across rows and across columns, respectively. If  $b_1=b_2$ , Smith's one-dimensional model holds as a special case. If two-



$$MSE(p/tp) = \left\{ t \cdot MSE(p/N) - MSE(tp/N) \right\} / (t-1) + \frac{\beta}{t-1} \{ MSE(tp/N) - MSE(p/N) \} \dots 1) \text{ where}$$

$N = R \times C$ ,  $p$  = number units per plot,  $t$  = number of plots per block and  $\beta = tp/N$ , the size of

the new block relative to the size of the original block. If  $\frac{\alpha}{t-1}$  is small enough to enable the

second term to be ignored, and if Smith's model holds i.e.  $\frac{MSE(p/N)}{p} = \frac{(V_1)_N}{p^b}$ , then equation

1) becomes 
$$\frac{MSE(p/tp)}{p} = \frac{t \cdot (1-t^{-b})(V_p)_N}{(t-1)}$$
 which is the Smith's (1938) result after adjustment

for block size. However the mean square among plots of dimension  $r \times c = p$  within blocks of dimension  $\alpha.r \times \gamma.c$  is,

$$\text{approximately, } MSE(rc/\alpha r \times \gamma c) = \{ MSE(rc/RC) - MSE(\alpha r \times \gamma c/RC) \} / (t-1).$$

Substitution of the two-dimensional version of Smith's model gives

$$V(rc/\alpha r \times \gamma c) = \frac{t \cdot (V_1)_N}{(t-1)r^{b_1}c^{b_2}} (1 - \alpha^{b_2-b_1}t^{-b_2}).$$

If cost is a function of only plot size,  $p$ , and not of plot shape, the variance is minimized for given  $p = r \times c$  by making  $r = p$ ,  $c = 1$  if  $b_1 > b_2$ , or

$r = 1$ ,  $c = p$  if  $b_2 > b_1$ . The optimum plot is one unit wide and  $p$  units long with longer axis of the plot running in the direction of the larger  $b$ ; that is, in the direction of greater variability as indicated by Smith (1938). Further, the optimum block shape is given by  $\alpha = 1$ ,  $\gamma = t$  if  $b_1 > b_2$ ,

or  $\alpha = t$ ,  $\gamma = 1$  if  $b_2 > b_1$ , that is, the optimum block shape will contain  $t$  optimum plots side by side. Assuming without loss of generality that  $b_2 > b_1$ , then  $r_{opt} = 1$ ,  $c_{opt} = p$  and  $\alpha_{opt} = t$  and the

cost per unit information is 
$$\frac{t(V_1)_N}{(t-1)p^{b_2}} (1 - t^{-b_1})(k_1 + k_2 p),$$
 where  $k_1$  and  $k_2$  are costs as defined

by Smith (1938). Minimization with respect to  $p$  gives 
$$p_{opt} = \frac{b_2 \cdot k_1}{(1-b_2) \cdot k_2}$$
 which is the Smith's

original formula for optimum plot size except that the larger  $b$  in this case  $b_2$  determines optimum plot size. However in the conventional analysis of uniformity data we obtain some sort of average of  $b_1$  and  $b_2$  as the measure of soil heterogeneity causing underestimation of the optimum plot size.

(iii) The two dimensional model does not hold. In this general case a matrix of costs per unit of information can be computed as  $Cost / I = [(k_1 J_m + k_2 N) \# MSE(RC)] \# / N$  where  $N = L_m * J_n * L_n' = \{(number\ of\ unit\ plots\ per\ plot)\}$ , and the symbol '#' means element wise multiplication. Inspection of  $Cost / I$  for the minimum value will reveal the optimum plot size within a block of size  $R \times C$ .

**3.4 Result and discussion:** Yield was not constant within any of these regions and appeared to change along both row and column. The only obvious patter was a cycling across rows, but because the pattern lacked regularity no cycle length could be ascertained from a visual inspection of the field response surface.

The spatial correlations started at relatively low values and remained fairly constant within the rows of Table 3.4.1. Within the columns of Table 3.4.1, correlations decreased to a negative correlation at about lag 12 as large in absolute value as the positive lag-one correlations. This suggested that there was a major micro-environmental cycle in the field with a half-cycle length of about 12 units, and that conditions with a row remained relatively constant.

TABLE 3.4.1: Jute data: Spatial correlation left =>R-(l, k) right =>R+(l, k)

|    | k      |        |        |        |        |        |        |        |        |       |        |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|
| l  | -5     | -4     | -3     | -2     | -1     | 0      | 1      | 2      | 3      | 4     | 5      |
| 0  | 0.156  | 0.111  | 0.005  | -0.068 | 0.192  | 1      | 0.192  | -0.068 | 0.005  | 0.111 | 0.156  |
| 1  | 0.012  | -0.008 | -0.062 | -0.191 | 0.081  | 0.245  | 0.056  | -0.154 | -0.048 | 0.099 | 0.145  |
| 2  | 0.158  | 0.174  | -0.038 | -0.089 | 0.161  | 0.109  | -0.007 | -0.139 | 0.016  | 0.186 | 0.1    |
| 3  | 0.173  | 0.121  | -0.101 | -0.065 | 0.136  | 0.245  | 0.02   | -0.178 | -0.061 | 0.176 | 0.108  |
| 4  | 0.11   | -0.032 | -0.126 | -0.023 | 0.119  | 0.186  | 0.022  | -0.216 | -0.063 | 0.106 | 0.059  |
| 5  | 0.108  | 0      | 0.001  | 0.005  | 0.065  | 0.182  | -0.037 | -0.142 | 0.021  | 0.248 | 0.119  |
| 6  | 0.036  | -0.136 | -0.052 | -0.089 | 0.019  | 0.123  | -0.099 | -0.169 | 0      | 0.12  | 0.077  |
| 7  | 0.078  | 0.02   | -0.062 | 0.015  | 0.081  | 0.133  | -0.07  | -0.165 | 0.137  | 0.12  | 0.096  |
| 8  | 0.025  | 0.014  | 0.02   | 0.026  | 0.099  | 0.078  | -0.074 | -0.008 | 0.1    | 0.189 | 0.055  |
| 9  | 0.009  | -0.08  | -0.004 | -0.055 | 0.056  | 0.019  | -0.161 | -0.027 | 0.073  | 0.184 | 0.016  |
| 10 | -0.029 | 0.019  | -0.065 | 0.012  | -0.023 | -0.061 | -0.104 | -0.15  | -0.035 | 0.07  | -0.052 |
| 11 | 0.002  | -0.012 | 0.064  | 0.103  | 0.112  | -0.049 | -0.059 | -0.016 | 0.128  | 0.13  | -0.07  |
| 12 | -0.106 | -0.126 | -0.007 | -0.016 | 0.01   | 0.03   | -0.052 | 0.004  | 0.189  | 0.107 | -0.008 |
| 13 | -0.025 | -0.023 | -0.012 | 0.023  | -0.014 | 0.003  | -0.101 | 0.01   | 0.133  | 0.067 | -0.108 |
| 14 | -0.07  | 0.02   | 0.103  | 0.114  | 0.129  | -0.047 | -0.084 | 0.066  | 0.133  | 0.081 | -0.032 |
| 15 | -0.158 | -0.119 | 0.029  | 0.045  | 0.036  | 0.003  | -0.086 | 0.056  | 0.094  | -0.01 | -0.138 |

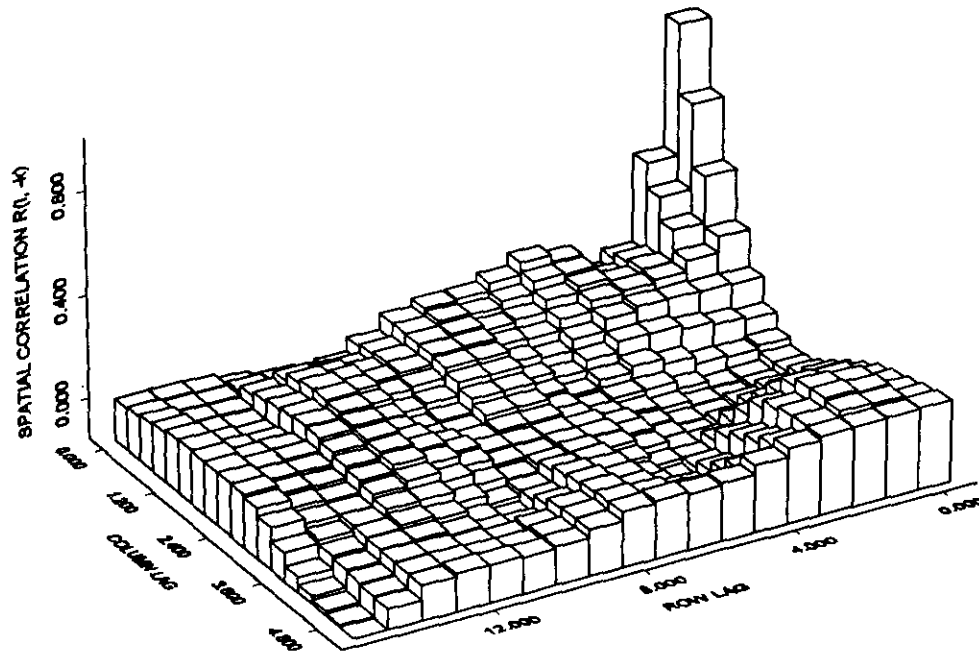


Fig. 3.4.1 (Jute data) Spatial correlation surface  $R(l, k)$  for different row and column lags.

The patterns of change in  $\hat{\rho}^+$  and  $\hat{\rho}^-$  differ appreciably. There are sizeable negative correlations in  $\hat{\rho}^+$  than in  $\hat{\rho}^-$ . For lag columns 4 & 5 there is a clear tendency for the +ve correlations to cycle to negative values as large as the lag zero correlations. However in general correlation values with increase in lag both in row and column directions. But the decay is more uniform in  $\hat{\rho}^-$  than in  $\hat{\rho}^+$  as obvious from fig.4 and fig.5. The first column of  $\hat{\rho}^-$  showed a slow decay relative to the decay from  $\hat{\rho}(0,0) = 1$  to  $\hat{\rho}^-(1,0)$ . In general spatial correlation decays at a faster rate along columns than along rows. For reference, the correlation attenuation curves predicted from Smith's model with  $b_1 \cong 0.9$  and  $b_2 \cong 0.6$  are included in Fig. 4 as  $\rho_s(0.9)$  and  $\rho_s(0.6)$ , respectively. These correlation patterns reflect a pattern of 'fertility' ridges running the length of the field with more or less constant performance within any one column.

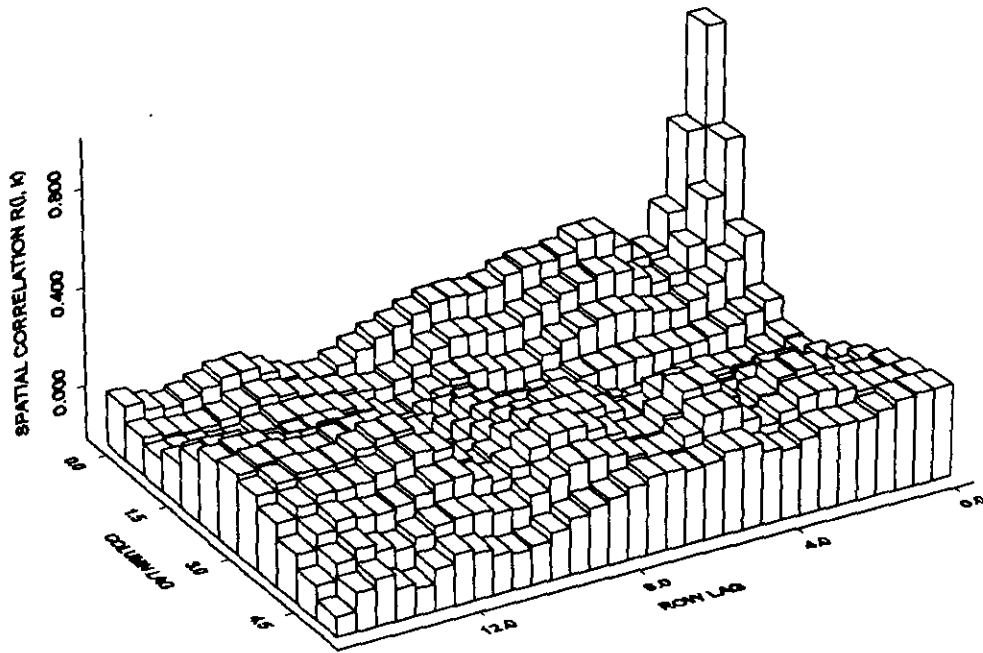


Fig. 3.4.2. (Jute data) Spatial correlation surface  $R(l, k)$  for different row and column lags.

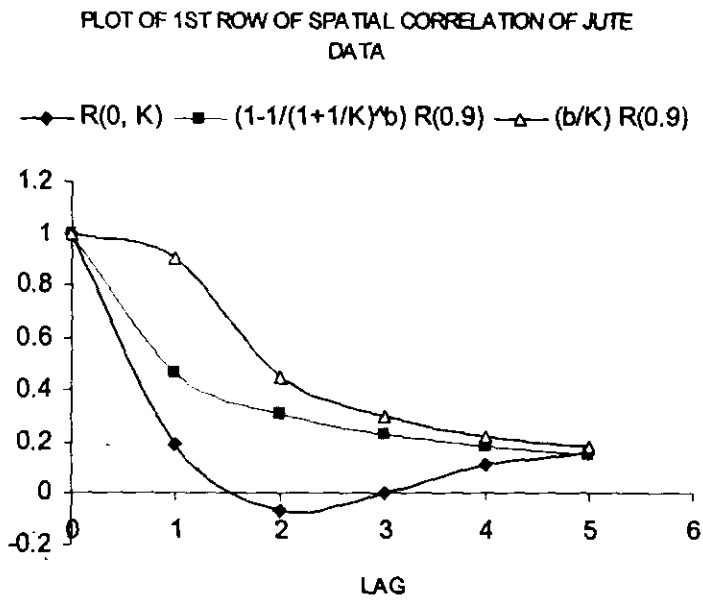


Fig. 3.4.3. (Jute data) plot of first row of spatial correlation matrix.

FLOT OF 1ST COLUMN OF SPATIAL  
CORRELATION FOR JUTE DATA

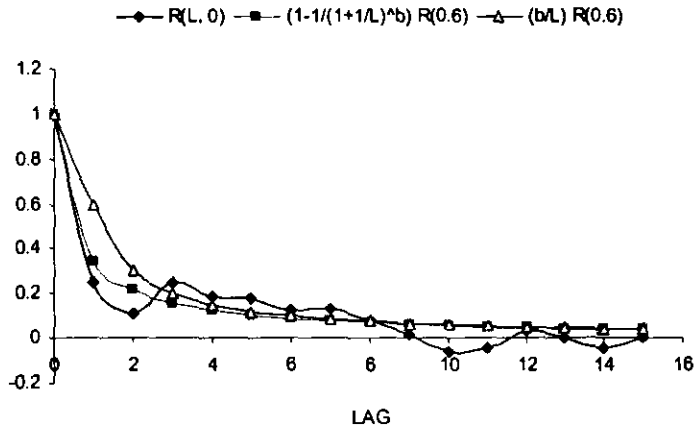


Fig. 3.4.4. (Jute data) plot of first column of spatial correlation matrix.

TABLE 3.4.2: Average Spatial correlation  $R(l, k)$

| l  | K      |        |        |        |        |        |
|----|--------|--------|--------|--------|--------|--------|
|    | 0      | 1      | 2      | 3      | 4      | 5      |
| 0  | 1.000  | 0.192  | -0.068 | 0.005  | 0.111  | 0.156  |
| 1  | 0.245  | 0.069  | -0.173 | -0.055 | 0.045  | 0.079  |
| 2  | 0.109  | 0.077  | -0.114 | -0.011 | 0.180  | 0.129  |
| 3  | 0.245  | 0.078  | -0.121 | -0.081 | 0.149  | 0.140  |
| 4  | 0.186  | 0.071  | -0.119 | -0.094 | 0.037  | 0.085  |
| 5  | 0.182  | 0.014  | -0.068 | 0.011  | 0.124  | 0.114  |
| 6  | 0.123  | -0.040 | -0.129 | -0.026 | -0.008 | 0.056  |
| 7  | 0.133  | 0.005  | -0.075 | 0.037  | 0.070  | 0.087  |
| 8  | 0.078  | 0.012  | 0.009  | 0.060  | 0.101  | 0.040  |
| 9  | 0.019  | -0.052 | -0.041 | 0.034  | 0.052  | 0.012  |
| 10 | -0.061 | -0.063 | -0.069 | -0.050 | 0.044  | -0.040 |
| 11 | -0.049 | 0.026  | 0.044  | 0.096  | 0.059  | -0.034 |
| 12 | 0.030  | -0.021 | -0.006 | 0.091  | -0.009 | -0.057 |
| 13 | 0.003  | -0.058 | 0.016  | 0.060  | 0.022  | -0.067 |
| 14 | -0.047 | 0.023  | 0.090  | 0.118  | 0.050  | -0.051 |
| 15 | 0.003  | -0.025 | 0.050  | 0.062  | -0.064 | -0.148 |

The matrix of  $STMSE(ac/AC)$ , shown in Table 3.4.4, revealed a faster increase in variance along rows than along columns. For example, a 1 X 4 plot was better than either a 2 X 2 or a 4 X 1. The advantage of orienting plot length with columns became even greater as plot length increased. A 1 X 6 plot is 28 % more efficient than a 3 X 2 plot and 46 % more efficient than a 6 X 1 plot. In

this field, very little penalty would be paid, in STMSE by doubling plot size from  $R \times 3$  to  $R \times 6$ . This is because the negative correlations of lags greater than about three offset the impact of the earlier positive correlations. The overall behavior of STMSE was shown by graphing  $\ln \{STMSE(ac/AC)/ac\}$  versus  $\ln(ac)$  using only the border rows and columns of STMSE for simplicity. Independent units would give a line with slope  $-1.0$ . If Smith's model holds, all points would fall about a line with slope  $-b$ . If the two-dimensional model holds the graph would be a parallelogram with the slopes for all columns being  $-b_1$  and those for all rows being  $-b_2$ . For the Jute data (Fig.3.4.6), the graphs of rows were reasonably linear but showed a gradual change in slope from  $-0.578$  for Column 1 to  $-0.661$  for Column 6. The graphs of rows showed a distinct downward curvature, reflecting the impact of the negative lag correlations, with the average slope changing from  $-0.85$  for Row 1 to  $-1.06$  for Row 16. Analyses of the four quarters of the Jute field data demonstrated the sensitivity of uniformity trial data to the specific location of the trial. The northeast quarter gave a Smith's  $b \cong 0.95$ . That for the southwest quarter also gave concordant regression but with a distinct upward curvature and  $b \cong 0.739$ . The northwest and southeast quarters gave the  $b$  values as 0.60 and 0.87. The spatial correlation matrices for the four quarters were also different. It is evident that results from uniformity trials, for both correlation and variance, are specific to the particular field being studied.

TABLE 3.4.3: MSE for plots  $a \times c$  units

|    | Number of unit plots, c |         |         |         |         |         |
|----|-------------------------|---------|---------|---------|---------|---------|
| a  | 1                       | 2       | 3       | 4       | 5       | 6       |
| 1  | 1610.48                 | 1921.48 | 1951.94 | 1970.69 | 2051.66 | 2189.29 |
| 2  | 2002.92                 | 2424.12 | 2305.87 | 2208.12 | 2247.77 | 2400.08 |
| 3  | 2251.37                 | 2792.27 | 2570.00 | 2400.64 | 2482.57 | 2723.45 |
| 4  | 2575.75                 | 3240.66 | 2921.85 | 2662.98 | 2781.23 | 3114.83 |
| 5  | 2892.36                 | 3678.13 | 3264.96 | 2904.88 | 3025.66 | 3420.58 |
| 6  | 3201.47                 | 4075.41 | 3577.33 | 3141.45 | 3285.01 | 3755.20 |
| 7  | 3478.46                 | 4397.40 | 3793.07 | 3274.60 | 3416.06 | 3936.20 |
| 8  | 3740.20                 | 4695.19 | 3991.63 | 3408.66 | 3558.01 | 4133.54 |
| 9  | 3971.69                 | 4959.22 | 4182.19 | 3560.87 | 3737.41 | 4374.73 |
| 10 | 4162.91                 | 5160.01 | 4309.82 | 3655.74 | 3859.12 | 4550.58 |
| 11 | 4301.85                 | 5288.72 | 4359.64 | 3662.42 | 3882.84 | 4611.56 |
| 12 | 4404.63                 | 5390.26 | 4405.87 | 3689.71 | 3940.43 | 4708.12 |
| 13 | 4498.61                 | 5478.44 | 4444.62 | 3720.67 | 4000.66 | 4799.12 |
| 14 | 4579.73                 | 5542.19 | 4464.30 | 3738.64 | 4048.42 | 4871.84 |
| 15 | 4640.28                 | 5592.65 | 4491.02 | 3782.66 | 4133.50 | 4985.16 |
| 16 | 4693.81                 | 5632.61 | 4515.18 | 3830.04 | 4216.72 | 5083.60 |

TABLE 3.4.4: Standardised Mean Square Error for plots of a x c units

| a  | Number of unit plots, c |       |       |       |       |       |
|----|-------------------------|-------|-------|-------|-------|-------|
|    | 1                       | 2     | 3     | 4     | 5     | 6     |
| 1  | 1.000                   | 1.193 | 1.212 | 1.224 | 1.274 | 1.359 |
| 2  | 1.244                   | 1.505 | 1.432 | 1.371 | 1.396 | 1.490 |
| 3  | 1.398                   | 1.734 | 1.596 | 1.491 | 1.542 | 1.691 |
| 4  | 1.599                   | 2.012 | 1.814 | 1.654 | 1.727 | 1.934 |
| 5  | 1.796                   | 2.284 | 2.027 | 1.804 | 1.879 | 2.124 |
| 6  | 1.988                   | 2.531 | 2.221 | 1.951 | 2.040 | 2.332 |
| 7  | 2.160                   | 2.730 | 2.355 | 2.033 | 2.121 | 2.444 |
| 8  | 2.322                   | 2.915 | 2.479 | 2.117 | 2.209 | 2.567 |
| 9  | 2.466                   | 3.079 | 2.597 | 2.211 | 2.321 | 2.716 |
| 10 | 2.585                   | 3.204 | 2.676 | 2.270 | 2.396 | 2.826 |
| 11 | 2.671                   | 3.284 | 2.707 | 2.274 | 2.411 | 2.863 |
| 12 | 2.735                   | 3.347 | 2.736 | 2.291 | 2.447 | 2.923 |
| 13 | 2.793                   | 3.402 | 2.760 | 2.310 | 2.484 | 2.980 |
| 14 | 2.844                   | 3.441 | 2.772 | 2.321 | 2.514 | 3.025 |
| 15 | 2.881                   | 3.473 | 2.789 | 2.349 | 2.567 | 3.095 |
| 16 | 2.915                   | 3.497 | 2.804 | 2.378 | 2.618 | 3.157 |

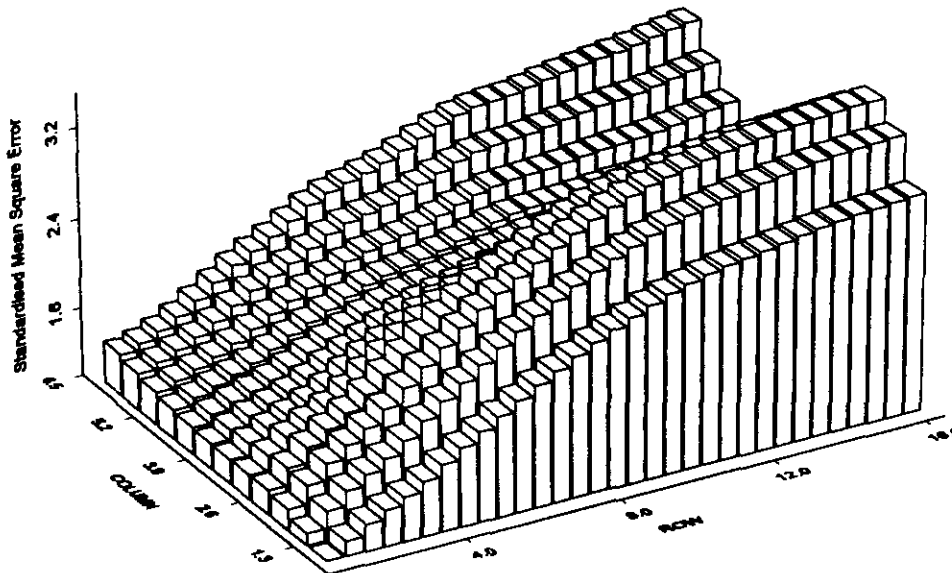


Fig.3.4.5: Three dimensional plot of Standardised Mean Square Error for plots of a x c units

TABLE 3.4.5: Cost per unit of information for plots a x c units

| a  | Number of unit plots, c |         |         |         |                |         |
|----|-------------------------|---------|---------|---------|----------------|---------|
|    | 1                       | 2       | 3       | 4       | 5              | 6       |
| 1  | 3308.57                 | 2305.49 | 1786.02 | 1522.51 | 1409.74        | 1379.58 |
| 2  | 2403.21                 | 1872.81 | 1453.04 | 1234.20 | 1160.32        | 1170.58 |
| 3  | 2060.00                 | 1759.55 | 1375.46 | 1170.85 | <b>1140.10</b> | 1199.00 |
| 4  | 1989.96                 | 1811.33 | 1425.06 | 1203.98 | 1198.03        | 1297.37 |
| 5  | 1987.40                 | 1898.69 | 1499.40 | 1251.29 | 1251.61        | 1376.00 |
| 6  | 2017.41                 | 1987.68 | 1574.92 | 1308.45 | 1321.46        | 1474.95 |
| 7  | 2050.40                 | 2055.25 | 1618.45 | 1330.60 | 1346.38        | 1519.35 |
| 8  | 2090.54                 | 2122.78 | 1662.56 | 1359.06 | 1380.60        | 1574.49 |
| 9  | 2125.65                 | 2183.30 | 1708.84 | 1398.62 | 1432.47        | 1649.06 |
| 10 | 2148.94                 | 2222.70 | 1733.71 | 1418.53 | 1464.47        | 1700.94 |
| 11 | 2153.82                 | 2237.06 | 1731.18 | 1406.89 | 1461.40        | 1711.79 |
| 12 | 2148.25                 | 2245.11 | 1730.52 | 1405.43 | 1472.87        | 1737.47 |
| 13 | 2144.80                 | 2251.83 | 1729.50 | 1407.04 | 1486.62        | 1762.29 |
| 14 | 2140.47                 | 2252.01 | 1723.19 | 1405.05 | 1496.76        | 1781.37 |
| 15 | 2131.00                 | 2249.75 | 1721.32 | 1413.90 | 1521.49        | 1816.04 |
| 16 | 2122.16                 | 2245.77 | 1719.86 | 1424.79 | 1546.12        | 1845.87 |

TABLE 3.4.6 JUTE DATA

| PLOT SIZE  | ln(p)    | STMSE | STMSE/p  | ln(STMSE/p) |
|------------|----------|-------|----------|-------------|
| (row1)     |          |       |          |             |
| 1          | 0        | 1     | 1        | 0           |
| 2          | 0.693147 | 1.193 | 0.5965   | -0.51667604 |
| 3          | 1.098612 | 1.212 | 0.404    | -0.90634041 |
| 4          | 1.386294 | 1.224 | 0.306    | -1.18417019 |
| 5          | 1.609438 | 1.274 | 0.2548   | -1.36727637 |
| 6          | 1.791759 | 1.359 | 0.2265   | -1.48501035 |
| (row 16)   |          |       |          |             |
| 16         | 2.772589 | 2.915 | 0.182188 | -1.70271892 |
| 32         | 3.465736 | 3.497 | 0.109281 | -2.21383047 |
| 48         | 3.871201 | 2.804 | 0.058417 | -2.84015407 |
| 64         | 4.158883 | 2.378 | 0.037156 | -3.29262332 |
| 80         | 4.382027 | 2.618 | 0.032725 | -3.419616   |
| 96         | 4.564348 | 3.157 | 0.032885 | -3.41472602 |
| (Column 1) |          |       |          |             |
| 1          | 0        | 1     | 1        | 0           |
| 2          | 0.693147 | 1.244 | 0.622    | -0.47481519 |

|            |          |       |          |             |
|------------|----------|-------|----------|-------------|
| 3          | 1.098612 | 1.398 | 0.466    | -0.76356965 |
| 4          | 1.386294 | 1.599 | 0.39975  | -0.91691594 |
| 5          | 1.609438 | 1.796 | 0.3592   | -1.02387595 |
| 6          | 1.791759 | 1.988 | 0.331333 | -1.10463037 |
| 7          | 1.94591  | 2.16  | 0.308571 | -1.17580194 |
| 8          | 2.079442 | 2.322 | 0.29025  | -1.23701267 |
| 9          | 2.197225 | 2.466 | 0.274    | -1.29462719 |
| 10         | 2.302585 | 2.585 | 0.2585   | -1.3528596  |
| 11         | 2.397895 | 2.671 | 0.242818 | -1.41544235 |
| 12         | 2.484907 | 2.735 | 0.227917 | -1.47877523 |
| 13         | 2.564949 | 2.793 | 0.214846 | -1.53783309 |
| 14         | 2.639057 | 2.844 | 0.203143 | -1.59384583 |
| 15         | 2.70805  | 2.881 | 0.192067 | -1.64991276 |
| 16         | 2.772589 | 2.915 | 0.182188 | -1.70271892 |
| (Column 6) | 1.791759 | 1.359 | 0.2265   | -1.48501035 |
| 6          |          |       |          |             |
| 12         | 2.484907 | 1.49  | 0.124167 | -2.08613055 |
| 18         | 2.890372 | 1.691 | 0.093944 | -2.36505171 |
| 24         | 3.178054 | 1.934 | 0.080583 | -2.51846346 |
| 30         | 3.401197 | 2.124 | 0.0708   | -2.64789631 |
| 36         | 3.583519 | 2.332 | 0.064778 | -2.7367927  |
| 42         | 3.73767  | 2.444 | 0.05819  | -2.84403361 |
| 48         | 3.871201 | 2.567 | 0.053479 | -2.92846314 |
| 54         | 3.988984 | 2.716 | 0.050296 | -2.98982387 |
| 60         | 4.094345 | 2.826 | 0.0471   | -3.05548231 |
| 66         | 4.189655 | 2.863 | 0.043379 | -3.13778475 |
| 72         | 4.276666 | 2.923 | 0.040597 | -3.20405567 |
| 78         | 4.356709 | 2.98  | 0.038205 | -3.26478556 |
| 84         | 4.430817 | 3.025 | 0.036012 | -3.32390574 |
| 90         | 4.49981  | 3.095 | 0.034389 | -3.3700218  |
| 96         | 4.564348 | 3.157 | 0.032885 | -3.41472602 |

b

b

row1-> -0.85186

row2-> -0.9379631

row16-> -1.06021

row15-> -1.0655809

col1-> -0.57843

col2-> -0.5786431

col6-> -0.6612

col5-> -0.7132134

## JUTE DATA

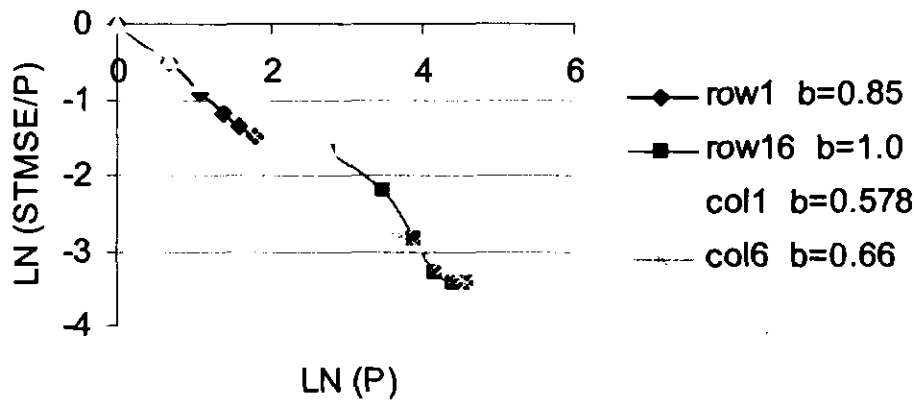


Fig. 3.4.6 Plot of  $\ln(\text{STMSE}/p)$  versus  $\ln(p)$  using the first and last rows and columns of the STMSE matrix from the Jute data.

The changing slopes over rows and columns and the distinct curvature of the graphs (Fig.7) for the rows are clear indications that in this case even two-dimensional version of Smith's model may be inadequate to find the optimum plot size. However we can use the table 12 containing the cost aspect. It is observed that the cost per unit of information is minimum for 3m. x 5m. plot for the Jute data.

One end of the Rice field was dominated by very high yields, the middle region by low yield, and the other end by a mixture of high and intermediate yields. Yield was not constant within any of these regions and appeared to change along both row and column. The only obvious patten was a cycling across rows, but because the pattern lacked regularity no cycle length could be ascertained from a visual inspection of the field response surface.

The spatial correlations started at relatively low values and remained fairly constant within the rows of Table 3.4.7. Within the columns of Table 3.4.7, correlations decreased to a negative correlation at about lag 5 to lag 7. This suggested that there was a minor micro-environmental cycle in the field with a half-cycle length of about 6 units, and that conditions with a row remained relatively constant. There is some indication that diagonal lag correlations decreased faster in  $\hat{\rho}^-$  than in  $\hat{\rho}^+$ , suggesting slight skewness of the fertility pattern relative to the sides of the field.

The matrix of  $STMSE(ac/AC)$ , shown in Table 3.4.11, revealed a faster increase in variance along columns than along rows. For example, a 4 X 1 plot was better than either a 2 X 2 or a 1 X 4. The advantage of orienting plot length with columns became even greater as plot length increased. A 8 X 1 plot is 47 % more efficient than a 4 X 2 plot, 90.6 % more efficient than a 2 X 4 plot and 132 % more efficient than a 1 X 8 plot. In this field, very little penalty would be paid, in STMSE by doubling plot size from 5 X C to 10 X C. This is because the negative correlations of lags greater than about three offset the impact of the earlier positive correlations.

The overall behavior of STMSE was shown by graphing  $\ln \{STMSE(ac/AC)/ac\}$  versus  $\ln (ac)$  using only the border rows and columns of STMSE for simplicity. Independent units would give a line with slope  $- 1.0$ . If Smith's model holds, all points would fall about a line with slope  $- b$ . If the two-dimensional model holds the graph would be a parallelogram with the slopes for all columns being  $- b_1$  and those for all rows being  $- b_2$ . For the Rice data (Fig.3.4.12), the graphs of rows were reasonably linear but showed a gradual change in slope from  $- 0.625$  for row 1 to  $- 0.57$  for row 11. The graphs of columns showed a upward curvature, reflecting the impact of the negative lag correlations, with the average slope changing from  $- 1.04$  for column 1 to  $- 0.99$  for column 9. The patterns of change in  $\hat{\rho}^+$  and  $\hat{\rho}^-$  differed appreciably, there were sizeable negative correlations, was a clear tendency for the correlations to cycle back to positive values, some nearly as large as the lag-one correlations. The first row of  $\hat{\rho}^-$  showed a slow decay relative to the decay from  $\hat{\rho}(0,0) = 1$  to  $\hat{\rho}^-(1,0)$  and the first column of  $\hat{\rho}^-$  showed a very strong cycle from positive values at  $l = 1$  to negative at  $l = 4, 5$  and  $7$  and back to positive at  $l = 8, 9$  and  $10$  [see  $\hat{\rho}^-(1,0)$  and  $\hat{\rho}^-(0,k)$ , respectively in Fig. 3.4.10 & 3.4.9]. For reference, the correlation attenuation curves predicted from Smith's model with  $b_1 \cong 0.9$  and  $b_2 \cong 0.6$  are included in Fig.3.4.10 as  $\rho_1(0.9)$  and  $\rho_2(0.6)$ , respectively. These correlation patterns reflect a pattern of 'fertility' ridges running the length of the field with more or less constant performance within any one column.

TABLE 3.4.7: Rice data: Spatial correlation  $R(l, k)$

| l  | k      |        |        |        |        |        |        |        |        |  |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|--|
|    | -8     | -7     | -6     | -5     | -4     | -3     | -2     | -1     | 0      |  |
| 0  | 0.101  | 0.065  | 0.054  | 0.139  | 0.056  | 0.214  | 0.206  | 0.195  | 1.000  |  |
| 1  | 0.012  | 0.028  | -0.081 | -0.097 | 0.067  | 0.037  | 0.04   | 0.07   | -0.039 |  |
| 2  | -0.052 | -0.102 | -0.018 | -0.013 | -0.097 | -0.059 | -0.021 | 0.063  | 0.035  |  |
| 3  | 0.037  | -0.018 | -0.06  | -0.016 | 0.021  | -0.062 | -0.015 | -0.029 | 0.029  |  |
| 4  | -0.056 | -0.05  | 0.119  | -0.094 | -0.069 | -0.002 | -0.17  | -0.074 | -0.041 |  |
| 5  | 0.017  | 0.055  | -0.057 | 0.008  | -0.021 | -0.077 | -0.035 | -0.043 | -0.107 |  |
| 6  | -0.036 | 0.073  | 0.075  | 0.061  | -0.012 | -0.056 | 0.076  | 0.014  | 0.063  |  |
| 7  | -0.02  | -0.007 | 0.119  | 0.032  | 0      | -0.064 | -0.004 | -0.131 | -0.093 |  |
| 8  | -0.059 | -0.026 | -0.124 | -0.15  | -0.013 | 0.107  | 0.074  | 0.17   | 0.08   |  |
| 9  | 0.057  | 0.048  | -0.092 | 0.112  | 0.183  | -0.022 | 0.134  | 0.126  | 0.005  |  |
| 10 | -0.037 | 0.029  | 0.004  | 0.048  | 0.01   | 0.005  | 0.005  | -0.013 | 0.113  |  |

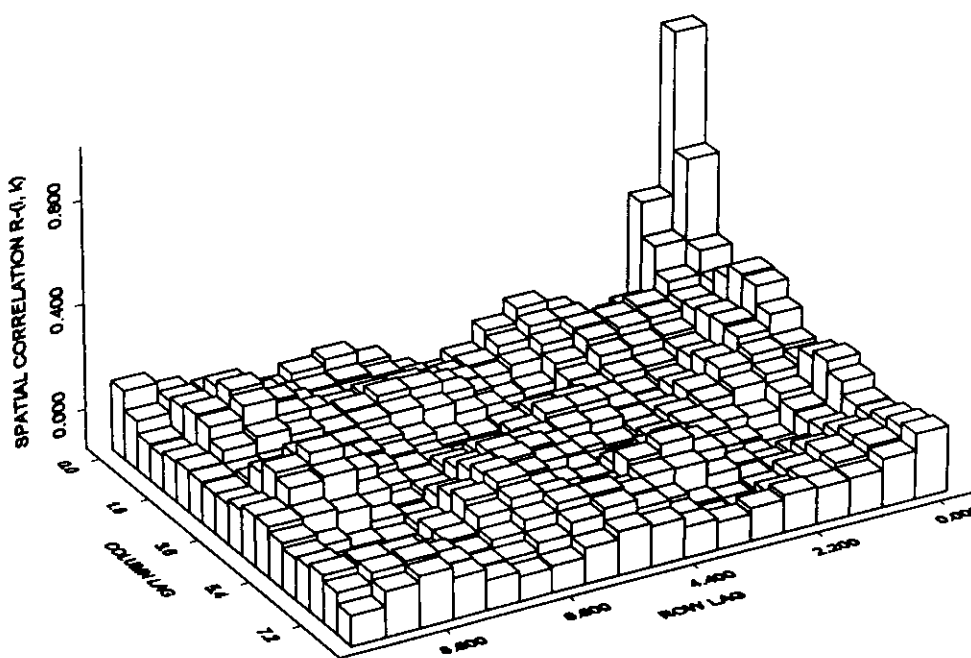


Fig. 3.4.7 (Rice data) Spatial correlation surface  $R(l, k)$  for different row and column lags.

TABLE 3.4.8: Rice data: Spatial correlation  $R+(l, k)$

| l  | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 0  | 1      | 0.195  | 0.206  | 0.214  | 0.056  | 0.139  | 0.054  | 0.065  | 0.101  |
| 1  | -0.039 | 0.084  | 0.031  | 0.052  | 0.037  | 0.081  | 0.094  | 0.096  | -0.018 |
| 2  | 0.035  | -0.016 | 0.062  | 0.029  | 0.057  | 0.009  | 0.049  | 0.064  | 0.07   |
| 3  | 0.029  | 0.065  | -0.002 | 0.034  | 0.191  | 0.087  | 0.068  | 0.126  | 0.042  |
| 4  | -0.041 | -0.075 | 0.056  | -0.041 | -0.024 | 0.005  | -0.049 | 0.065  | 0.02   |
| 5  | -0.107 | -0.064 | -0.013 | -0.102 | -0.046 | 0.004  | 0.03   | 0.117  | 0.117  |
| 6  | 0.063  | 0.031  | -0.025 | -0.004 | -0.105 | -0.031 | 0.067  | 0.06   | 0.046  |
| 7  | -0.093 | -0.043 | -0.147 | -0.17  | -0.028 | -0.085 | -0.064 | -0.052 | 0.011  |
| 8  | 0.08   | 0.032  | -0.065 | 0.006  | -0.089 | 0.01   | 0.031  | -0.037 | -0.222 |
| 9  | 0.005  | 0.069  | 0.125  | -0.01  | 0.205  | 0.005  | 0.088  | 0.035  | -0.033 |
| 10 | 0.113  | 0.071  | 0.014  | 0.077  | -0.076 | 0.043  | -0.091 | -0.008 | 0.097  |

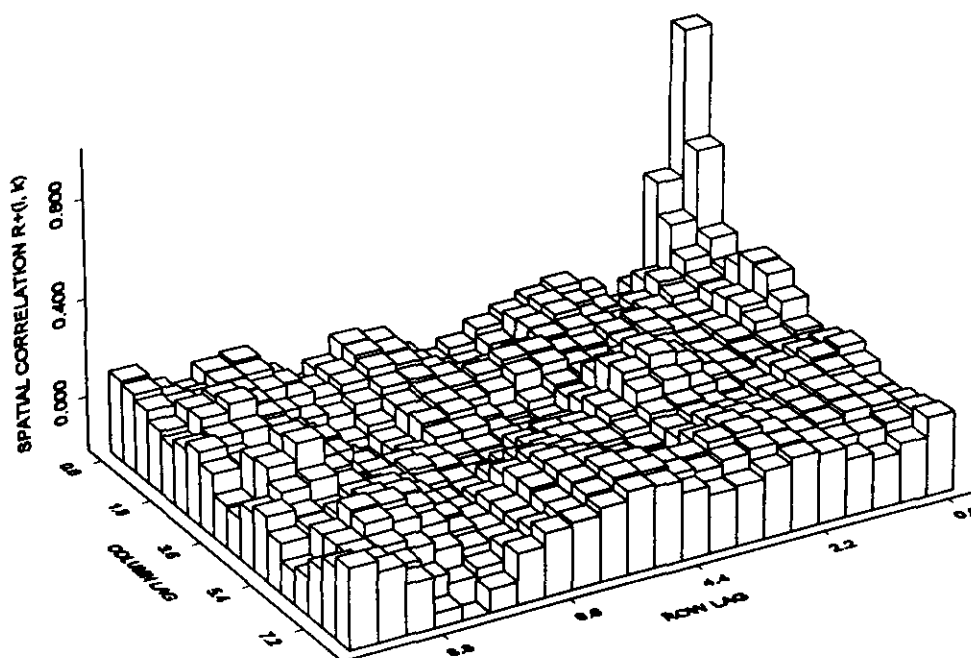


Fig.3.4.8 (Rice data) Spatial correlation surface  $R+(l, k)$  for different row and column lags.

PLOT OF 1ST ROW OF SPATIAL CORRELATION OF RICE DATA

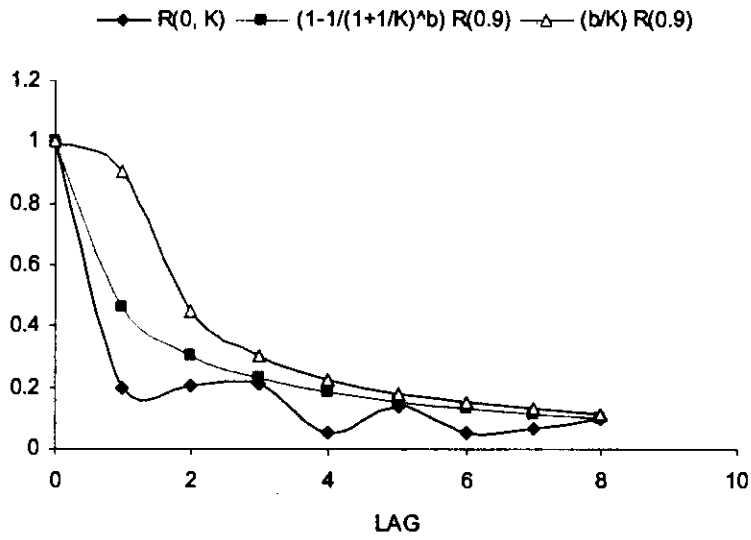


Fig. 3.4.9: Plot of first row of spatial correlation matrix.

PLOT OF 1ST COLUMN OF SPATIAL CORRELATION FOR RICE DATA

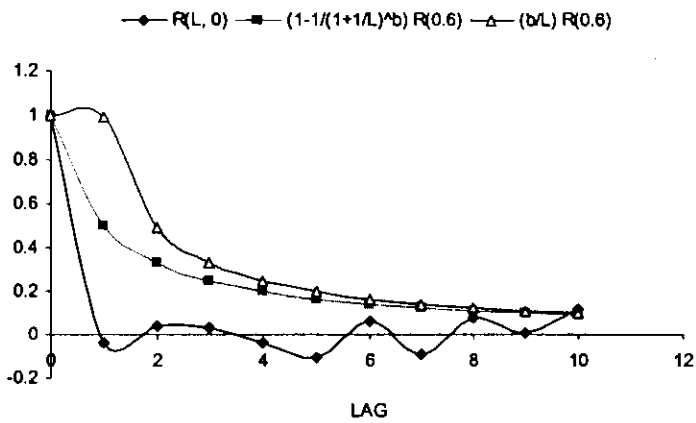


Fig. 3.4.10: Plot of the correlation attenuation curve for rows and columns for rice data.

TABLE 3.4.9: Average Spatial correlation R(l,k)

| l  | K      |        |        |        |        |        |        |        |        |
|----|--------|--------|--------|--------|--------|--------|--------|--------|--------|
|    | 0      | 1      | 2      | 3      | 4      | 5      | 6      | 7      | 8      |
| 0  | 1.000  | 0.195  | 0.206  | 0.214  | 0.056  | 0.139  | 0.054  | 0.065  | 0.101  |
| 1  | -0.039 | 0.077  | 0.035  | 0.045  | 0.052  | -0.008 | 0.006  | 0.062  | -0.003 |
| 2  | 0.035  | 0.024  | 0.021  | -0.015 | -0.020 | -0.002 | 0.015  | -0.019 | 0.009  |
| 3  | 0.029  | 0.018  | -0.009 | -0.014 | 0.106  | 0.036  | 0.004  | 0.054  | 0.039  |
| 4  | -0.041 | -0.074 | -0.057 | -0.021 | -0.046 | -0.045 | 0.035  | 0.008  | -0.018 |
| 5  | -0.107 | -0.054 | -0.024 | -0.090 | -0.034 | 0.006  | -0.013 | 0.086  | 0.067  |
| 6  | 0.063  | 0.023  | 0.025  | -0.030 | -0.058 | 0.015  | 0.071  | 0.066  | 0.005  |
| 7  | -0.093 | -0.087 | -0.076 | -0.117 | -0.014 | -0.027 | 0.027  | -0.029 | -0.005 |
| 8  | 0.080  | 0.101  | 0.004  | 0.057  | -0.051 | -0.070 | -0.047 | -0.032 | -0.140 |
| 9  | 0.005  | 0.097  | 0.129  | -0.016 | 0.194  | 0.058  | -0.002 | 0.041  | 0.012  |
| 10 | 0.113  | 0.029  | 0.009  | 0.041  | -0.033 | 0.046  | -0.043 | 0.010  | 0.030  |

TABLE 3.4.10: MSE for plots a x c units

| a  | Number of unit plots, c |          |          |          |          |          |          |          |          |
|----|-------------------------|----------|----------|----------|----------|----------|----------|----------|----------|
|    | 1                       | 2        | 3        | 4        | 5        | 6        | 7        | 8        | 9        |
| 1  | 13988.34                | 16722.78 | 19522.36 | 22372.56 | 24391.87 | 26379.21 | 28013.28 | 29463.74 | 30904.72 |
| 2  | 13445.82                | 17250.38 | 20725.50 | 24210.71 | 26893.61 | 29288.35 | 31239.74 | 33141.07 | 34922.14 |
| 3  | 13586.70                | 17961.08 | 21855.03 | 25586.01 | 28443.99 | 30939.59 | 33012.97 | 35038.39 | 36934.46 |
| 4  | 13857.45                | 18644.59 | 22751.74 | 26563.37 | 29776.52 | 32583.97 | 34916.32 | 37248.09 | 39453.29 |
| 5  | 13794.68                | 18420.95 | 22313.25 | 25944.88 | 29133.66 | 31889.61 | 34259.91 | 36698.39 | 39008.27 |
| 6  | 13259.72                | 17535.93 | 21132.53 | 24369.45 | 27316.52 | 29896.49 | 32174.40 | 34693.39 | 37151.17 |
| 7  | 13110.08                | 17219.14 | 20691.57 | 23637.26 | 26319.83 | 28729.58 | 30984.20 | 33652.75 | 36293.78 |
| 8  | 12695.06                | 16400.25 | 19524.84 | 21938.88 | 24216.63 | 26330.63 | 28470.33 | 31153.96 | 33854.22 |
| 9  | 12608.98                | 16295.03 | 19254.94 | 21387.84 | 23370.78 | 25201.99 | 27176.63 | 29792.23 | 32381.74 |
| 10 | 12553.95                | 16477.66 | 19610.71 | 21651.05 | 23675.52 | 25515.64 | 27523.52 | 30235.20 | 32859.86 |
| 11 | 12775.23                | 16961.51 | 20273.23 | 22303.64 | 24370.54 | 26259.07 | 28294.28 | 31090.66 | 33765.93 |

TABLE 3.4.11: Standardised MSE for plots a x c units

| a  | Number of unit plots, c |       |       |       |       |       |       |       |       |
|----|-------------------------|-------|-------|-------|-------|-------|-------|-------|-------|
|    | 1                       | 2     | 3     | 4     | 5     | 6     | 7     | 8     | 9     |
| 1  | 1.000                   | 1.195 | 1.396 | 1.599 | 1.744 | 1.886 | 2.003 | 2.106 | 2.209 |
| 2  | 0.961                   | 1.233 | 1.482 | 1.731 | 1.923 | 2.094 | 2.233 | 2.369 | 2.497 |
| 3  | 0.971                   | 1.284 | 1.562 | 1.829 | 2.033 | 2.212 | 2.360 | 2.505 | 2.640 |
| 4  | 0.991                   | 1.333 | 1.626 | 1.899 | 2.129 | 2.329 | 2.496 | 2.663 | 2.820 |
| 5  | 0.986                   | 1.317 | 1.595 | 1.855 | 2.083 | 2.280 | 2.449 | 2.623 | 2.789 |
| 6  | 0.948                   | 1.254 | 1.511 | 1.742 | 1.953 | 2.137 | 2.300 | 2.480 | 2.656 |
| 7  | 0.937                   | 1.231 | 1.479 | 1.690 | 1.882 | 2.054 | 2.215 | 2.406 | 2.595 |
| 8  | 0.908                   | 1.172 | 1.396 | 1.568 | 1.731 | 1.882 | 2.035 | 2.227 | 2.420 |
| 9  | 0.901                   | 1.165 | 1.376 | 1.529 | 1.671 | 1.802 | 1.943 | 2.130 | 2.315 |
| 10 | 0.897                   | 1.178 | 1.402 | 1.548 | 1.693 | 1.824 | 1.968 | 2.161 | 2.349 |
| 11 | 0.913                   | 1.213 | 1.449 | 1.594 | 1.742 | 1.877 | 2.023 | 2.223 | 2.414 |

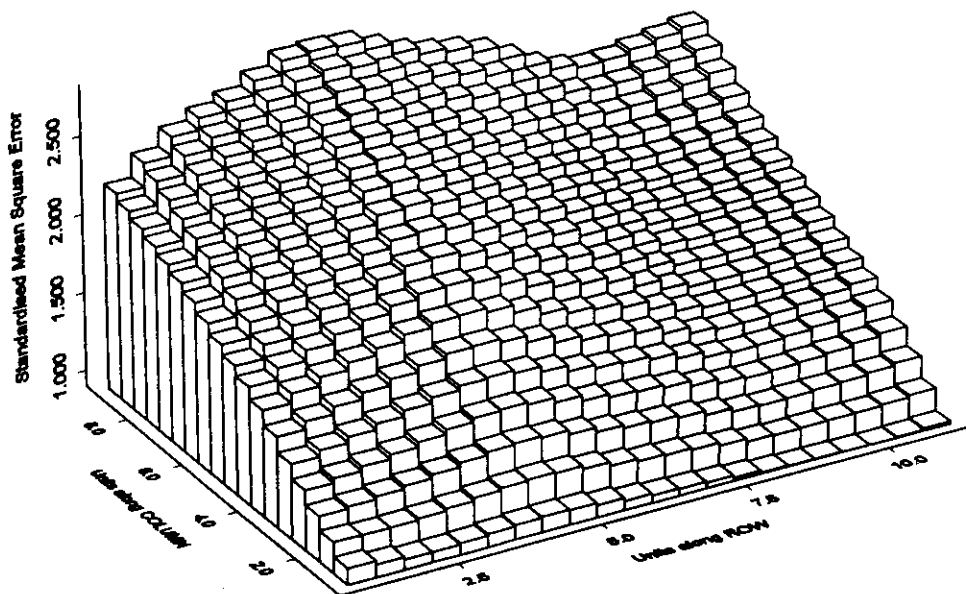


Fig.3.4.11 Three dimensional plot of Standardised Mean Square Error for plots of a x c units

TABLE 3.4.12: Cost per unit of information for plots a x c units for Rice data.

| a  | Number of unit plots, c |          |          |          |          |          |          |          |          |
|----|-------------------------|----------|----------|----------|----------|----------|----------|----------|----------|
|    | 1                       | 2        | 3        | 4        | 5        | 6        | 7        | 8        | 9        |
| 1  | 21069.79                | 14808.69 | 13248.65 | 12868.48 | 12515.96 | 12444.13 | 12386.99 | 12375.21 | 12447.60 |
| 2  | 11906.81                | 9922.24  | 9777.05  | 10168.86 | 10461.08 | 10786.61 | 11043.60 | 11348.42 | 11657.24 |
| 3  | 9220.48                 | 8472.96  | 8802.62  | 9423.07  | 9887.13  | 10327.84 | 10694.69 | 11091.93 | 11479.89 |
| 4  | 7970.67                 | 7831.01  | 8379.24  | 9096.03  | 9734.24  | 10314.94 | 10795.28 | 11309.78 | 11809.29 |
| 5  | 7078.33                 | 7165.38  | 7756.09  | 8481.64  | 9162.42  | 9765.24  | 10288.54 | 10858.14 | 11407.06 |
| 6  | 6255.14                 | 6458.31  | 7054.18  | 7714.51  | 8364.86  | 8948.72  | 9472.05  | 10085.46 | 10693.18 |
| 7  | 5797.05                 | 6087.16  | 6703.12  | 7308.07  | 7904.07  | 8457.91  | 8990.83  | 9658.60  | 10327.20 |
| 8  | 5332.12                 | 5615.90  | 6180.88  | 6661.38  | 7165.10  | 7654.38  | 8171.21  | 8855.10  | 9549.65  |
| 9  | 5078.56                 | 5439.39  | 5984.78  | 6401.88  | 6834.24  | 7253.86  | 7732.97  | 8403.84  | 9072.26  |
| 10 | 4883.24                 | 5386.71  | 6005.19  | 6406.01  | 6858.04  | 7285.48  | 7777.44  | 8476.67  | 9155.85  |
| 11 | <b>4825.13</b>          | 5449.18  | 6131.80  | 6536.16  | 7004.36  | 7448.36  | 7949.62  | 8672.64  | 9365.97  |

TABLE 3.4.13: RICE DATA

| PLOT SIZE  | ln(p)    | STMSE | STMSE/p  | ln(STMSE/p) |
|------------|----------|-------|----------|-------------|
| (Row 1)    |          |       |          |             |
| 2          | 0.693147 | 1.195 | 0.5975   | -0.515      |
| 3          | 1.098612 | 1.396 | 0.465333 | -0.765      |
| 4          | 1.386294 | 1.599 | 0.39975  | -0.91692    |
| 5          | 1.609438 | 1.744 | 0.3488   | -1.05326    |
| 6          | 1.791759 | 1.886 | 0.314333 | -1.1573     |
| 7          | 1.94591  | 2.003 | 0.286143 | -1.25126    |
| 8          | 2.079442 | 2.106 | 0.26325  | -1.33465    |
| 9          | 2.197225 | 2.209 | 0.245444 | -1.40468    |
| (Row 11)   |          |       |          |             |
| 22         | 3.091042 | 1.213 | 0.055136 | -2.89795    |
| 33         | 3.496508 | 1.449 | 0.043909 | -3.12563    |
| 44         | 3.78419  | 1.594 | 0.036227 | -3.31794    |
| 55         | 4.007333 | 1.742 | 0.031673 | -3.4523     |
| 66         | 4.189655 | 1.877 | 0.028439 | -3.55998    |
| 77         | 4.343805 | 2.023 | 0.026273 | -3.63922    |
| 88         | 4.477337 | 2.223 | 0.025261 | -3.67848    |
| 99         | 4.59512  | 2.414 | 0.024384 | -3.71383    |
| (Column 1) |          |       |          |             |
| 2          | 0.693147 | 0.961 | 0.4805   | -0.73293    |
| 3          | 1.098612 | 0.971 | 0.323667 | -1.12804    |
| 4          | 1.386294 | 0.991 | 0.24775  | -1.39534    |
| 5          | 1.609438 | 0.986 | 0.1972   | -1.62354    |
| 6          | 1.791759 | 0.948 | 0.158    | -1.84516    |
| 7          | 1.94591  | 0.937 | 0.133857 | -2.01098    |
| 8          | 2.079442 | 0.908 | 0.1135   | -2.17595    |
| 9          | 2.197225 | 0.901 | 0.100111 | -2.30147    |

|            |          |       |          |          |
|------------|----------|-------|----------|----------|
| 9          | 2.197225 | 0.901 | 0.100111 | -2.30147 |
| 10         | 2.302585 | 0.897 | 0.0897   | -2.41128 |
| 11         | 2.397895 | 0.913 | 0.083    | -2.48891 |
| (Column 9) |          |       |          |          |
| 9          | 2.197225 | 2.209 | 0.245444 | -1.40468 |
| 18         | 2.890372 | 2.497 | 0.138722 | -1.97528 |
| 27         | 3.295837 | 2.64  | 0.097778 | -2.32506 |
| 36         | 3.583519 | 2.82  | 0.078333 | -2.54678 |
| 45         | 3.806663 | 2.789 | 0.061978 | -2.78098 |
| 54         | 3.988984 | 2.656 | 0.049185 | -3.01216 |
| 63         | 4.143135 | 2.595 | 0.04119  | -3.18955 |
| 72         | 4.276666 | 2.42  | 0.033611 | -3.3929  |
| 81         | 4.394449 | 2.315 | 0.02858  | -3.55504 |
| 90         | 4.49981  | 2.349 | 0.0261   | -3.64582 |
| 99         | 4.59512  | 2.414 | 0.024384 | -3.71383 |

### rice data

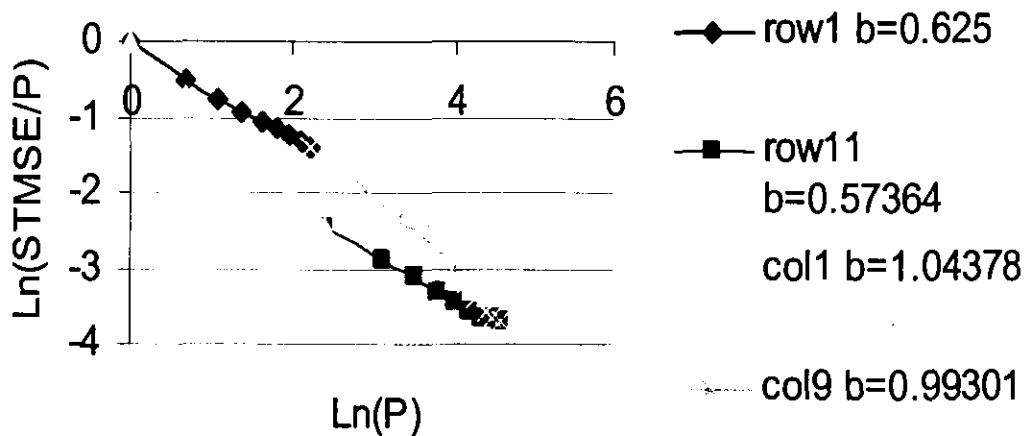


Fig. 3.4.12 Plot of  $\ln(\text{STMSE}/p)$  versus  $\ln(p)$  using the first and last rows and columns of the STMSE matrix from the Rice data.

The changing slopes over rows and columns and the distinct curvature of the graphs (Fig.7) for the rows are clear indications that in this case even two-dimensional version of Smith's model may be inadequate to find the optimum plot size. However we can use the table 3.4.12 containing the cost aspect. It is observed that the cost per unit of information is minimum for 11m. x 1m. plot for the Rice data. However, using M.S.E. matrix we can find C.V. for each plot size and shape. Now using method of maximum curvature optimum plot size for Jute field is 4.02 sq.m. with  $b_1=0.83$ ,  $b_2=1.0$  and  $X_{\text{opt}}=1.28\text{m.} \times 3.13\text{m.}$  & optimum plot size for Rice field is 3.73 sq.m. with  $b_1=1.0$ ,  $b_2=0.77$  and  $X_{\text{opt}}=3.205\text{m.} \times 1.165\text{m.}$

## Chapter 4

### MODELING SPATIAL VARIABILITY

**4.1 INTRODUCTION:** Since the beginning of the application of statistics, observations are assumed to have been taken under identical conditions and they are independent of each other. Here independence is a convenient assumption that makes the analysis / algebra tractable. However, the assumption of independence in real life data is often unrealistic. R.A.Fisher was aware of the spatial dependence of agricultural field experiments. He established the principles of randomizations, blocking and replication. Randomization controls unwanted bias and neutralizes (but does not remove) the effect of spatial correlation. Randomization does not neutralize the spatial correlation at spatial scales larger or smaller than the plot dimensions.

To measure the spatial dependence in a data set we have to see the similarity among data values separated and situated at a particular distance or lag. One quick way to express the similarity or dissimilarity between the paired values is to plot them in a  $Z(s)$  vs  $Z(s+h)$  scattergram. The plot is known as  $h$  scattergram. If the difference between all the  $Z(s)$  and  $Z(s+h)$  values is small, then all the points (scatter of points) will be close to the 45E line and the variable is described as autocorrelated. Alternatively, the larger the difference between the pairs, the more diffuse will be the scatter of points around the 45E or  $Z(s)$  vs  $Z(s+h)$  line. When  $h$  is small the scatter of points will, on average, be tighter; when  $h$  is large, the scatter is typically more diffuse. The tightness or diffuseness of the cloud of points about the 45E line may be thought of as their moment of inertia about the line. If  $s_i$  and  $s_j$  are the co-ordinates for all  $i = 1$  to  $N$  points in an  $h$ -scattergram then the moment of inertia for all points is defined as moment of inertia =

$\frac{1}{2N} \sum_{i=1}^N (s_i - s_j)$ . In other words, the moment of inertia summarizes the spread of the cloud in an  $h$ -scattergram. The  $h$ -scattergram can be useful models of the degree of similarity or dissimilarity between samples separated by a common distance but they are not practical because too many  $h$ -scattergrams would be required to adequately characterize the spatial similarity for all samples and for all  $h$  values. Therefore a meaningful summary of these  $h$ -scattergrams is moment of inertia. Intimately, related to the moment of inertia is one of the most familiar tools in geostatistics: the semivariogram or simply the variogram.

**4.2. Spatial model:** Suppose that the data  $\{Z(s_1), Z(s_2), \dots, Z(s_n)\}$ , observed at known spatial locations  $\{s_1, s_2, \dots, s_n\}$  are modeled as a realization of a partially samples random process  $\{Z(s): s \in D \subset \mathbb{R}^d\}$ . Here the spatial index set  $D$  could have positive Lebesgue measure, be a countable set of points of  $\mathbb{R}^d$ , or be a finite subset of  $\mathbb{R}^d$ . Here let  $Z(s) = \mu(s) + \delta(s)$ ,  $s \in D$  where  $\delta(\cdot)$  is a zero mean error process that is not generally white noise. We call a random variable to be white noise when it is distributed normally, independently, identically with a zero mean and constant variance. The mean process  $\mu(\cdot) = E(Z(\cdot))$  is assumed to be made up of spatial trend, exogenous variables and treatment effects  $\alpha$  (should different treatments be applied at different locations throughout  $D$ ) and will be called large scale variation. The error process is assumed to contain no treatment component, and as such is only of consequence in how it affects efficient estimation of  $\tau$ , the treatment contrasts. We can assume and decompose  $\delta(\cdot)$  as  $\delta(s) = W(s) + \eta(s) + \varepsilon(s)$ ,  $s \in D$ .  $W(\cdot)$  is a zero mean  $L_2$  continuous [i.e.  $E(W(s+h) - W(s))^2 \rightarrow 0$  as  $\|h\| \rightarrow 0$ .] intrinsically stationary process whose variogram range is larger than  $\min\{\|s_i - s_j\| : 1 \leq i < j \leq n\}$ . Here  $W(\cdot)$  is called the smooth scale variation.  $\eta(\cdot)$  is a zero mean, intrinsically stationary process, independent of  $W$  whose variogram range exists and is smaller than  $\min\{\|s_i - s_j\| : 1 \leq i < j \leq n\}$ . Here  $\eta(\cdot)$  is called the micro scale variation and its variance is called  $C_{MS}$ .  $\varepsilon(\cdot)$  is a zero mean white noise process independent of  $W(\cdot)$  and  $\eta(\cdot)$ .  $\eta(\cdot)$  is also called the measurement error and its variance is called  $C_{ME}$ . Here we assume that the error process  $\delta(\cdot)$  is intrinsically stationary. The intrinsic stationarity can be defined through first differences as  $E(Z(s+h) - Z(s)) = 0$  and  $\text{Var}(Z(s+h) - Z(s)) = 2\gamma(h)$  where  $\{Z(s): s \in D\}$  and  $h = (s_i - s_j)$ . The quantity  $2\gamma(h)$  is known as variogram and  $\gamma(h)$  is called the semivariogram. Alternatively this means that  $E(\delta(s_1) - \delta(s_2))^2 = 2\gamma(s_1 - s_2)$  where  $s_1, s_2 \in D$ . The classical estimator of variogram  $2\gamma(h)$  is a crucial parameter. The classical estimator of the variogram as

proposed by Matheron (1963) is 
$$2\hat{\gamma}(h) \equiv \frac{1}{|N(h)|} \sum_{N(h)} (Z(s_i) - Z(s_j))^2$$
 where sum is over

$N(h) \equiv \{(i, j) : s_i - s_j = h\}$  and  $|N(h)|$  is the number of distinct elements of  $N(h)$ . Cressie and

Hawkins(1980) present a more robust approach to the estimation of variogram :

$$2.\bar{\gamma}(h) \equiv \frac{\left\{ \frac{1}{|N(h)|} \sum_{N(h)} |Z(s_i) - Z(s_j)|^{1/2} \right\}^4}{\left( 0.457 + \frac{0.494}{|N(h)|} \right)}$$

Here the word “robust” is used to describe inference procedures that are stable when model assumptions depart from those of a central model. In case of above robust estimator Cressie and Hawkins (1980) use the available knowledge of robust *location* estimation and take fourth roots of squared differences. Thus the estimator is robust to contamination by outliers (Hawkins and Cressie, 1984). Another robust estimator is

$$2.\tilde{\gamma}(h) \equiv \left[ \text{med} \left\{ |Z(s_i) - Z(s_j)|^{1/2} : (s_i - s_j) \in N(h) \right\} \right]^4 / B(h)$$

where  $\text{med}(\cdot)$  denotes the median of the sequence  $\{.\}$  and  $B(h)$  corrects for bias [ asymptotically,  $B(h) = 0.457$  ]. The variogram must satisfy a property called conditional negative definiteness i.e.  $\sum_{i=1}^m \sum_{j=1}^m a_i a_j .2\gamma(s_i - s_j) \leq 0$  for any

finite number of spatial locations  $(s_i: i = 1,2,\dots,m)$  and real numbers  $(a_i: i = 1, 2,\dots,m)$  satisfying  $\sum_{i=1}^m a_i = 0$ . The function  $C(\cdot) = C(s_i - s_j) = \text{Cov}(Z(s_i), Z(s_j))$  is called a covariogram.

Now,

$$2.\gamma(h) = \text{var} (Z(s_i) - Z(s_j))$$

$$\text{or, } 2.\gamma(h) = \text{var} (Z(s_i)) + \text{var} (Z(s_j)) - 2.\text{cov}(Z(s_i), Z(s_j))$$

$$\text{or, } 2.\gamma(h) = 2.C(0) - 2.C(h) = 2.(C(0) - C(h))$$

where  $C(0) = \text{var} (Z(s))$ . Here the semivariogram is very simply related to covariogram. If  $C(h) \rightarrow 0$  as  $\|h\| \rightarrow 4$  [ e.g. when  $Z(\cdot)$  is a stationary ergodic Gaussian process], then  $2.\gamma(h) \rightarrow 2.(C(0))$

i.e.  $.\gamma(h) \rightarrow C(0)$ ; the quantity  $C(0)$  is called the *sill* of the semivariogram. Moreover any vector  $r_0$  for which  $\gamma(r_0(1+\epsilon)) = C(0)$  for any  $\epsilon > 0$  is called the range of the variogram in the direction

$r_0 / \|r_0\|$ . This means the correlation between  $Z(s)$  and  $Z(s + (h.r_0 / \|r_0\|))$  is zero for all  $h \geq \|r_0\|$ .

Here if  $2.\gamma(s_i - s_j)$  is a function of only of  $\|s_i - s_j\|$ , it is called *isotropic*. Clearly  $\gamma(-h) = \gamma(h)$  and

$\gamma(0) = 0$ . If  $\gamma(h) \rightarrow C_0 > 0$  as  $h \rightarrow 0$ , then  $C_0$  was called the nugget effect by Matheron(1962). This

component of the semivariogram is often used to model micro scale variation (small nuggets) and causes a discontinuity at the origin. More generally the nugget effect is made up of two components  $C_0 = C_{MS} + C_{ME}$  where  $C_{MS}$  represents the variance of a white noise process used to model the noncontinuous micro scale variation of the physical process and  $C_{ME}$  represents the variance of a white noise process used to model measurement error i.e. error resulting from doing the measurement several times and not being able to obtain exactly the same result.

**4.3. Spatial modeling of uniformity data:** Let the model be  $Z(s) = \mu(s) + \delta(s)$ . The most common problems in statistical analysis involve inference on the large scale variation  $\mu(\cdot)$ . Usually  $\delta(\cdot)$  is assumed to be white noise. Modelling and fitting spatial dependence parameters from the data allows for efficient estimation of the parameters in  $\mu(\cdot)$ . Besag(1977) illustrated use of modeling spatial or temporal correlation in error process  $\delta(\cdot)$  for the efficient estimation of  $\mu(\cdot)$ . To illustrate and to obtain a true model for spatial variation responses from the uniformity trials shall be used. By treating the uniformity data as a spatial data we can write the data as  $\{Z(i(1.0), j(1.0)): i = 1, 2, \dots, R; j = 1, 2, \dots, C\}$ . Here each unit plot is a square plot of area 1mt. X 1mt. We denote  $Z(i,j)$ , the  $(i,j)$ -th data where  $i = 1$  corresponds to the most Easterly row and  $j = 1$  corresponds to the most Northerly column. Considering the two way layout of the plots we can propose the stochastic model  $Z(i,j) = a + r_i + c_j + \delta(i,j)$ . Now we can estimate the mean process i.e.  $\mu(s) = a + r_i + c_j$  (where  $s = (i,j)$ ) by *median polish*. Assuming one observation per grid node o.l.s. estimators of  $a, r_i, c_j$  can be obtained. However its disadvantage is that the residuals  $(Z(s_i) - \hat{\mu}(s_i): i = 1, 2, \dots, n)$  give biased estimators of the unknown spatial dependence in the error process  $\delta(\cdot)$ . But median polish technique is a sensible one. When the distribution of error process is symmetric,  $E(\text{ave}\{Z(s_i): i \in A\}) = E(\text{med}\{Z(s_i): i \in A\})$ . Further,  $\text{med}\{Z(s_i): i \in A\}$  has attractive outlier resistance properties.

**MEDIAN POLISH ALGORITHM:** The median polish algorithm (Emerson and Hoaglin, 1983) that produces the all effect  $\bar{a}$ , the row effects  $\{\underline{r}_k: k = 1, 2, \dots, R\}$  and the column effects  $\{\check{c}_l: l = 1, 2, \dots, C\}$  from a  $p \times q$  array of numbers  $\{Z(i,j): i = 1, 2, \dots, R; j = 1, 2, \dots, C\}$  also gives less biased residuals.

For  $i = 1, 3, 5, \dots$ , define

$$Z_{k,l}^{(i)} \equiv Z_{k,l}^{(i-1)} - \text{med}\{Z_{k,l}^{(i-1)}: l = 1, \dots, C\}, k = 1, \dots, R+1; l = 1, \dots, C$$

$$Z_{k,C+1}^{(i)} \equiv Z_{k,C+1}^{(i-1)} - \text{med} \{ Z_{kl}^{(i-1)} : l = 1, \dots, C \}, k = 1, \dots, R+1;$$

----- (i)

and for  $i = 2, 4, 6, \dots$ , define

$$Z_{k,l}^{(i)} \equiv Z_{k,l}^{(i-1)} - \text{med} \{ Z_{k,l}^{(i-1)} : k = 1, \dots, R \}, k = 1, \dots, R; l = 1, \dots, C+1$$

$$Z_{p+1,l}^{(i)} \equiv Z_{p+1,l}^{(i-1)} + \text{med} \{ Z_{k,l}^{(i-1)} : k = 1, \dots, R \}, l = 1, \dots, C+1;$$

To start the algorithm, assume  $Z_{k,l}^{(0)} = \begin{cases} Z_{k,l} & k = 1, \dots, R; l = 1, \dots, C \\ 0, & \text{elsewhere} \end{cases}$

In words start with  $R \times C$  data and create  $R+C+1$  extra cells with zero in them. Use equations at (i) to remove row medians from the data and accumulate the amounts removed in the  $p$  extra row cells. Do the same to the columns of the table, removing column medians from not only the data but also the column of accumulated row removals. This last amount removed goes into the extra  $(R+1, C+1)$ -th cell. Repeat the process until convergence. Assuming convergence, the estimated effects are

$$\bar{a} \equiv Z_{R+1,C+1}^{\infty}$$

$$\underline{c}_k \equiv Z_{k,C+1}^{\infty}; k = 1, \dots, R$$

$$\check{c}_l \equiv Z_{R+1,C+1}^{\infty}; l = 1, \dots, C$$

with the property that

$$Z_{k,l} = \bar{a} + \underline{c}_k + \check{c}_l + Z_{k,l}^{\infty}; k = 1, \dots, R$$

$$l = 1, \dots, C$$

Thus, the original  $R \times C$  table is replaced with a  $R \times C$  table of residuals.

$\{ Z_{k,l}^{\infty}; k = 1, \dots, R; l = 1, \dots, C \}$  and the  $R + C + 1$  extra cells contain the row effect  $\underline{c}_k$ , the column effect  $\check{c}_l$  and the all effect  $\bar{a}$ . Now observing the row and column effects we can detrend the data as  $R(i,j) = Z(i,j) - \bar{a} - \underline{c}_k - \check{c}_l$ . Now we have to analyse the median-polish residuals  $R(i,j)$  as if they are a sampling from an intrinsically stationary random process. Now these residuals will be used to estimate  $2\gamma(h) = \text{var}(\delta(s+h) - \delta(s))$ . The common variogram models ( $\gamma_u$ ) in terms of a Dimensionless Length  $h/a$  are given in the following table:

**Table 4.3.1:**

| Name        | Function         | Effective range |
|-------------|------------------|-----------------|
| Exponential | $1 - \exp(-h/a)$ | $3.0 a$         |

|                  |   |        |
|------------------|---|--------|
| Spherical        | $1.5 (h/a) - 0.5 (h/a)^3, h < a$<br>$1, h \geq a$ | 0.82 a |
| Gaussian         | $1 - \exp [-(h/a)^2]$                             | 1.7 a  |
| Michaelis-Menton | $(h/a) / [1 + (h/a)]$                             | 19.0 a |
| Linear           | $h/a$   | None   |

As sample support size increases, variance is expected to decrease. With respect to a variogram this would correspond to a decrease in sill. Some other models considered are rational quadratic model, wave model and power model. Various parametric variogram models are presented by Journel and Huijbregts(1978). Here we consider the following basic models:

(i) *Linear model*:  $\gamma(h; \theta) = \begin{cases} 0, & \dots, h = 0 \\ c_o + b_l \|h\|, & \dots, h \neq 0 \end{cases}$

$\theta = (c_o, b_l)'$ , where  $c_o \geq 0$ , and  $b_l \geq 0$ .

(ii) *Spherical model*:  $\gamma(h; \theta) = \begin{cases} 0, & \dots, h = 0, \\ c_o + c_s \{ (3/2)(\|h\|/a_s) - (1/2)(\|h\|/a_s)^3 \}, & \dots, 0 < \|h\| \leq a_s, \\ c_o + c_s, & \dots, \|h\| \geq a_s, \end{cases}$

$\theta = (c_o, c_s, a_s)'$ , where  $c_o \geq 0, c_s \geq 0, a_s \geq 0$ .

(iii) *Exponential model*:  $\gamma(h; \theta) = \begin{cases} 0, & \dots, h = 0 \\ c_o + c_e \{ 1 - \exp(\|h\|/a_e) \}, & \dots, h \neq 0 \end{cases}$

$\theta = (c_o, c_e, a_e)'$ , where  $c_o \geq 0, c_e \geq 0, a_e \geq 0$ .

(iv) *Rational quadratic model*:  $\gamma(h; \theta) = \begin{cases} 0, & \dots, h = 0 \\ c_o + c_r \|h\|^2 / (1 + \|h\|^2 / a_r), & \dots, h \neq 0 \end{cases}$

$\theta = (c_o, c_r, a_r)'$ , where  $c_o \geq 0, c_r \geq 0, a_r \geq 0$ .

(v) *Wave model*:  $\gamma(h; \theta) = \begin{cases} 0, & \dots, h = 0 \\ c_o + c_w \{ 1 - a_w \text{Sin}(\|h\|/a_w) / \|h\| \}, & \dots, h \neq 0 \end{cases}$

$\theta = (c_o, c_w, a_w)'$ , where  $c_o \geq 0, c_w \geq 0, a_w \geq 0$ .

(vi) *Power model*: 
$$\gamma(h; \theta) = \begin{cases} 0, & \dots \dots \dots h = 0 \\ c_o + b_p \|h\|^\lambda, & \dots \dots \dots h \neq 0 \end{cases}$$

$\theta = (c_o, b_p, \lambda)'$ , where  $c_o \geq 0, b_p \geq 0, 0 \leq \lambda < 2$ .

(vii) *Gaussian model*: 
$$\gamma(h; \theta) = \begin{cases} 0, & \dots \dots \dots h = 0 \\ c_o + c_g \{1 - \exp[-(\|h\|/a_g)^2]\}, & \dots \dots \dots h \neq 0 \end{cases}$$

$\theta = (c_o, c_g, a_g)'$ , where  $c_o \geq 0, c_g \geq 0, a_g \geq 0$ .

(viii) *Michaelis-Menton model*: 
$$\gamma(h; \theta) = \begin{cases} 0, & \dots \dots \dots h = 0 \\ c_o + c_m (\|h\|/a_m)/(1 + \|h\|/a_m), & \dots \dots \dots h \neq 0 \end{cases}$$

$\theta = (c_o, c_m, a_m)'$ , where  $c_o \geq 0, c_m \geq 0, a_m \geq 0$ .

**4.4 RESULTS OF VARIGRAM MODEL FITTINGS:** The following is the result of different variogram model fittings through nonlinear regression techniques. The asymptotic standard errors of the parameters is displayed (StdErr.) in column three. The standard errors and coefficients of variation can be used as a gauge of the fitted curve's accuracy. The parameter coefficients of variation, expressed as a percentage, are displayed [CV(%)] in column four. This is the normalized version of the standard errors i.e. CV% = standard error \* (100/ parameter value). The coefficient of variation values and standard errors (see above) can be used as a gauge of the accuracy of the fitted curve. The last column shows the parameter dependencies. Parameters with dependencies near 1 are strongly dependent on one another. This may indicate that the equation(s) used are too complicated and "over-parameterized"—too many parameters are being used, and a model with fewer parameters may be better. Dependencies are used to determine when the data has been "over-parameterized." Too many parameters result in dependencies very near 1.0. If a mathematical model contains too many parameters, a less complex model may be found that adequately describes the data. Dependencies near 1.0 (0.999 for example) indicate that the equation uses too many parameters. If two parameters are dependent on one another, one can probably use an equation with one less parameter. 'Converged, tolerance satisfied' message appears when the convergence criterion, which compares the relative change in the norm to the specified tolerance, is satisfied. This is to be noted that result may still be a false or local minimum. Hence choice of the initial parameter value is important in fitting of nonlinear

regression. By observing the actual data, fitting a linear equation and from experience we are able to find a suitable guess for initial parameter values of our data.

**JUTE DATA**

Plot size (1X1) Average variogram (Spherical model)      Rsquare =0.75008

| Parameter | Value     | StdErr   | CV(%)    | Dependencies |
|-----------|-----------|----------|----------|--------------|
| a         | -6.669e-1 | 2.045e+2 | 3.067e+4 | 0.9850332    |
| b         | 2.825e+3  | 2.060e+2 | 7.291e+0 | 0.9849500    |
| c         | 1.569e+0  | 1.888e-1 | 1.204e+1 | 0.0437719    |

**EXPONENTIAL MODEL FITTING**     $y = a - b.exp(-x/c)$

1X1plot      Rsq.= 0.747920763

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.828e+3 | 2.603e+1 | 9.204e-1 | 0.0677606    |
| b         | 2.832e+3 | 2.071e+2 | 7.314e+0 | 0.0368422    |
| c         | 5.157e-1 | 1.126e-1 | 2.182e+1 | 0.0678951    |

**JUTE DATA GAUSSIAN MODEL**     $y = a - b.exp[-(x/c)^2]$

1 X 1 plot      Rsq.= 0.749893722

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.825e+3 | 2.554e+1 | 9.039e-1 | 0.0392436    |
| b         | 2.826e+3 | 2.063e+2 | 7.300e+0 | 0.0426184    |
| c         | 7.514e-1 | 8.753e-2 | 1.165e+1 | 0.0465566    |

**MICHAELIS-MENTON MODEL FITTING**     $y = a - b / (1+x/c)$

1X1plot      Rsq.= 0.741325044

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.869e+3 | 4.001e+1 | 1.395e+0 | 0.5951695    |
| b         | 2.870e+3 | 2.119e+2 | 7.384e+0 | 0.0700972    |
| c         | 1.153e-1 | 6.949e-2 | 6.027e+1 | 0.5811760    |

**VB (1X1) MODEL FITTING**     $y = li*(1-exp(-k*(t-t0)))$     Rsquare =0.748515357

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| li        | 2.826e+3 | 2.640e+1 | 9.343e-1 | 0.0488314    |
| k         | 1.948e+0 | 4.151e-1 | 2.131e+1 | 0.0708874    |

t0      7.606e-4      3.807e-2                      5.005e+3      0.0240221

Plot size (3X4) Average variogram (Spherical model) Rsquare =0.997048

| Parameter | Value     | StdErr   | CV(%)    | Dependencies |
|-----------|-----------|----------|----------|--------------|
| a         | -3.972e+0 | 3.655e+1 | 9.202e+2 | 0.7261903    |
| b         | 1.430e+5  | 3.377e+8 | 2.362e+5 | 1.0000000    |
| c         | 6.821e+2  | 1.611e+6 | 2.362e+5 | 1.0000000    |

Plot size (1X9) Average variogram (Spherical model) Rsquare =0.144939

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 3.201e+2 | 9.930e+1 | 3.102e+1 | 0.8311002    |
| b         | 1.993e+2 | 1.343e+2 | 6.738e+1 | 0.8262073    |
| c         | 9.644e+0 | 1.683e+0 | 1.745e+1 | 0.0906206    |

1 X 5 plot      Exponential model    Rsq.= 0.80138329

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 8.573e+2 | 3.767e+1 | 4.394e+0 | 0.3417261    |
| b         | 8.120e+2 | 1.201e+2 | 1.479e+1 | 0.2152217    |
| c         | 1.228e+0 | 3.983e-1 | 3.244e+1 | 0.3341955    |

1 X 9 plot                      Exponential model    Rsq.= 0.520408977

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 4.775e+2 | 3.207e+1 | 6.717e+0 | 0.1250416    |
| b         | 4.651e+2 | 1.242e+2 | 2.670e+1 | 0.0666696    |
| c         | 6.579e-2 | 2.121e+1 | 3.224e+4 | 0.0666904    |

3 X 4 plot                      Exponential model    Rsq.= 0.997047272

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 5.410e+6 | 2.706e+3 | 5.002e-2 | 0.9999500    |
| b         | 5.410e+6 | 2.706e+3 | 5.002e-2 | 0.9999500    |
| c         | 1.720e+4 | 6.892e+2 | 4.006e+0 | 0.6428947    |

2 X 4 plot                      Gaussian model    Rsq.= 0.926215626

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 3.772e+2 | 2.527e+1 | 6.698e+0 | 0.4560605    |
| b         | 3.577e+2 | 5.147e+1 | 1.439e+1 | 0.3479337    |

c 1.453e+0 3.032e-1 2.087e+1 0.3678394

7 X 1 plot Gaussian model Rsq.= 0.765057035

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 5.351e+3 | 5.627e+2 | 1.052e+1 | 0.4462170    |
| b         | 5.133e+3 | 1.278e+3 | 2.491e+1 | 0.2716941    |
| c         | 1.037e+0 | 3.099e-1 | 2.989e+1 | 0.3492266    |

1 X 5 plot Michaelis-menton model Rsq.= 0.835191808

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 9.197e+2 | 5.445e+1 | 5.920e+0 | 0.7384739    |
| b         | 9.122e+2 | 1.170e+2 | 1.283e+1 | 0.3543180    |
| c         | 6.338e-1 | 3.305e-1 | 5.215e+1 | 0.6895369    |

2 X 9 plot Michaelis-menton model Rsq.= 0.831729125

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.058e+2 | 4.820e+1 | 2.343e+1 | 0.9534801    |
| b         | 2.022e+2 | 5.060e+1 | 2.503e+1 | 0.8259530    |
| c         | 1.650e+0 | 1.419e+0 | 8.602e+1 | 0.9050725    |

3 X 4 plot Michaelis-menton model Rsq.= 0.997047527

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 1.289e+7 | 2.706e+3 | 2.099e-2 | 0.9999500    |
| b         | 1.289e+7 | 2.706e+3 | 2.099e-2 | 0.9999500    |
| c         | 4.099e+4 | 1.625e+3 | 3.964e+0 | 0.6428697    |

JUTE DATA (Plot size: 1 X 1)

VB Model fit  $y = li*(1-\exp(-k*(t-t_0)))$

PLOT SIZE 1 X 5 Rsq.= 0.801400488

| Parameter | Value     | StdErr   | CV(%)    | Dependencies |
|-----------|-----------|----------|----------|--------------|
| li        | 8.584e+2  | 3.803e+1 | 4.430e+0 | 0.2353937    |
| k         | 7.976e-1  | 2.582e-1 | 3.237e+1 | 0.4146764    |
| t0        | -7.252e-2 | 1.917e-1 | 2.643e+2 | 0.2624308    |

PLOT SIZE 2 X 9 Rsq.= 0.828658671

| Parameter | Value     | StdErr   | CV(%)             | Dependencies |
|-----------|-----------|----------|-------------------|--------------|
| li        | 1.707e+2  | 2.741e+1 | 1.606e+1          | 0.7497911    |
| k         | 5.070e-1  |          | 2.849e-1 5.620e+1 | 0.8093811    |
| t0        | -9.577e-2 |          | 3.748e-1 3.913e+2 | 0.4015472    |

PLOT SIZE 3 X 5

Rsq.= 0.982025531

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| li        | 1.731e+4 | 2.821e+5 | 1.629e+3 | 0.9999781    |
| k         | 1.530e-2 | 3.009e-1 | 1.967e+3 | 0.9999782    |
| t0        | 6.471e-2 | 2.669e-1 | 4.124e+2 | 0.6824447    |

**Rice data**

RICE DATA(22 x 18) SPHERICAL MODEL

\*\*\*\*\*

Plot size= 1X1 considering value of variogram zero at lag distance zero.

(Average) Rsquare= 0.7393

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 5.304e+0 | 1.924e+3 | 3.627e+4 | 0.9824561    |
| b         | 2.400e+4 | 1.941e+3 | 8.087e+0 | 0.9824286    |
| c         | 1.251e+0 | 2.375e-1 | 1.899e+1 | 0.0188417    |

Plot size (4X1) (specify zero value at lag distance zero)

Variogram Rsquare=0.2539 (deleting some outliers)

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.350e+4 | 1.100e+4 | 4.679e+1 | 0.8652831    |
| b         | 2.389e+4 | 1.403e+4 | 5.870e+1 | 0.8454202    |
| c         | 4.652e+0 | 5.340e-1 | 1.148e+1 | 0.3405543    |

Plot size (7X1) (specify zero value at lag distance zero)

Variogram(+ve) Rsquare=0.60456

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 5.733e+4 | 3.955e+4 | 6.899e+1 | 0.7767580    |
| b         | 1.444e+5 | 5.870e+4 | 4.064e+1 | 0.7765686    |
| c         | 4.641e+0 | 5.156e-1 | 1.111e+1 | 0.1322368    |

RICE DATA

EXPONENTIAL MODEL FITTING  $y = a - b \cdot \exp(-x/c)$

1 X 1 plot Rsqu.= 0.743520975

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.406e+4 | 2.620e+2 | 1.089e+0 | 0.0689071    |
| b         | 2.401e+4 | 1.925e+3 | 8.019e+0 | 0.0294025    |
| c         | 4.466e-1 | 1.313e-1 | 2.940e+1 | 0.0579423    |

3 X 4 plot Rsqu.= 0.969082944

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.680e+4 | 2.863e+3 | 1.068e+1 | 0.5008269    |
| b         | 2.611e+4 | 4.956e+3 | 1.898e+1 | 0.3337013    |
| c         | 3.449e-2 | 8.631e+3 | 2.503e+7 | 0.3344359    |

5 X 3 plot Rsqu.= 0.838761915

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 5.742e+4 | 5.358e+4 | 9.331e+1 | 0.9765797    |
| b         | 5.682e+4 | 5.425e+4 | 9.546e+1 | 0.9255816    |
| c         | 1.050e+0 | 2.234e+0 | 2.127e+2 | 0.9460384    |

RICE DATA GAUSSIAN MODEL

1 X 1 plot Rsqu.= 0.739834638

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.401e+4 | 2.598e+2 | 1.082e+0 | 0.0399447    |
| b         | 2.401e+4 | 1.939e+3 | 8.079e+0 | 0.0228372    |
| c         | 6.092e-1 | 1.307e-1 | 2.146e+1 | 0.0251401    |

3 X 4 plot Rsqu.= 0.62834579

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.019e+4 | 9.522e+3 | 4.717e+1 | 0.5000022    |
| b         | 1.936e+4 | 1.649e+4 | 8.518e+1 | 0.3333343    |
| c         | 1.326e-1 | 4.099e+3 | 3.090e+6 | 0.3333353    |

**RICE DATA:** The nonlinear fit for each model for different plot sizes and shapes for Rice field.

MICHAELIS-MENTON MODEL FITTING  $y = a - b / (1+x/c)$

1X1plot Rsqu.= 0.74668923

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.443e+4 | 4.147e+2 | 1.698e+0 | 0.6330444    |
| b         | 2.443e+4 | 1.939e+3 | 7.939e+0 | 0.0731899    |
| c         | 1.017e-1 | 7.696e-2 | 7.566e+1 | 0.6174203    |

3 X 3 plot Rsqu.= 0.741799083

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 4.400e+4 | 3.459e+4 | 7.863e+1 | 0.9728021    |
| b         | 4.387e+4 | 3.645e+4 | 8.309e+1 | 0.8995999    |
| c         | 4.641e-1 | 1.607e+0 | 3.463e+2 | 0.9444143    |

3 X 4 plot Rsqu.= 0.799663134

| Parameter | Value     | StdErr   | CV(%)    | Dependencies |
|-----------|-----------|----------|----------|--------------|
| a         | 1.530e+4  | 1.103e+4 | 7.209e+1 | 0.7667423    |
| b         | 1.506e+4  | 1.440e+4 | 9.560e+1 | 0.7377259    |
| c         | -4.682e-1 | 5.186e-1 | 1.108e+2 | 0.8803511    |

#### RICE DATA VB model

PLOT SIZE 1 x 1 Rsqu.=0.743524413

| Parameter | Value     | StdErr   | CV(%)    | Dependencies |
|-----------|-----------|----------|----------|--------------|
| li        | 2.406e+4  | 2.623e+2 | 1.090e+0 | 0.0490000    |
| k         | 2.212e+0  | 6.106e-1 | 2.760e+1 | 0.0646307    |
| t0        | -1.112e-3 | 3.657e-2 | 3.290e+3 | 0.0169929    |

PLOT SIZE 3 x 1 Rsqu.=0.425702768

| Parameter | Value     | StdErr   | CV(%)     | Dependencies |
|-----------|-----------|----------|-----------|--------------|
| li        | 1.054e+4  | 6.550e+3 | 6.211e+1  | 0.0991765    |
| k         | 4.818e+0  | 3.357e+9 | 6.968e+10 | 0.9999985    |
| t0        | -2.240e+0 | 1.559e+9 | 6.961e+10 | 0.9999985    |

PLOT SIZE 5 x 3 Rsqu.=0.838750937

| Parameter | Value     | StdErr   | CV(%)    | Dependencies |
|-----------|-----------|----------|----------|--------------|
| li        | 5.749e+4  | 5.392e+4 | 9.378e+1 | 0.9450076    |
| k         | 9.492e-1  | 2.101e+0 | 2.213e+2 | 0.9473917    |
| t0        | -1.105e-2 | 3.043e-1 | 2.755e+3 | 0.2073947    |

**4.5 Relating variogram parameters to plot and block size and shape:** Soil heterogeneity complicates the design and analysis of field experiments. A variety of complicated block designs are developed to tackle such heterogeneity in the experimental materials. Generally analysis of experimental results supposes that residuals are spatially independent. But in field experiments strong spatial autocorrelation of soil properties is observed. To overcome the effect of spatial dependence of soil properties, plots are randomized within blocks. Randomisation of plots within blocks is expected to equalize error over all treatment differences thus allowing the use of usual statistical methods of analysis. However, the underlying hypothesis is that spatial variability is random; i.e., spatially unstructured within blocks. But, in the presence of a significant spatial correlation over small distances, the assumption of independence between plots is violated. In such a situation, a field researcher may be faced with contradictory results: clear difference in crop yields between experimental plots but no significant treatment effect. One way to tackle such spatial correlation is to study and analyse the structure of spatial variability of crop yield data obtained from uniformity trials. Using variogram parameters like nugget, sill and range we can investigate the optimal experimental plot size and shape and the configuration of blocks. Here it is understood that the range is the separation distance beyond which two observations are independent of each other. The sill is the variogram value corresponding to the range. The discontinuity at the origin is called the nugget effect and arises from a combination of random errors and sources of variation at distances smaller than the shortest sampling interval (Goovaerts, 1998). The nugget/sill ratio (**NSR**) can be used as a criterion indicating the extent to which the experimental errors between plots were randomly distributed in space (Bhatti *et al.*, 1991; Ersboll, 1996). We find **NSR** for every plot configuration studied. The determination criteria is that the smaller the **NSR**, the less random errors remain between plots; thus the less the plot configuration meets the condition that experimental errors can be considered to be random. Conversely, the largest **NSR** represents the configuration which best meets the underlying hypothesis of classical ANOVA techniques (Fagroud *et al.*, 2002). Similarly we can also study

for block configuration. So far parameters of the variogram model of plot observations are summarized in the NSR ratio. Since the ranges of the variogram models greatly differ, this NSR ratio is standardized as NSR/Range by Fagroud *et al*(2002) for studying the best block configuration. From the plot of NSR/Range vs. number of plots per block the ratio NSR/Range indicates that the optimal number of plots per block should be neither too high (i.e. NSR small) nor too small (i.e. significant spatial correlation) since it represents a compromise between two parameter requirements indicating a weak spatial dependence of the residual errors: a large NSR and a short range.

Using the variogram parameters found after fitting we compute the nugget to sill ratios for different plot sizes and shapes and also for different models. The values of NSR and NSR/range are shown in the following tables:

TABLE : 4.5.1

| JUTE | SPHERICAL  |        | NSR      | range | NSR/range |
|------|------------|--------|----------|-------|-----------|
| plot | nugget     |        |          |       |           |
| 1X1  | -0.6669    | 2825   | -0.00024 | 1.569 | -0.00015  |
| 2X1  | 6.209      | 1662   | 0.003722 | 1.607 | 0.002316  |
| 3X1  | 66.01      | 2628   | 0.024503 | 2.186 | 0.011209  |
| 4X1  | 170.6      | 1002   | 0.145489 | 2.912 | 0.049962  |
| 5X1  | 1109       | 4255   | 0.206749 | 3.304 | 0.062575  |
| 6X1  | 1147       | 6314   | 0.153733 | 2.991 | 0.051398  |
| 7X1  | 348.2      | 5598   | 0.058558 | 2.824 | 0.020736  |
| 8X1  | 116.8      | 779    | 0.130386 | 2.489 | 0.052385  |
| 9X1  | 679.9      | 8621   | 0.0731   | 2.173 | 0.03364   |
| 1X2  | -10.36     | 1599   | -0.00652 | 1.584 | -0.00412  |
| 2X2  | 3.789      | 1009   | 0.003741 | 1.469 | 0.002547  |
| 3X2  | 291.6      | 1559   | 0.157571 | 2.725 | 0.057824  |
| 4X2  | 55.04      | 737.4  | 0.069456 | 2.587 | 0.026848  |
| 5X2  | 198        | 6302   | 0.030462 | 3.224 | 0.009448  |
| 1X3  | 0.00005994 | 1119   | 5.36E-08 | 1.336 | 4.01E-08  |
| 2X3  | 46.36      | 743.6  | 0.058687 | 4.589 | 0.012789  |
| 3X3  | 45.33      | 951.6  | 0.04547  | 3.141 | 0.014476  |
| 4X3  | -18.96     | 564.6  | -0.03475 | 3.604 | -0.00964  |
| 1X4  | 0.001341   | 884.2  | 1.52E-06 | 1.295 | 1.17E-06  |
| 2X4  | 34.85      | 383.6  | 0.083284 | 4.652 | 0.017903  |
| 3X4  | -3.972     | 143000 | -2.8E-05 | 682.1 | -4.1E-08  |
| 4X4  | -8.883     | 208    | -0.04461 | 2.209 | -0.0202   |
| 1X5  | 167.3      | 693.7  | 0.194309 | 4.408 | 0.044081  |
| 2X5  | 28.99      | 428.4  | 0.063381 | 3.95  | 0.016046  |
| 3X5  | -15.69     | 79690  | -0.0002  | 457.9 | -4.3E-07  |
| 4X5  | -1.922     | 228.1  | -0.0085  | 2.514 | -0.00338  |
| 1X6  | 0.004263   | 951.2  | 4.48E-06 | 1.764 | 2.54E-06  |
| 2X6  | 27.2       | 606.5  | 0.042923 | 4.733 | 0.009069  |
| 3X6  | -15.59     | 943.2  | -0.01681 | 3.917 | -0.00429  |

| <i>plot</i> | <i>nugget</i> |       | <i>NSR</i> | <i>range</i> | <i>NSR/range</i> |
|-------------|---------------|-------|------------|--------------|------------------|
| 4X6         | -4.965        | 335.4 | -0.01503   | 2.734        | -0.0055          |
| 1X7         | 5.494         | 748.1 | 0.00729    | 1.059        | 0.006884         |
| 2X7         | 35.09         | 462.5 | 0.07052    | 5.078        | 0.013887         |
| 3X7         | 13.17         | 650.3 | 0.01985    | 3.952        | 0.005023         |
| 4X7         | 2.701         | 21870 | 0.000123   | 335.1        | 3.69E-07         |
| 1X8         | 0.006294      | 511.9 | 1.23E-05   | 0.5686       | 2.16E-05         |
| 2X8         | -14.03        | 341.7 | -0.04282   | 4.972        | -0.00861         |
| 3X8         | -22.83        | 444.3 | -0.05417   | 3.606        | -0.01502         |
| 4X8         | -12.17        | 193   | -0.0673    | 2.607        | -0.02582         |
| 1X9         | 320.1         | 199.3 | 0.616288   | 9.644        | <b>0.063904</b>  |
| 2X9         | 19.02         | 153.4 | 0.110312   | 5.381        | 0.0205           |
| 3X9         | 3.383         | 273.7 | 0.012209   | 3.011        | 0.004055         |
| 4X9         | -9.274        | 116.9 | -0.08617   | 2.691        | -0.03202         |

TABLE: 4.5.2

| JUTE        |             | EXPONENTIAL |                |          |                  |
|-------------|-------------|-------------|----------------|----------|------------------|
| <i>plot</i> | <i>sill</i> | <i>b</i>    | <i>NSR</i>     | <i>c</i> | <i>NSR/range</i> |
| 1X1         | 2828        | 2832        | -0.00141       | 0.5157   | -0.00274         |
| 1X2         | 1594        | 1596        | -0.00125       | 0.5527   | -0.00227         |
| 1X3         | 1121        | 1120        | 0.000892       | 0.4265   | 0.002092         |
| 1X4         | 885.7       | 885.1       | 0.000677       | 0.4118   | 0.001645         |
| 1X5         | 857.3       | 812         | <b>0.05284</b> | 1.228    | 0.04303          |
| 1X6         | 963.4       | 952.1       | 0.011729       | 0.8488   | 0.013819         |
| 1X7         | 753.9       | 753.9       | 0              | 0.1824   | 0                |
| 1X8         | 512.2       | 512.1       | 0.000195       | 0.06504  | 0.003002         |
| 1X9         | 477.5       | 465.1       | 0.025969       | 0.06579  | <b>0.394719</b>  |
| 2X1         | 1668        | 1673        | -0.003         | 0.4637   | -0.00646         |
| 2X2         | 1012        | 1013        | -0.00099       | 0.3885   | -0.00254         |
| 2X3         | 766.6       | 778.8       | -0.01591       | 1.57     | -0.01014         |
| 2X4         | 405         | 405.7       | -0.00173       | 1.522    | -0.00114         |
| 2X5         | 383.8       | 394.1       | -0.02684       | 0.9367   | -0.02865         |
| 2X6         | 555.6       | 588         | -0.05832       | 1.289    | -0.04524         |
| 2X7         | 462         | 475.9       | -0.03009       | 1.502    | -0.02003         |
| 2X8         | 313.9       | 331         | -0.05448       | 2.003    | -0.0272          |
| 2X9         | 170.6       | 162.6       | 0.046893       | 1.97     | 0.023804         |
| 3X1         | 2731        | 2737        | -0.0022        | 0.7756   | -0.00283         |
| 3X2         | 1610        | 1611        | -0.00062       | 0.3414   | -0.00182         |
| 3X3         | 1147        | 1136        | 0.00959        | 1.587    | 0.006043         |
| 3X4         | 5410000     | 5410000     | 0              | 17200    | 0                |
| 3X5         | 2583000     | 2583000     | 0              | 9892     | 0                |
| 3X6         | 1329        | 1342        | -0.00978       | 3.094    | -0.00316         |
| 3X7         | 820         | 824         | -0.00488       | 2.347    | -0.00208         |
| 3X8         | 555.4       | 575.2       | -0.03565       | 2.527    | -0.01411         |
| 3X9         | 263         | 267.6       | -0.01749       | 1.067    | -0.01639         |
| 4X1         | 994.9       | 1004        | -0.00915       | 0.5014   | -0.01824         |
| 4X2         | 783.5       | 778.1       | 0.006892       | 0.8425   | 0.008181         |
| 4X3         | 1159        | 1172        | -0.01122       | 4.773    | -0.00235         |
| 4X4         | 186         | 189.3       | -0.01774       | 0.9018   | -0.01967         |
| 4X5         | 244.9       | 247.1       | -0.00898       | 1.242    | -0.00723         |
| 4X6         | 409         | 413.2       | -0.01027       | 1.728    | -0.00594         |
| 4X7         | 350600      | 350600      | 0              | 3580     | 0                |

| <i>plot</i> | <i>sill</i> | <i>b</i> | <i>NSR</i> | <i>c</i> | <i>NSR/range</i> |
|-------------|-------------|----------|------------|----------|------------------|
| 4X8         | 239.7       | 246.3    | -0.02753   | 1.969    | -0.01398         |
| 4X9         | 161.1       | 166.4    | -0.0329    | 2.438    | -0.01349         |
| 5X1         | 5018        | 4992     | 0.005181   | 0.6152   | 0.008422         |
| 5X2         | 8154        | 8067     | 0.01067    | 2.022    | 0.005277         |
| 6X1         | 6655        | 6609     | 0.006912   | 0.4848   | 0.014258         |
| 7X1         | 5447        | 5451     | -0.00073   | 0.7885   | -0.00093         |
| 8X1         | 745.9       | 747.5    | -0.00215   | 0.3773   | -0.00569         |
| 9X1         | 7668        | 7656     | 0.001565   | 0.06809  | 0.022983         |

TABLE 4.5.3

| JUTE<br><i>plot</i> | <i>sill</i> | Gaussian<br><i>b</i> <i>NSR</i> |          | <i>c</i> | <i>NSR/range</i> |
|---------------------|-------------|---------------------------------|----------|----------|------------------|
| 1X1                 | 2825        | 2826                            | -0.00035 | 0.7514   | -0.00047         |
| 1X2                 | 1589        | 1595                            | -0.00378 | 0.7681   | -0.00492         |
| 1X3                 | 1119        | 1119                            | 0        | 0.6396   | 0                |
| 1X4                 | 884.2       | 884.2                           | 0        | 0.6165   | 0                |
| 1X5                 | 826.7       | 825.7                           | 0.00121  | 0.7963   | 0.001519         |
| 1X6                 | 951.7       | 950.9                           | 0.000841 | 0.8445   | 0.000995         |
| 1X7                 | 756.5       | 754.8                           | 0.002247 | 0.5664   | 0.003967         |
| 1X8                 | 513.8       | 514.4                           | -0.00117 | 0.5682   | -0.00206         |
| 1X9                 | 535.1       | 581.3                           | -0.08634 | 0.5637   | -0.15316         |
| 2X1                 | 1668        | 1667                            | 0.0006   | 0.7547   | 0.000794         |
| 2X2                 | 1014        | 1017                            | -0.00296 | 0.6893   | -0.00429         |
| 2X3                 | 715.9       | 689.1                           | 0.037435 | 1.53     | 0.024468         |
| 2X4                 | 377.2       | 357.7                           | 0.051697 | 1.453    | 0.035579         |
| 2X5                 | 382.2       | 378.7                           | 0.009158 | 1.19     | 0.007695         |
| 2X6                 | 545.9       | 557.1                           | -0.02052 | 1.48     | -0.01386         |
| 2X7                 | 436.9       | 436.1                           | 0.001831 | 1.438    | 0.001273         |
| 2X8                 | 300.8       | 287.5                           | 0.044215 | 2.268    | 0.019495         |
| 2X9                 | 144.4       | 141.5                           | 0.020083 | 0.9651   | 0.020809         |
| 3X1                 | 2683        | 2638                            | 0.016772 | 0.9616   | 0.017442         |
| 3X2                 | 1607        | 1607                            | 0        | 0.5893   | 0                |
| 3X3                 | 897.1       | 889.3                           | 0.008695 | 1        | 0.008695         |
| 3X4                 | 1112        | 1067                            | 0.040468 | 2.211    | 0.018303         |
| 3X5                 | 1156        | 1110                            | 0.039792 | 2.824    | 0.014091         |
| 3X6                 | 940.1       | 902.5                           | 0.039996 | 1.877    | 0.021308         |
| 3X7                 | 624.1       | 610                             | 0.022593 | 1.495    | 0.015112         |
| 3X8                 | 415.1       | 428.5                           | -0.03228 | 1.584    | -0.02038         |
| 3X9                 | 250.8       | 252.5                           | -0.00678 | 1.111    | -0.0061          |
| 4X1                 | 1002        | 1002                            | 0        | 0.8606   | 0                |
| 4X2                 | 713.7       | 710.3                           | 0.004764 | 0.7991   | 0.005962         |
| 4X3                 | 533.2       | 539.2                           | -0.01125 | 1.563    | -0.0072          |
| 4X4                 | 181.1       | 183.7                           | -0.01436 | 1.03     | -0.01394         |
| 4X5                 | 217.1       | 217.8                           | -0.00322 | 1.083    | -0.00298         |
| 4X6                 | 325.9       | 326.5                           | -0.00184 | 1.216    | -0.00151         |
| 4X7                 | 342.2       | 324.7                           | 0.05114  | 2.155    | 0.023731         |
| 4X8                 | 184.1       | 190.5                           | -0.03476 | 1.3      | -0.02674         |
| 4X9                 | 111.7       | 117.5                           | -0.05192 | 1.367    | -0.03798         |
| 5X1                 | 4908        | 4878                            | 0.006112 | 0.7294   | 0.00838          |

| <i>plot</i> | <i>sill</i> | <i>b</i> | <i>NSR</i> | <i>c</i> | <i>NSR/range</i> |
|-------------|-------------|----------|------------|----------|------------------|
| 5X2         | 5061        | 4900     | 0.031812   | 1.024    | 0.031066         |
| 6X1         | 6365        | 6365     | 0          | -0.1521  | 0                |
| 7X1         | 5351        | 5133     | 0.04074    | 1.037    | 0.039286         |
| 8X1         | 755.5       | 758.2    | -0.00357   | 0.7338   | -0.00487         |
| 9X1         | 7696        | 7695     | 0.00013    | 0.1859   | 0.000699         |

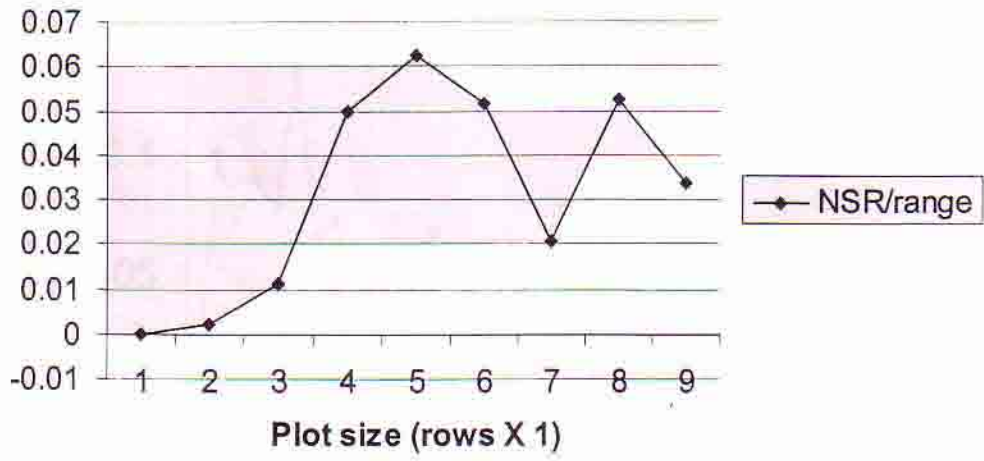
TABLE:4.5.4  
JUTE

| plot | Michaelis-menton |          |          |          |            |
|------|------------------|----------|----------|----------|------------|
|      | sill             | b        | NSR      | range    | NSR/range  |
| 1X1  | 2869             | 2870     | -0.00035 | 0.1153   | -0.003023  |
| 1X2  | 1638             | 1639     | -0.00061 | 0.1868   | -0.0032682 |
| 1X3  | 1177             | 1174     | 0.002549 | 0.2657   | 0.009593   |
| 1X4  | 909.6            | 909.3    | 0.00033  | 0.1516   | 0.0021756  |
| 1X5  | 919.7            | 912.2    | 0.008155 | 0.6338   | 0.0128666  |
| 1X6  | 1018             | 1018     | 0        | 0.4347   | 0          |
| 1X7  | 751              | 751      | 0        | -0.01598 | 0          |
| 1X8  | 525.3            | 525.2    | 0.00019  | 0.1182   | 0.0016106  |
| 1X9  | 470              | 469.9    | 0.000213 | -0.1168  | -0.0018216 |
| 2X1  | 1631             | 1631     | 0        | 0.08459  | 0          |
| 2X2  | 1031             | 1031     | 0        | 0.07935  | 0          |
| 2X3  | 973.7            | 984.1    | -0.01068 | 1.583    | -0.0067473 |
| 2X4  | 504.7            | 506.9    | -0.00436 | 1.449    | -0.0030083 |
| 2X5  | 431.8            | 436.4    | -0.01065 | 0.6315   | -0.0168695 |
| 2X6  | 664.6            | 684.1    | -0.02934 | 1.127    | -0.0260346 |
| 2X7  | 568.6            | 579.3    | -0.01882 | 1.408    | -0.0133652 |
| 2X8  | 418.6            | 430.7    | -0.02891 | 2.289    | -0.0126282 |
| 2X9  | 205.8            | 202.2    | 0.017493 | 1.65     | 0.0106016  |
| 3X1  | 3033             | 3039     | -0.00198 | 0.454    | -0.0043574 |
| 3X2  | 1615             | 1615     | 0        | 0.02729  | 0          |
| 3X3  | 1578             | 1572     | 0.003802 | 1.866    | 0.0020377  |
| 3X4  | 12890000         | 12890000 | 0        | 40990    | 0          |
| 3X5  | 6087000          | 6087000  | 0        | 23310    | 0          |
| 3X6  | 2147             | 2158     | -0.00512 | 4.833    | -0.0010601 |
| 3X7  | 1224             | 1228     | -0.00327 | 3.235    | -0.0010102 |
| 3X8  | 897.1            | 913.7    | -0.0185  | 3.963    | -0.0046692 |
| 3X9  | 330.6            | 333.4    | -0.00847 | 1.048    | -0.0080815 |
| 4X1  | 1002             | 1002     | 0        | 0.0691   | 0          |
| 4X2  | 949.2            | 947.6    | 0.001686 | 0.7014   | 0.0024032  |
| 4X3  | 2151             | 2163     | -0.00558 | 8.855    | -0.00063   |
| 4X4  | 236.8            | 238.5    | -0.00718 | 0.9104   | -0.0078856 |
| 4X5  | 337.6            | 339.1    | -0.00444 | 1.494    | -0.002974  |
| 4X6  | 616.1            | 619.2    | -0.00503 | 2.435    | -0.0020664 |
| 4X7  | 609000           | 609000   | 0        | 6218     | 0          |
| 4X8  | 389.4            | 394.6    | -0.01335 | 3.132    | -0.0042637 |
| 4X9  | 279.3            | 283.7    | -0.01575 | 4.218    | -0.0037349 |
| 5X1  | 5529             | 5524     | 0.000904 | 0.3414   | 0.0026489  |
| 5X2  | 11500            | 11440    | 0.005217 | 2.532    | 0.0020606  |
| 6X1  | 7183             | 7175     | 0.001114 | 0.2254   | 0.0049412  |
| 7X1  | 6187             | 6194     | -0.00113 | 0.5116   | -0.0022115 |
| 8X1  | 707.4            | 707.8    | -0.00057 | -0.07468 | 0.0075717  |
| 9X1  | 7500             | 7500     | 0        | -0.05585 | 0          |

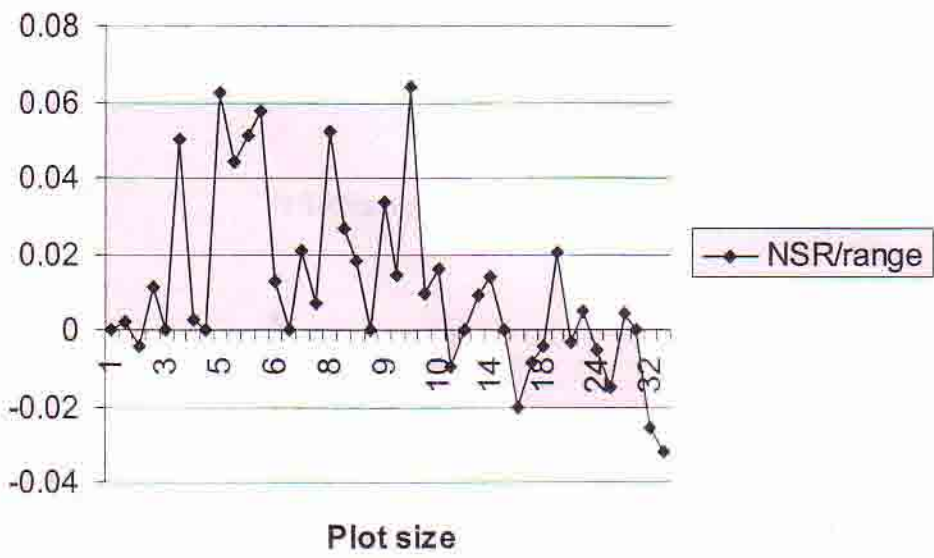
TABLE 4.5.5

| JUTE |       | VB      |          |          |          |           |
|------|-------|---------|----------|----------|----------|-----------|
| plot | Li    | K       | t0       | nugget   | NSR      | NSR/range |
| 1X1  | 2826  | 1.948   | 0.000761 | -4.19024 | -0.00148 | -0.00076  |
| 1X2  | 1594  | 1.809   | 0.000721 | -2.07982 | -0.0013  | -0.00072  |
| 1X3  | 1121  | 2.341   | -0.00023 | 0.612073 | 0.000546 | 0.000233  |
| 1X4  | 885.7 | 2.43    | -0.00029 | 0.618126 | 0.000698 | 0.000287  |
| 1X5  | 858.4 | 0.7976  | -0.07252 | 48.24285 | 0.056201 | 0.070463  |
| 1X6  | 963.5 | 1.177   | -0.01008 | 11.36358 | 0.011794 | 0.01002   |
| 1X7  | 753.9 | 5.31    | -3.1E-05 | 0.124009 | 0.000164 | 3.1E-05   |
| 1X8  | 512   | 8.055   | 2.16E-06 | -0.00889 | -1.7E-05 | -2.2E-06  |
| 1X9  | 482   | 10.13   | 0.001123 | -5.51453 | -0.01144 | -0.00113  |
| 2X1  | 1668  | 2.145   | 0.001389 | -4.97706 | -0.00298 | -0.00139  |
| 2X2  | 1012  | 2.556   | 0.000694 | -1.797   | -0.00178 | -0.00069  |
| 2X3  | 766.6 | 0.637   | 0.02475  | -12.1818 | -0.01589 | -0.02495  |
| 2X4  | 405   | 0.6572  | 0.002639 | -0.70302 | -0.00174 | -0.00264  |
| 2X5  | 383.9 | 1.066   | 0.02459  | -10.1962 | -0.02656 | -0.02492  |
| 2X6  | 555.5 | 0.7759  | 0.07317  | -32.4496 | -0.05842 | -0.07529  |
| 2X7  | 461.9 | 0.6658  | 0.04463  | -13.9312 | -0.03016 | -0.0453   |
| 2X8  | 314.8 | 0.4938  | 0.1039   | -16.5726 | -0.05264 | -0.10661  |
| 2X9  | 170.7 | 0.507   | -0.09577 | 8.090399 | 0.047395 | 0.093482  |
| 3X1  | 2731  | 1.29    | 0.001811 | -6.38759 | -0.00234 | -0.00181  |
| 3X2  | 1610  | 2.931   | 4.16E-05 | -0.19627 | -0.00012 | -4.2E-05  |
| 3X3  | 1148  | 0.6297  | -0.01619 | 11.64422 | 0.010143 | 0.016108  |
| 3X4  | 9168  | 0.03584 | 0.02734  | -8.98781 | -0.00098 | -0.02735  |
| 3X5  | 17310 | 0.0153  | 0.06471  | -17.1465 | -0.00099 | -0.06474  |
| 3X6  | 1329  | 0.3232  | 0.03119  | -13.4649 | -0.01013 | -0.03135  |
| 3X7  | 820   | 0.4261  | 0.01128  | -3.95074 | -0.00482 | -0.01131  |
| 3X8  | 555.2 | 0.3958  | 0.08862  | -19.8196 | -0.0357  | -0.09019  |
| 3X9  | 263   | 0.9372  | 0.0184   | -4.57463 | -0.01739 | -0.01856  |
| 4X1  | 994.6 | 2.008   | 0.004607 | -9.24359 | -0.00929 | -0.00463  |
| 4X2  | 783.6 | 1.187   | -0.00588 | 5.44737  | 0.006952 | 0.005857  |
| 4X3  | 1159  | 0.2096  | 0.05408  | -13.2122 | -0.0114  | -0.05439  |
| 4X4  | 186.1 | 1.105   | 0.01586  | -3.29021 | -0.01768 | -0.016    |
| 4X5  | 244.8 | 0.8059  | 0.0113   | -2.23949 | -0.00915 | -0.01135  |
| 4X6  | 409   | 0.5789  | 0.01749  | -4.16214 | -0.01018 | -0.01758  |
| 4X7  | 5887  | 0.01702 | -0.01889 | 1.892412 | 0.000321 | 0.018887  |
| 4X8  | 238.9 | 0.5109  | 0.05359  | -6.63124 | -0.02776 | -0.05433  |
| 4X9  | 161.1 | 0.4103  | 0.07797  | -5.23709 | -0.03251 | -0.07923  |
| 5X1  | 5017  | 1.627   | -0.00309 | 25.11871 | 0.005007 | 0.003077  |
| 5X2  | 8155  | 0.4943  | -0.02162 | 86.68655 | 0.01063  | 0.021505  |
| 6X1  | 6652  | 2.073   | -0.00324 | 44.50119 | 0.00669  | 0.003227  |
| 7X1  | 5448  | 1.267   | 0.000576 | -3.97529 | -0.00073 | -0.00058  |
| 8X1  | 745.6 | 2.748   | 0.001286 | -2.63956 | -0.00354 | -0.00129  |
| 9X1  | 7767  | 15.74   | 4.83E-06 | -0.59075 | -7.6E-05 | -4.8E-06  |

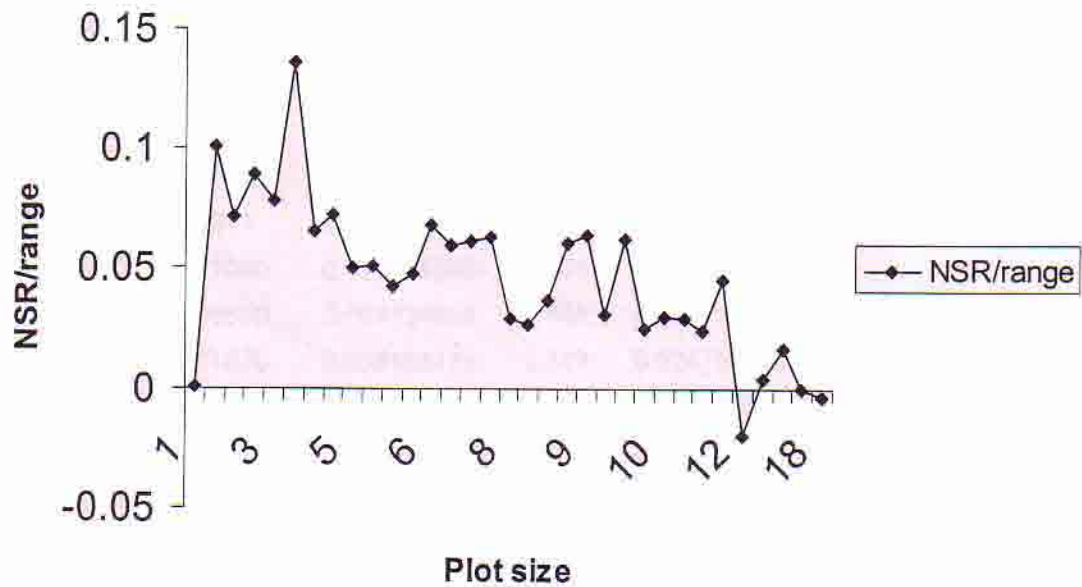
Nugget-Sill / range (JUTE)



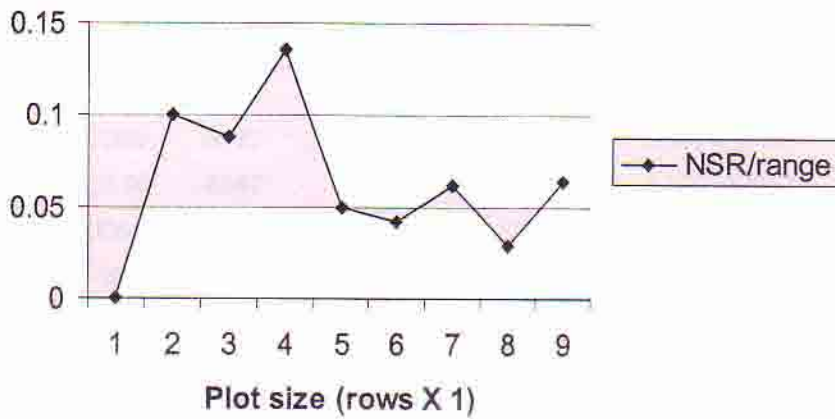
Nugget-Sill / range (JUTE)



Nugget-Sill / Range ratio (Rice)



NSR/range (RICE)



RICE SPHERICAL

| plot | nugget |       | NSR         | range | NSR/range   |
|------|--------|-------|-------------|-------|-------------|
| 1X1  | 3.542  | 24170 | 0.000146524 | 1.268 | 0.000115555 |
| 2X1  | 6616   | 5565  | 0.543140957 | 5.431 | 0.100007541 |
| 3X1  | 18200  | 25230 | 0.419065162 | 4.742 | 0.088373084 |

| <i>plot</i> | <i>nugget</i> |        | <i>NSR</i>  | <i>range</i> | <i>NSR / range</i> |
|-------------|---------------|--------|-------------|--------------|--------------------|
| 4X1         | 25860         | 13550  | 0.656178635 | 4.825        | 0.135995572        |
| 5X1         | 21560         | 53520  | 0.287160362 | 5.78         | 0.049681724        |
| 6X1         | 10040         | 41130  | 0.196208716 | 4.629        | 0.042386847        |
| 7X1         | 57330         | 144400 | 0.284191741 | 4.641        | 0.061235023        |
| 8X1         | 18240         | 46320  | 0.282527881 | 9.784        | 0.028876521        |
| 9X1         | 54570         | 112400 | 0.326825178 | 5.129        | 0.063721033        |
| 1X2         | 8770          | 9158   | 0.489178938 | 6.893        | 0.070967494        |
| 2X2         | 1929          | 7671   | 0.2009375   | 3.081        | 0.065218273        |
| 3X2         | 3785          | 31080  | 0.108561595 | 2.301        | 0.04718018         |
| 4X2         | 2642          | 38550  | 0.064138668 | 2.401        | 0.026713314        |
| 5X2         | 3817          | 61820  | 0.058153176 | 2.349        | 0.024756567        |
| 6X2         | 2373          | 37210  | 0.059949979 | 2.066        | 0.029017415        |
| 1X3         | 7014          | 7702   | 0.476624083 | 6.155        | 0.077436894        |
| 2X3         | 1446          | 5806   | 0.199393271 | 2.947        | 0.067659746        |
| 3X3         | 2987          | 36640  | 0.075377899 | 2.445        | 0.030829407        |
| 4X3         | 2027          | 38970  | 0.049442642 | 2.053        | 0.024083118        |
| 5X3         | 2214          | 51710  | 0.041057785 | 2.454        | 0.016730964        |
| 1X4         | 5592          | 7461   | 0.428407263 | 5.973        | 0.071723968        |
| 2X4         | 798.9         | 7416   | 0.097250119 | 2.638        | 0.036865094        |
| 3X4         | 1887          | 23710  | 0.073719577 | 1.642        | 0.04489621         |
| 1X5         | 3259          | 8599   | 0.274835554 | 5.363        | 0.051246607        |
| 2X5         | 528.8         | 7211   | 0.068322179 | 2.263        | 0.030190976        |
| 1X6         | 3397          | 7458   | 0.312943344 | 5.301        | 0.059034775        |
| 2X6         | -310.3        | 8229   | -0.03918572 | 2.012        | -0.019476006       |
| 1X7         | 3009          | 6072   | 0.331351173 | 5.305        | 0.062460165        |
| 2X7         | 58.95         | 6987   | 0.008366508 | 2.114        | 0.003957667        |
| 1X8         | 3060          | 6146   | 0.332391918 | 5.52         | 0.060215927        |
| 2X8         | -10.33        | 6163   | -0.00167895 | 2.222        | -0.000755601       |
| 1X9         | 2649          | 5263   | 0.334807887 | 5.445        | 0.061489052        |
| 2X9         | -41.82        | 5190   | -0.00812326 | 2.044        | -0.003974197       |

RICE EXPONENTIAL

| <i>plot</i> | <i>sill</i> | <i>b</i> | <i>NSR</i>  | <i>range</i> | <i>NSR / range</i> |
|-------------|-------------|----------|-------------|--------------|--------------------|
| 1X1         | 24060       | 24010    | 0.002078138 | 0.4466       | 0.004653242        |
| 1X2         | 16630       | 16590    | 0.002405292 | 0.6933       | 0.003469337        |
| 1X3         | 13200       | 13270    | -0.00530303 | 0.7179       | -0.0073868         |
| 1X4         | 11460       | 11480    | -0.0017452  | 0.6949       | -0.0025114         |
| 1X5         | 9560        | 9573     | -0.00135983 | 0.5216       | -0.0026070         |
| 1X6         | 8966        | 9083     | -0.0130493  | 0.6304       | 0.020700028        |
| 1X7         | 7424        | 7436     | -0.00161638 | 0.3932       | -0.0041108         |

| plot | sill   | b      | NSR         | range   | NSR/range   |
|------|--------|--------|-------------|---------|-------------|
| 1X8  | 7786   | 7807   | -0.00269715 | 0.5127  | -0.0052606  |
| 1X9  | 6715   | 6801   | -0.01280715 | 0.6068  | -0.0211060  |
| 2X1  | 11880  | 11920  | -0.003367   | 0.4901  | -0.0068700  |
| 2X2  | 8911   | 8942   | -0.00347885 | 0.4325  | -0.0080435  |
| 2X3  | 6565   | 6577   | -0.00182788 | 0.4564  | -0.0040049  |
| 2X4  | 7013   | 7058   | -0.00641665 | 0.5025  | -0.0127694  |
| 2X5  | 5959   | 5925   | 0.005705655 | 0.03167 | 0.180159625 |
| 2X6  | 6197   | 6248   | -0.00822979 | 0.5394  | -0.0152573  |
| 2X7  | 5879   | 5896   | -0.00289165 | 0.5071  | -0.0057023  |
| 2X8  | 5550   | 5586   | -0.00648649 | 0.715   | -0.0090720  |
| 2X9  | 4110   | 4124   | -0.00340633 | 0.4758  | -0.0071591  |
| 3X1  | 38450  | 38400  | 0.00130039  | 0.1029  | 0.012637416 |
| 3X2  | 27370  | 26800  | 0.020825722 | 0.08392 | 0.248161601 |
| 3X3  | 38470  | 37930  | 0.014036912 | 0.7206  | 0.019479478 |
| 3X4  | 26800  | 26110  | 0.025746269 | 0.03449 | 0.746485029 |
| 4X1  | 39680  | 39670  | 0.000252016 | 0.076   | 0.003316002 |
| 4X2  | 39040  | 38670  | 0.009477459 | 0.6663  | 0.014224012 |
| 4X3  | 35200  | 35190  | 0.000284091 | 0.04587 | 0.006193392 |
| 5X1  | 61130  | 61010  | 0.00196303  | 0.4427  | 0.004434221 |
| 5X2  | 61610  | 61250  | 0.005843207 | 0.6296  | 0.009280825 |
| 5X3  | 57420  | 56820  | 0.010449321 | 1.05    | 0.009951734 |
| 6X1  | 41820  | 41890  | -0.00167384 | 0.6105  | -0.0027417  |
| 6X2  | 31700  | 31750  | -0.00157729 | 0.07332 | -0.0215123  |
| 7X1  | 168200 | 168200 | 0           | 0.3188  | 0           |
| 8X1  | 54760  | 54720  | 0.00073046  | 0.4232  | 0.00172604  |
| 9X1  | 142400 | 139800 | 0.018258427 | 0.05253 | 0.347580944 |

| RICE |       | Gaussian |             |         |              |
|------|-------|----------|-------------|---------|--------------|
| plot | sill  | b        | NSR         | range   | NSR/range    |
| 1X1  | 24010 | 24010    | 0           | 0.6092  | 0            |
| 1X2  | 16520 | 16490    | 0.001815981 | 0.8364  | 0.002171187  |
| 1X3  | 13120 | 12970    | 0.011432927 | 0.9326  | 0.012259197  |
| 1X4  | 11390 | 11220    | 0.014925373 | 0.9091  | 0.016417746  |
| 1X5  | 9550  | 9551     | -0.00010471 | 0.7441  | -0.0001407   |
| 1X6  | 9002  | 9015     | -0.00144412 | 0.9097  | -0.0015874   |
| 1X7  | 7450  | 7451     | -0.00013423 | 0.6833  | -0.0001964   |
| 1X8  | 7800  | 7804     | -0.00051282 | 0.7666  | -0.0006689   |
| 1X9  | 6754  | 6783     | -0.00429375 | 0.9008  | -0.0047665   |
| 2X1  | 11880 | 11870    | 0.000841751 | 0.7602  | 0.0011072    |
| 2X2  | 8933  | 8962     | -0.00324639 | 0.7362  | -0.004409657 |
| 2X3  | 6558  | 6552     | 0.000914913 | 0.7281  | 0.001256576  |
| 2X4  | 7168  | 7164     | 0.000558036 | 0.8532  | 0.00065405   |
| 2X5  | 6638  | 6638     | 0           | 0.5739  | 0            |
| 2X6  | 6373  | 6402     | -0.00455045 | 0.8645  | -0.005263675 |
| 2X7  | 5929  | 5933     | -0.00067465 | 0.7721  | -0.000873786 |
| 2X8  | 5478  | 5491     | -0.00237313 | 0.8944  | -0.002653319 |
| 2X9  | 4182  | 4187     | -0.0011956  | 0.7752  | -0.001542312 |
| 3X1  | 42210 | 44430    | -0.05259417 | 0.3133  | -0.167871599 |
| 3X2  | 29980 | 29980    | 0           | 0.1592  | 0            |
| 3X3  | 33140 | 33070    | 0.002112251 | 0.09366 | 0.022552328  |

| Plot | sill   | b      | NSR         | range  | NSR/range    |
|------|--------|--------|-------------|--------|--------------|
| 3X4  | 20190  | 19360  | 0.04110946  | 0.1326 | 0.310026094  |
| 4X1  | 39620  | 39500  | 0.003028773 | 0.3208 | 0.009441313  |
| 4X2  | 35220  | 35250  | -0.00085179 | 0.2236 | -0.003809431 |
| 4X3  | 44000  | 43640  | 0.008181818 | 1.031  | 0.007935808  |
| 5X1  | 60350  | 60340  | 0.0001657   | 0.347  | 0.000477522  |
| 5X2  | 56760  | 56760  | 0           | 0.3152 | 0            |
| 5X3  | 42090  | 42090  | 0           | 0.2045 | 0            |
| 6X1  | 41570  | 41570  | 0           | 0.7935 | 0            |
| 6X2  | 31220  | 31210  | 0.000320307 | 0.2031 | 0.001577093  |
| 7X1  | 168300 | 168300 | 0           | 0.5753 | 0            |
| 8X1  | 54420  | 54420  | 0           | 0.6164 | 0            |
| 9X1  | 143100 | 141800 | 0.009084556 | 0.2978 | 0.030505562  |

RICE VB

| plot | sill   | b      | NSR         | range   | NSR/range   |
|------|--------|--------|-------------|---------|-------------|
| 1X1  | 24060  | 24010  | 0.002078138 | 0.4466  | 0.004653242 |
| 1X2  | 16630  | 16590  | 0.002405292 | 0.6933  | 0.003469337 |
| 1X3  | 13200  | 13270  | -0.00530303 | 0.7179  | -0.0073868  |
| 1X4  | 11460  | 11480  | -0.0017452  | 0.6949  | -0.0025114  |
| 1X5  | 9560   | 9573   | -0.00135983 | 0.5216  | -0.0026070  |
| 1X6  | 8966   | 9083   | -0.0130493  | 0.6304  | -0.0207000  |
| 1X7  | 7424   | 7436   | -0.00161638 | 0.3932  | -0.0041108  |
| 1X8  | 7786   | 7807   | -0.00269715 | 0.5127  | -0.0052606  |
| 1X9  | 6715   | 6801   | -0.01280715 | 0.6068  | -0.0211060  |
| 2X1  | 11880  | 11920  | -0.003367   | 0.4901  | -0.0068700  |
| 2X2  | 8911   | 8942   | -0.00347885 | 0.4325  | -0.0080435  |
| 2X3  | 6565   | 6577   | -0.00182788 | 0.4564  | -0.0040049  |
| 2X4  | 7013   | 7058   | -0.00641665 | 0.5025  | -0.0127694  |
| 2X5  | 5959   | 5925   | 0.005705655 | 0.03167 | 0.180159625 |
| 2X6  | 6197   | 6248   | -0.00822979 | 0.5394  | -0.0152573  |
| 2X7  | 5879   | 5896   | -0.00289165 | 0.5071  | -0.0057023  |
| 2X8  | 5550   | 5586   | -0.00648649 | 0.715   | -0.0090720  |
| 2X9  | 4110   | 4124   | -0.00340633 | 0.4758  | -0.0071591  |
| 3X1  | 38450  | 38400  | 0.00130039  | 0.1029  | 0.012637416 |
| 3X2  | 27370  | 26800  | 0.020825722 | 0.08392 | 0.248161601 |
| 3X3  | 38470  | 37930  | 0.014036912 | 0.7206  | 0.019479478 |
| 3X4  | 26800  | 26110  | 0.025746269 | 0.03449 | 0.746485029 |
| 4X1  | 39680  | 39670  | 0.000252016 | 0.076   | 0.003316002 |
| 4X2  | 39040  | 38670  | 0.009477459 | 0.6663  | 0.014224012 |
| 4X3  | 35200  | 35190  | 0.000284091 | 0.04587 | 0.006193392 |
| 5X1  | 61130  | 61010  | 0.00196303  | 0.4427  | 0.004434221 |
| 5X2  | 61610  | 61250  | 0.005843207 | 0.6296  | 0.009280825 |
| 5X3  | 57420  | 56820  | 0.010449321 | 1.05    | 0.009951734 |
| 6X1  | 41820  | 41890  | -0.00167384 | 0.6105  | -0.0027417  |
| 6X2  | 31700  | 31750  | -0.00157729 | 0.07332 | -0.0215123  |
| 7X1  | 168200 | 168200 | 0           | 0.3188  | 0           |
| 8X1  | 54760  | 54720  | 0.00073046  | 0.4232  | 0.00172604  |
| 9X1  | 142400 | 139800 | 0.018258427 | 0.05253 | 0.347580944 |

| RICE | Michaelis-menton |        |             |          |              |
|------|------------------|--------|-------------|----------|--------------|
| plot | sill             | b      | NSR         | range    | NSR/range    |
| 1X1  | 24430            | 24430  | 0           | 0.1017   | 0            |
| 1X2  | 17140            | 17170  | -0.00175029 | 0.2052   | -0.008529687 |
| 1X3  | 13460            | 13500  | -0.00297177 | 0.1671   | -0.01778437  |
| 1X4  | 11700            | 11730  | -0.0025641  | 0.1758   | -0.014585339 |
| 1X5  | 9558             | 9559   | -0.00010462 | 0.06292  | -0.001662816 |
| 1X6  | 8978             | 8988   | -0.00111383 | 0.1059   | -0.010517789 |
| 1X7  | 7259             | 7260   | -0.00013776 | -0.04027 | 0.003420909  |
| 1X8  | 7803             | 7806   | -0.00038447 | 0.06873  | -0.005593882 |
| 1X9  | 6764             | 6774   | -0.00147842 | 0.1186   | -0.012465558 |
| 2X1  | 12010            | 12010  | 0           | 0.07236  | 0            |
| 2X2  | 8966             | 8967   | -0.00011153 | 0.04856  | -0.002296797 |
| 2X3  | 6763             | 6765   | -0.00029573 | 0.1133   | -0.002610121 |
| 2X4  | 7352             | 7359   | -0.00095212 | 0.1498   | -0.006355954 |
| 2X5  | 6910             | 6910   | 0           | 0.09604  | 0            |
| 2X6  | 6624             | 6633   | -0.0013587  | 0.2394   | -0.00567542  |
| 2X7  | 6260             | 6264   | -0.00063898 | 0.2118   | -0.003016892 |
| 2X8  | 6523             | 6538   | -0.00229956 | 0.5501   | -0.00418025  |
| 2X9  | 4256             | 4258   | -0.00046992 | 0.1446   | -0.003249826 |
| 3X1  | 38490            | 38490  | 0           | -0.00371 | 0            |
| 3X2  | 30130            | 30130  | 0           | -0.02913 | 0            |
| 3X3  | 44000            | 43870  | 0.002954545 | 0.4641   | 0.006366183  |
| 3X4  | 15300            | 15060  | 0.015686275 | -0.4682  | -0.033503363 |
| 4X1  | 39400            | 39400  | 0           | -0.02508 | 0            |
| 4X2  | 44060            | 43990  | 0.001588743 | 0.4038   | 0.003934479  |
| 4X3  | 42510            | 42480  | 0.000705716 | 0.2621   | 0.002692546  |
| 5X1  | 61720            | 61720  | 0           | 0.06429  | 0            |
| 5X2  | 69440            | 69370  | 0.001008065 | 0.3795   | 0.002656296  |
| 5X3  | 72660            | 72390  | 0.003715937 | 1.005    | 0.00369745   |
| 6X1  | 43760            | 43800  | -0.00091408 | 0.2414   | -0.003786565 |
| 6X2  | 28940            | 28940  | 0           | -0.1479  | 0            |
| 7X1  | 167600           | 167600 | 0           | 0.01082  | 0            |
| 8X1  | 57320            | 57310  | 0.000174459 | 0.1703   | 0.001024423  |
| 9X1  | 144400           | 144400 | 0           | -0.01447 | 0            |

## Chapter 5

### A NEW METHOD FOR DETERMINATION OF PLOT SIZE.

**5.1 Introduction:** It is well known that the application of classical analysis of variance technique to data from designed experiments assumes that the observations are independent. In real life situation, it is not an usual phenomenon that the observed data are random. The data from field experiments are often found to be spatially correlated. This chapter is devoted to the development of a new method for obtaining optimum plot size using the well known variogram technique which is used to discover the spatial heterogeneity structure in a set of data. This method calls for determination of particular (optimum) plot size for (and higher) the data become random. The particular plot size is identified by invoking the theory of minimization of curvature(maximization of radius of curvature). The fundamental basis of the method lies in studying the nature of the curvature of variogram curve for each possible plot size and shape. Decrease in range implies that with a slight increase in the lag distance between pairs of sample observations the variogram immediately attains its sill value. Attaining sill value again indicates that pairs of observations are no longer dependent on the separation distance between them. In other words, at this point pairs of observations become independent of each other.

**5.2 Material and method:** Here we determine the point at which the radius of curvature becomes maximum. To find this we use the method of determination of maximum curvature as described in section 2.3. We have deduced the values of  $h_{opt}$  for each of the spherical, exponential, Michaelis-Menton and VB models. The following table summarizes the solutions corresponding to  $h_{opt}$  for different models:

TABLE 5.2.1 : Point of maximum curvature for different models.

| Model   | $h_{opt}$  |
|---|--|
| <i>Spherical:</i> $y = a + b \cdot (1.5 \cdot (x/c) - 0.5 \cdot (x/c)^3)$ | $c \cdot \sqrt{\frac{6b + \sqrt{81b^2 + 20c^2}}{15b}}$     |
| <i>Exponential:</i> $y = a - b \cdot \exp(-x/c)$                          | $c \cdot \log_e \left( \frac{\sqrt{2} \cdot b}{c} \right)$ |
| <i>Michaelis-Menton:</i> $y = a - b \cdot \exp[-(x/c)^2]$                 | $-c + \sqrt{b \cdot c}$                                    |
| <i>VB:</i> $y = L_{\infty} \cdot [1 - \exp\{-k \cdot (t - t_0)\}]$        | $\frac{1}{\sqrt{2} \cdot L_{\infty} \cdot k}$              |

Finally we compute the amount of curvature at the  $h_{opt}$  value for each of different plot sizes and shapes. We choose that plot size and shape which gives the maximum amount of radius of curvature at  $h_{opt}$ . As the centre of curvature of the variogram curve is on the negative side of the normal, the curvature values will be -ve. The following tables present the maximum curvature values for different plot sizes and shapes.

### 5.3. Results:

TABLE 5.3.1 : Amount of curvature of spherical curve for Jute data.

| plot | b      | c      |          | $h_{opt}$ | y1       | y2       | curvature  |
|------|--------|--------|----------|-----------|----------|----------|------------|
| 1X1  | 2825   | 1.569  | 25425    | 4432.425  | -2.2E+10 | -9725508 | -1.03E+24  |
| 1X2  | 1599   | 1.584  | 14391    | 2532.816  | -3.9E+09 | -3057087 | -1.898E+22 |
| 1X3  | 1119   | 1.336  | 10071    | 1494.984  | -1.6E+09 | -2104595 | -1.85E+21  |
| 1X4  | 884.2  | 1.295  | 7957.802 | 1145.039  | -8E+08   | -1398565 | -3.671E+20 |
| 1X5  | 693.7  | 4.408  | 6243.331 | 3057.834  | -1.1E+08 | -74298.9 | -1.973E+19 |
| 1X6  | 951.2  | 1.764  | 8560.804 | 1677.917  | -7.3E+08 | -872304  | -4.493E+20 |
| 1X7  | 748.1  | 1.059  | 6732.902 | 792.238   | -5.9E+08 | -1497093 | -1.393E+20 |
| 1X8  | 511.9  | 0.5686 | 4607.101 | 291.0664  | -3.5E+08 | -2431520 | -1.822E+19 |
| 1X9  | 199.3  | 9.644  | 1794.218 | 1922.216  | -1231460 | -1281.32 | -1.457E+15 |
| 2X1  | 1662   | 1.607  | 14958    | 2670.834  | -4.3E+09 | -3208866 | -2.452E+22 |
| 2X2  | 1009   | 1.469  | 9081.002 | 1482.221  | -1E+09   | -1415338 | -8.154E+20 |
| 2X3  | 743.6  | 4.589  | 6692.431 | 3412.385  | -1.3E+08 | -78770.7 | -3.082E+19 |
| 2X4  | 383.6  | 4.652  | 3452.463 | 1784.517  | -1.8E+07 | -20398.6 | -2.956E+17 |
| 2X5  | 428.4  | 3.95   | 3855.64  | 1692.185  | -3E+07   | -35288   | -7.542E+17 |
| 2X6  | 606.5  | 4.733  | 5458.541 | 2870.571  | -7.1E+07 | -49261.9 | -7.175E+18 |
| 2X7  | 462.5  | 5.078  | 4162.562 | 2348.585  | -2.9E+07 | -24886.4 | -1.003E+18 |
| 2X8  | 341.7  | 4.972  | 3075.38  | 1698.946  | -1.2E+07 | -14169.4 | -1.231E+17 |
| 2X9  | 153.4  | 5.381  | 1380.81  | 825.483   | -1006295 | -2438.18 | -4.179E+14 |
| 3X1  | 2628   | 2.186  | 23652    | 5744.808  | -1.2E+10 | -4335824 | -4.455E+23 |
| 3X2  | 1559   | 2.725  | 14031.01 | 4248.275  | -2.1E+09 | -981930  | -9.241E+21 |
| 3X3  | 951.6  | 3.141  | 8564.412 | 2988.977  | -4.1E+08 | -275356  | -2.531E+20 |
| 3X4  | 143000 | 682.1  | 1287004  | 97540382  | -6.4E+12 | -131855  | -2.017E+33 |
| 3X5  | 79690  | 457.9  | 717212.9 | 36490096  | -1.7E+12 | -90863.2 | -5.014E+31 |
| 3X6  | 943.2  | 3.917  | 8488.818 | 3694.517  | -3.2E+08 | -173949  | -1.907E+20 |
| 3X7  | 650.3  | 3.952  | 5852.727 | 2569.989  | -1E+08   | -81229.8 | -1.4E+19   |
| 3X8  | 444.3  | 3.606  | 3998.733 | 1602.15   | -3.6E+07 | -45543.2 | -1.066E+18 |
| 3X9  | 273.7  | 3.011  | 2463.337 | 824.1144  | -1E+07   | -24788.6 | -4.299E+16 |
| 4X1  | 1002   | 2.912  | 9018.009 | 2917.825  | -5.2E+08 | -355201  | -3.918E+20 |
| 4X2  | 737.4  | 2.587  | 6636.61  | 1907.655  | -2.3E+08 | -243745  | -5.156E+19 |
| 4X3  | 564.6  | 3.604  | 5081.426 | 2034.821  | -7.5E+07 | -73626.5 | -5.709E+18 |
| 4X4  | 208    | 2.209  | 1872.026 | 459.4739  | -6110534 | -26598.6 | -8.578E+15 |
| 4X5  | 228.1  | 2.514  | 2052.931 | 573.446   | -7081046 | -24696.9 | -1.438E+16 |
| 4X6  | 335.4  | 2.734  | 3018.625 | 916.9859  | -2.1E+07 | -45149.3 | -1.965E+17 |
| 4X7  | 21870  | 335.1  | 196835.7 | 7328701   | -4.7E+10 | -12778.3 | -8.034E+27 |
| 4X8  | 193    | 2.607  | 1737.039 | 503.1544  | -4136341 | -16442.1 | -4.304E+15 |
| 4X9  | 116.9  | 2.691  | 1052.169 | 314.5841  | -890443  | -5661.5  | -1.247E+14 |
| 5X1  | 4255   | 3.304  | 38295    | 14058.52  | -3.5E+10 | -4975541 | -8.598E+24 |
| 5X2  | 6302   | 3.224  | 56718    | 20317.65  | -1.2E+11 | -1.1E+07 | -1.378E+26 |

| plot | b    | c     |          | $h_{opt}$ | $y_1$    | $y_2$    | curvature  |
|------|------|-------|----------|-----------|----------|----------|------------|
| 6X1  | 6314 | 2.991 | 56826    | 18885.17  | -1.3E+11 | -1.3E+07 | -1.505E+26 |
| 7X1  | 5598 | 2.824 | 50382    | 15808.75  | -9.3E+10 | -1.2E+07 | -6.863E+25 |
| 8X1  | 779  | 2.489 | 7011.009 | 1938.932  | -2.8E+08 | -293864  | -7.868E+19 |
| 9X1  | 8621 | 2.173 | 77589    | 18733.43  | -4.4E+11 | -4.7E+07 | -1.832E+27 |

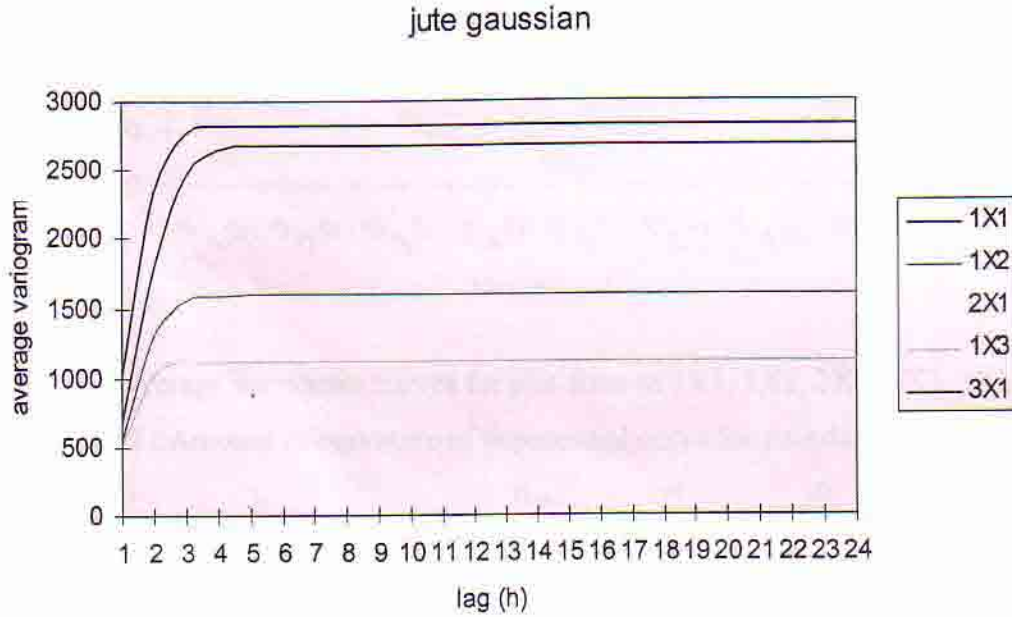


Fig. 5.3.1 : Average variogram curves for plot sizes of 1X1, 1X2, 2X1, 1X3, 3X1.

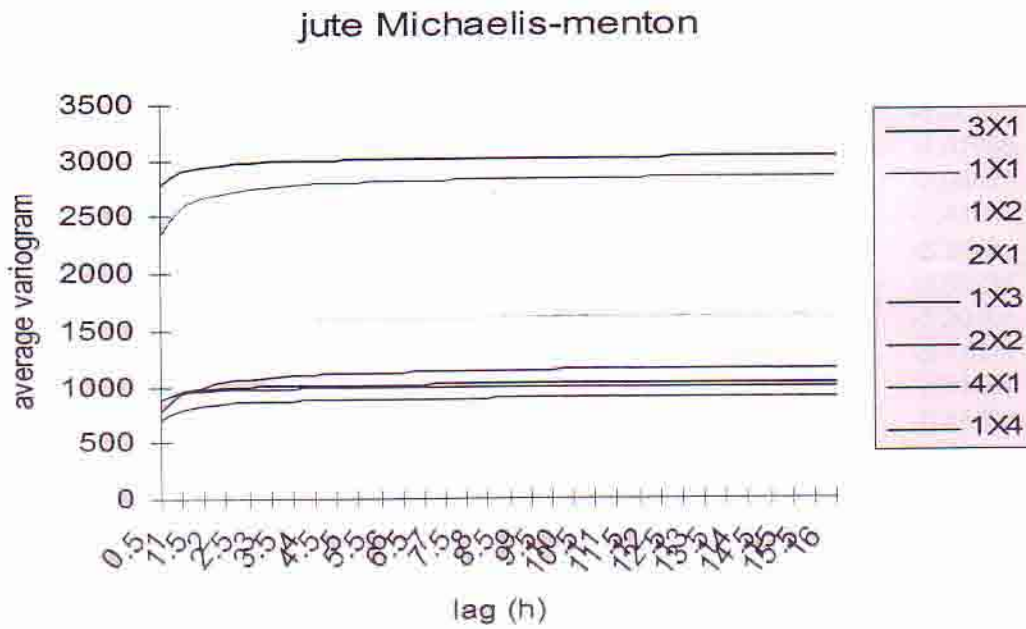


Fig. 5.3.2 : Average variogram curves for plot sizes of 1X1, 1X2, 2X1, 1X3, 3X1, 2X2, 1X4, 4X1.

### jute VB

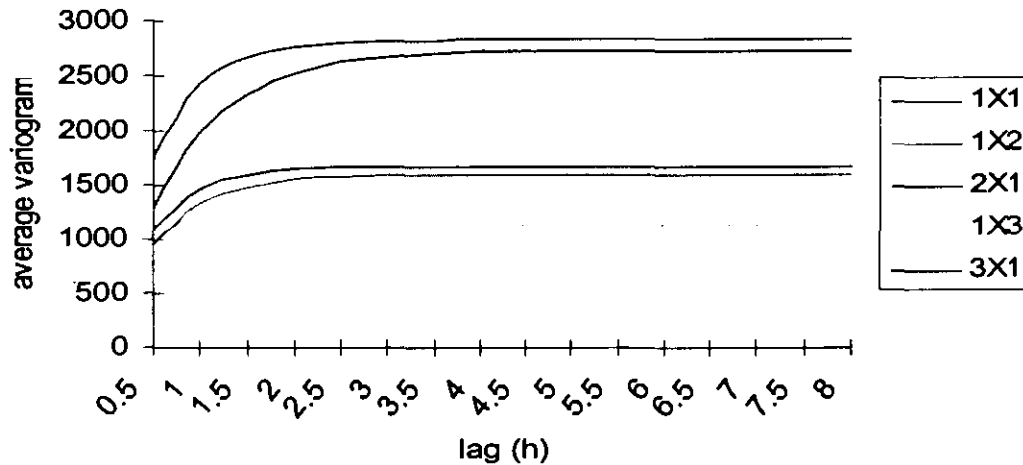


Fig. 5.3.3 : Average variogram curves for plot sizes of 1X1, 1X2, 2X1, 1X3, 3X1.

TABLE 5.3.2 : Amount of curvature of exponential curve for Jute data.

| plot | b       | c       |          | $h_{opt}$ | y1       | y2       | curvature |
|------|---------|---------|----------|-----------|----------|----------|-----------|
| 1X1  | 2832    | 0.5157  | 7766.246 | 4.619405  | 0.707107 | -1.37116 | -1.33983  |
| 1X2  | 1596    | 0.5527  | 4083.743 | 4.595573  | 0.707107 | -1.27937 | -1.43596  |
| 1X3  | 1120    | 0.4265  | 3713.761 | 3.505745  | 0.707107 | -1.65793 | -1.10808  |
| 1X4  | 885.1   | 0.4118  | 3039.632 | 3.302427  | 0.707107 | -1.71711 | -1.06989  |
| 1X5  | 812     | 1.228   | 935.1314 | 8.400364  | 0.707107 | -0.57582 | -3.19044  |
| 1X6  | 952.1   | 0.8488  | 1586.325 | 6.254956  | 0.707107 | -0.83307 | -2.20525  |
| 1X7  | 753.9   | 0.1824  | 5845.261 | 1.582026  | 0.707107 | -3.87668 | -0.47389  |
| 1X8  | 512.1   | 0.06504 | 11134.97 | 0.606033  | 0.707107 | -10.8719 | -0.16898  |
| 1X9  | 465.1   | 0.06579 | 9997.731 | 0.605933  | 0.707107 | -10.7479 | -0.17093  |
| 2X1  | 1673    | 0.4637  | 5102.392 | 3.958822  | 0.707107 | -1.52492 | -1.20473  |
| 2X2  | 1013    | 0.3885  | 3687.512 | 3.190637  | 0.707107 | -1.82009 | -1.00935  |
| 2X3  | 778.8   | 1.57    | 701.522  | 10.28861  | 0.707107 | -0.45039 | -4.07898  |
| 2X4  | 405.7   | 1.522   | 376.9688 | 9.028751  | 0.707107 | -0.46459 | -3.95427  |
| 2X5  | 394.1   | 0.9367  | 595.0054 | 5.984174  | 0.707107 | -0.75489 | -2.43362  |
| 2X6  | 588     | 1.289   | 645.1184 | 8.3391    | 0.707107 | -0.54857 | -3.34892  |
| 2X7  | 475.9   | 1.502   | 448.0854 | 9.169686  | 0.707107 | -0.47078 | -3.90231  |
| 2X8  | 331     | 2.003   | 233.7018 | 10.92445  | 0.707107 | -0.35302 | -5.20395  |
| 2X9  | 162.6   | 1.97    | 116.7265 | 9.376872  | 0.707107 | -0.35894 | -5.11821  |
| 3X1  | 2737    | 0.7756  | 4990.591 | 6.604474  | 0.707107 | -0.91169 | -2.01507  |
| 3X2  | 1611    | 0.3414  | 6673.398 | 3.006329  | 0.707107 | -2.0712  | -0.88698  |
| 3X3  | 1136    | 1.587   | 1012.317 | 10.98203  | 0.707107 | -0.44556 | -4.12315  |
| 3X4  | 5410000 | 17200   | 444.8195 | 104879.9  | 0.707107 | -4.1E-05 | -44686.9  |
| 3X5  | 2583000 | 9892    | 369.2796 | 58477.09  | 0.707107 | -7.1E-05 | -25700.2  |
| 3X6  | 1342    | 3.094   | 613.4048 | 19.86046  | 0.707107 | -0.22854 | -8.03845  |
| 3X7  | 824     | 2.347   | 496.5113 | 14.56925  | 0.707107 | -0.30128 | -6.09768  |
| 3X8  | 575.2   | 2.527   | 321.9057 | 14.59155  | 0.707107 | -0.27982 | -6.56534  |
| 3X9  | 267.6   | 1.067   | 354.68   | 6.264587  | 0.707107 | -0.66271 | -2.77215  |
| 4X1  | 1004    | 0.5014  | 2831.812 | 3.985464  | 0.707107 | -1.41026 | -1.30268  |

| plot | b      | c       | $h_{opt}$ | $y_1$    | $y_2$    | curvature |          |
|------|--------|---------|-----------|----------|----------|-----------|----------|
| 4X2  | 778.1  | 0.8425  | 1306.112  | 6.044778 | 0.707107 | -0.8393   | -2.18888 |
| 4X3  | 1172   | 4.773   | 347.2571  | 27.92236 | 0.707107 | -0.14815  | -12.4006 |
| 4X4  | 189.3  | 0.9018  | 296.8625  | 5.13419  | 0.707107 | -0.78411  | -2.34295 |
| 4X5  | 247.1  | 1.242   | 281.3625  | 7.004438 | 0.707107 | -0.56933  | -3.22681 |
| 4X6  | 413.2  | 1.728   | 338.1673  | 10.06308 | 0.707107 | -0.40921  | -4.48948 |
| 4X7  | 350600 | 3580    | 138.4981  | 17652.47 | 0.707107 | -0.0002   | -9301.11 |
| 4X8  | 246.3  | 1.969   | 176.9024  | 10.19075 | 0.707107 | -0.35912  | -5.11561 |
| 4X9  | 166.4  | 2.438   | 96.52385  | 11.14115 | 0.707107 | -0.29004  | -6.33411 |
| 5X1  | 4992   | 0.6152  | 11475.54  | 5.750873 | 0.707107 | -1.14939  | -1.59834 |
| 5X2  | 8067   | 2.022   | 5642.167  | 17.46608 | 0.707107 | -0.34971  | -5.25331 |
| 6X1  | 6609   | 0.4848  | 19279.16  | 4.783415 | 0.707107 | -1.45855  | -1.25955 |
| 7X1  | 5451   | 0.7885  | 9776.637  | 7.244542 | 0.707107 | -0.89677  | -2.04858 |
| 8X1  | 747.5  | 0.3773  | 2801.815  | 2.995016 | 0.707107 | -1.87412  | -0.98025 |
| 9X1  | 7656   | 0.06809 | 159013.4  | 0.815496 | 0.707107 | -10.3849  | -0.1769  |

TABLE 5.3.3 : Amount of curvature of VB curve for Jute data.

| plot | Li    | K       | $t_0$      | $h_{opt}$ | $y_1$    | $y_2$    | curvature |          |
|------|-------|---------|------------|-----------|----------|----------|-----------|----------|
| 1X1  | 2826  | 1.948   | 0.0007606  | 7785.314  | 4.600347 | 0.707107 | -1.37744  | -1.33371 |
| 1X2  | 1594  | 1.809   | 0.0007208  | 4077.95   | 4.596271 | 0.707107 | -1.27916  | -1.43619 |
| 1X3  | 1121  | 2.341   | -0.0002333 | 3711.265  | 3.510714 | 0.707107 | -1.65534  | -1.10981 |
| 1X4  | 885.7 | 2.43    | -0.0002873 | 3043.743  | 3.300471 | 0.707107 | -1.71827  | -1.06917 |
| 1X5  | 858.4 | 0.7976  | -0.07252   | 968.2552  | 8.54771  | 0.707107 | -0.56399  | -3.25737 |
| 1X6  | 963.5 | 1.177   | -0.01008   | 1603.774  | 6.260196 | 0.707107 | -0.83226  | -2.20737 |
| 1X7  | 753.9 | 5.31    | -3.098E-05 | 5661.392  | 1.627356 | 0.707107 | -3.75474  | -0.48928 |
| 1X8  | 512   | 8.055   | 2.155E-06  | 5832.443  | 1.0765   | 0.707107 | -5.69574  | -0.32254 |
| 1X9  | 482   | 10.13   | 0.001123   | 6905.124  | 0.87378  | 0.707107 | -7.16299  | -0.25647 |
| 2X1  | 1668  | 2.145   | 0.001389   | 5059.858  | 3.977657 | 0.707107 | -1.51674  | -1.21122 |
| 2X2  | 1012  | 2.556   | 0.0006941  | 3658.107  | 3.210671 | 0.707107 | -1.80736  | -1.01646 |
| 2X3  | 766.6 | 0.637   | 0.02475    | 690.5947  | 10.28778 | 0.707107 | -0.45043  | -4.07861 |
| 2X4  | 405   | 0.6572  | 0.002639   | 376.4156  | 9.026823 | 0.707107 | -0.46471  | -3.95325 |
| 2X5  | 383.9 | 1.066   | 0.02459    | 578.7491  | 5.991634 | 0.707107 | -0.75378  | -2.43722 |
| 2X6  | 555.5 | 0.7759  | 0.07317    | 609.5437  | 8.338037 | 0.707107 | -0.54864  | -3.34847 |
| 2X7  | 461.9 | 0.6658  | 0.04463    | 434.9174  | 9.169226 | 0.707107 | -0.47079  | -3.90219 |
| 2X8  | 314.8 | 0.4938  | 0.1039     | 219.837   | 11.0251  | 0.707107 | -0.34917  | -5.26139 |
| 2X9  | 170.7 | 0.507   | -0.09577   | 122.393   | 9.38596  | 0.707107 | -0.3585   | -5.12441 |
| 3X1  | 2731  | 1.29    | 0.001811   | 4982.26   | 6.601531 | 0.707107 | -0.91217  | -2.01401 |
| 3X2  | 1610  | 2.931   | 0.00004159 | 6673.547  | 3.004445 | 0.707107 | -2.07253  | -0.88641 |
| 3X3  | 1148  | 0.6297  | -0.01619   | 1022.329  | 10.98879 | 0.707107 | -0.44527  | -4.1259  |
| 3X4  | 9168  | 0.03584 | 0.02734    | 464.6839  | 171.3822 | 0.707107 | -0.02534  | -72.491  |
| 3X5  | 17310 | 0.0153  | 0.06471    | 374.5446  | 387.3661 | 0.707107 | -0.01082  | -169.809 |
| 3X6  | 1329  | 0.3232  | 0.03119    | 607.4511  | 19.86186 | 0.707107 | -0.22854  | -8.0386  |
| 3X7  | 820   | 0.4261  | 0.01128    | 494.129   | 14.56842 | 0.707107 | -0.3013   | -6.09734 |
| 3X8  | 555.2 | 0.3958  | 0.08862    | 310.7708  | 14.58851 | 0.707107 | -0.27987  | -6.56411 |
| 3X9  | 263   | 0.9372  | 0.0184     | 348.5805  | 6.264526 | 0.707107 | -0.6627   | -2.77217 |
| 4X1  | 994.6 | 2.008   | 0.004607   | 2824.406  | 3.961805 | 0.707107 | -1.41987  | -1.29386 |
| 4X2  | 783.6 | 1.187   | -0.005877  | 1315.407  | 6.044588 | 0.707107 | -0.83934  | -2.18878 |
| 4X3  | 1159  | 0.2096  | 0.05408    | 343.5498  | 27.91349 | 0.707107 | -0.14821  | -12.3954 |
| 4X4  | 186.1 | 1.105   | 0.01586    | 290.8196  | 5.149528 | 0.707107 | -0.78135  | -2.3512  |
| 4X5  | 244.8 | 0.8059  | 0.0113     | 279.0022  | 6.998792 | 0.707107 | -0.56986  | -3.22382 |

| plot | b     | c       |           | $h_{opt}$ | y1       | y2       | curvature | plot     |
|------|-------|---------|-----------|-----------|----------|----------|-----------|----------|
| 4X6  | 409   | 0.5789  | 0.01749   | 334.8435  | 10.06009 | 0.707107 | -0.40934  | -4.48795 |
| 4X7  | 5887  | 0.01702 | -0.01889  | 141.6996  | 291.0334 | 0.707107 | -0.01203  | -152.648 |
| 4X8  | 238.9 | 0.5109  | 0.05359   | 172.6104  | 10.13587 | 0.707107 | -0.36126  | -5.08529 |
| 4X9  | 161.1 | 0.4103  | 0.07797   | 93.47857  | 11.13752 | 0.707107 | -0.29013  | -6.33214 |
| 5X1  | 5017  | 1.627   | -0.003085 | 11543.74  | 5.746085 | 0.707107 | -1.15046  | -1.59685 |
| 5X2  | 8155  | 0.4943  | -0.02162  | 5700.718  | 17.47453 | 0.707107 | -0.34952  | -5.25607 |
| 6X1  | 6652  | 2.073   | -0.003238 | 19501.43  | 4.761954 | 0.707107 | -1.46583  | -1.25329 |
| 7X1  | 5448  | 1.267   | 0.0005757 | 9761.773  | 7.250954 | 0.707107 | -0.8959   | -2.05057 |
| 8X1  | 745.6 | 2.748   | 0.001286  | 2897.595  | 2.902173 | 0.707107 | -1.94313  | -0.94544 |
| 9X1  | 7767  | 15.74   | 4.832E-06 | 172891.3  | 0.766232 | 0.707107 | -11.1299  | -0.16506 |

TABLE 5.3.4 : Amount of curvature of Michaelis-menton curve for Jute data.

| plot | b        | c       | $h_{opt}$ | y1 | y2       | curvature  |
|------|----------|---------|-----------|----|----------|------------|
| 1X1  | 2870     | 0.1153  | 18.07566  | 1  | -0.10994 | -25.725901 |
| 1X2  | 1693     | 0.1868  | 17.59669  | 1  | -0.11246 | -25.149648 |
| 1X3  | 1174     | 0.2657  | 17.39589  | 1  | -0.11324 | -24.977262 |
| 1X4  | 909.3    | 0.1516  | 11.58935  | 1  | -0.17034 | -16.604209 |
| 1X5  | 912.2    | 0.6338  | 23.411    | 1  | -0.08318 | -34.004481 |
| 1X6  | 1018     | 0.4347  | 20.60157  | 1  | -0.09507 | -29.749776 |
| 1X8  | 525.2    | 0.1182  | 7.7608    | 1  | -0.25384 | -11.142589 |
| 2X1  | 1631     | 0.08459 | 11.66132  | 1  | -0.17027 | -16.611218 |
| 2X2  | 1031     | 0.07935 | 8.96553   | 1  | -0.22112 | -12.791392 |
| 2X3  | 984.1    | 1.583   | 37.88636  | 1  | -0.05067 | -55.818103 |
| 2X4  | 506.9    | 1.449   | 25.65263  | 1  | -0.0738  | -38.327486 |
| 2X5  | 436.4    | 0.6315  | 15.9693   | 1  | -0.12048 | -23.477078 |
| 2X6  | 684.1    | 1.127   | 26.63954  | 1  | -0.07203 | -39.267816 |
| 2X7  | 579.3    | 1.408   | 27.15166  | 1  | -0.07003 | -40.389464 |
| 2X8  | 430.7    | 2.289   | 29.1096   | 1  | -0.0637  | -44.404331 |
| 2X9  | 202.2    | 1.65    | 16.61554  | 1  | -0.1095  | -25.831376 |
| 3X1  | 3039     | 0.454   | 36.69039  | 1  | -0.05384 | -52.530106 |
| 3X2  | 1615     | 0.02729 | 6.611486  | 1  | -0.30126 | -9.3886474 |
| 3X3  | 1572     | 1.866   | 52.29443  | 1  | -0.03693 | -76.594412 |
| 3X4  | 12890000 | 40990   | 685894.5  | 1  | -2.8E-06 | -1027969.9 |
| 3X5  | 6087000  | 23310   | 353370.2  | 1  | -5.3E-06 | -532706.24 |
| 3X6  | 2158     | 4.833   | 97.29248  | 1  | -0.01958 | -144.42724 |
| 3X7  | 1228     | 3.235   | 59.79341  | 1  | -0.03173 | -89.135627 |
| 3X8  | 913.7    | 3.963   | 56.21169  | 1  | -0.03324 | -85.09986  |
| 3X9  | 333.4    | 1.048   | 17.64433  | 1  | -0.107   | -26.434947 |
| 4X1  | 1002     | 0.0691  | 8.251849  | 1  | -0.24036 | -11.7676   |
| 4X2  | 947.6    | 0.7014  | 25.07934  | 1  | -0.07758 | -36.459474 |
| 4X3  | 2163     | 8.855   | 129.5407  | 1  | -0.01445 | -195.72105 |
| 4X4  | 238.5    | 0.9104  | 13.82495  | 1  | -0.13573 | -20.838925 |
| 4X5  | 339.1    | 1.494   | 21.01412  | 1  | -0.08886 | -31.831286 |
| 4X6  | 619.2    | 2.435   | 36.39478  | 1  | -0.05151 | -54.913605 |
| 4X7  | 609000   | 6218    | 55318.67  | 1  | -3.3E-05 | -87025.996 |
| 4X8  | 394.6    | 3.132   | 32.02319  | 1  | -0.05689 | -49.716943 |
| 4X9  | 283.7    | 4.218   | 30.37458  | 1  | -0.05782 | -48.921296 |
| 5X1  | 5524     | 0.3414  | 43.08548  | 1  | -0.04605 | -61.414878 |
| 5X2  | 11440    | 2.532   | 167.6622  | 1  | -0.01175 | -240.69101 |

| plot | b    | c      | $h_{opt}$ | y1 | y2       | curvature  |
|------|------|--------|-----------|----|----------|------------|
| 6X1  | 7175 | 0.2254 | 39.98958  | 1  | -0.04973 | -56.872577 |
| 7X1  | 6194 | 0.5116 | 55.78094  | 1  | -0.03553 | -79.609678 |

TABLE 5.3.5 : Amount of curvature of spherical curve for Rice data.

| plot | b      | c     | $h_{opt}$ | y1       | y2       | curvature |            |
|------|--------|-------|-----------|----------|----------|-----------|------------|
| 1X1  | 24170  | 1.268 | 217530    | 30647.56 | -1.7E+13 | -1.1E+09  | -4.275E+30 |
| 1X2  | 9158   | 6.893 | 82422.01  | 63126.1  | -1.7E+11 | -5295488  | -8.818E+26 |
| 1X3  | 7702   | 6.155 | 69318.01  | 47405.81 | -1.1E+11 | -4697558  | -2.939E+26 |
| 1X4  | 7461   | 5.973 | 67149.01  | 44564.55 | -1E+11   | -4680910  | -2.424E+26 |
| 1X5  | 8599   | 5.363 | 77391     | 46116.44 | -1.8E+11 | -7712613  | -7.293E+26 |
| 1X6  | 7458   | 5.301 | 67122     | 39534.86 | -1.2E+11 | -5938140  | -2.724E+26 |
| 1X7  | 6072   | 5.305 | 54648.01  | 32211.96 | -6.3E+10 | -3930194  | -6.453E+25 |
| 1X8  | 6146   | 5.52  | 55314.01  | 33925.92 | -6.3E+10 | -3719018  | -6.751E+25 |
| 1X9  | 5263   | 5.445 | 47367.01  | 28657.04 | -4E+10   | -2802801  | -2.311E+25 |
| 2X1  | 5565   | 5.431 | 50085.01  | 30223.52 | -4.8E+10 | -3149865  | -3.424E+25 |
| 2X2  | 7671   | 3.081 | 69039     | 23634.35 | -2.2E+11 | -1.9E+07  | -5.707E+26 |
| 2X3  | 5806   | 2.947 | 52254     | 17110.28 | -1E+11   | -1.2E+07  | -8.49E+25  |
| 2X4  | 7416   | 2.638 | 66744     | 19563.41 | -2.3E+11 | -2.4E+07  | -5.261E+26 |
| 2X5  | 7211   | 2.263 | 64899     | 16318.49 | -2.5E+11 | -3E+07    | -5.04E+26  |
| 2X6  | 8229   | 2.012 | 74061     | 16556.75 | -4.2E+11 | -5E+07    | -1.429E+27 |
| 2X7  | 6987   | 2.114 | 62883     | 14770.52 | -2.4E+11 | -3.3E+07  | -4.326E+26 |
| 2X8  | 6163   | 2.222 | 55467     | 13694.19 | -1.6E+11 | -2.3E+07  | -1.71E+26  |
| 2X9  | 5190   | 2.044 | 46710     | 10608.36 | -1E+11   | -1.9E+07  | -5.583E+25 |
| 3X1  | 36110  | 5.127 | 324990    | 185136   | -1.4E+13 | -1.5E+08  | -1.757E+31 |
| 3X2  | 31080  | 2.301 | 279720    | 71515.08 | -2E+13   | -5.5E+08  | -1.37E+31  |
| 3X3  | 36640  | 2.445 | 329760    | 89584.8  | -3E+13   | -6.7E+08  | -4.079E+31 |
| 3X4  | 23710  | 1.642 | 213390    | 38931.82 | -1.2E+13 | -6.3E+08  | -2.886E+30 |
| 4X1  | 23890  | 4.652 | 215010    | 111136.3 | -4.4E+12 | -7.9E+07  | -1.074E+30 |
| 4X2  | 38550  | 2.401 | 346950    | 92558.55 | -3.6E+13 | -7.7E+08  | -5.928E+31 |
| 4X3  | 38970  | 2.053 | 350730    | 80005.41 | -4.3E+13 | -1.1E+09  | -7.48E+31  |
| 5X1  | 53520  | 5.78  | 481680    | 309345.6 | -4E+13   | -2.6E+08  | -2.448E+32 |
| 5X2  | 61820  | 2.349 | 556380    | 145215.2 | -1.5E+14 | -2.1E+09  | -1.653E+33 |
| 5X3  | 51710  | 2.454 | 465390    | 126896.3 | -8.5E+13 | -1.3E+09  | -4.532E+32 |
| 6X1  | 41130  | 4.629 | 370170    | 190390.8 | -2.3E+13 | -2.4E+08  | -4.839E+31 |
| 6X2  | 37210  | 2.066 | 334890    | 76875.86 | -3.7E+13 | -9.7E+08  | -5.378E+31 |
| 7X1  | 144400 | 4.641 | 1299600   | 670160.4 | -9.7E+14 | -2.9E+09  | -3.173E+35 |
| 8X1  | 46320  | 9.784 | 416880    | 453194.9 | -1.5E+13 | -6.7E+07  | -5.26E+31  |
| 9X1  | 112400 | 5.129 | 1011600   | 576499.6 | -4.2E+14 | -1.4E+09  | -4.971E+34 |

TABLE 5.3.6 : Amount of curvature of exponential curve for Rice data.

| plot | b     | c      | $h_{opt}$ | y1       | y2       | curvature |             |
|------|-------|--------|-----------|----------|----------|-----------|-------------|
| 1X1  | 24010 | 0.4466 | 76030.6   | 5.019289 | 0.707107 | -1.58331  | -1.16030084 |
| 1X2  | 16590 | 0.6933 | 33840.77  | 7.230718 | 0.707107 | -1.01991  | -1.80124624 |
| 1X3  | 13270 | 0.7179 | 26140.99  | 7.301947 | 0.707107 | -0.98497  | -1.86515891 |
| 1X4  | 11480 | 0.6949 | 23363.32  | 6.989945 | 0.707107 | -1.01757  | -1.80540316 |
| 1X5  | 9573  | 0.5216 | 25955.27  | 5.30161  | 0.707107 | -1.35565  | -1.35515655 |
| 1X6  | 9083  | 0.6304 | 20376.43  | 6.254913 | 0.707107 | -1.12168  | -1.63782724 |
| 1X7  | 7436  | 0.3932 | 26744.89  | 4.00832  | 0.707107 | -1.79834  | -1.02156357 |
| 1X8  | 7807  | 0.5127 | 21534.55  | 5.11542  | 0.707107 | -1.37918  | -1.33203367 |
| 1X9  | 6801  | 0.6068 | 15850.47  | 5.868335 | 0.707107 | -1.1653   | -1.57651265 |

| plot | b      | c       |          | $h_{opt}$ | y1       | y2       | curvature          |
|------|--------|---------|----------|-----------|----------|----------|--------------------|
| 2X1  | 11920  | 0.4901  | 34395.89 | 5.119434  | 0.707107 | -1.44278 | -1.27331715        |
| 2X2  | 8942   | 0.4325  | 29239.07 | 4.44751   | 0.707107 | -1.63493 | -1.12366796        |
| 2X3  | 6577   | 0.4564  | 20379.67 | 4.528535  | 0.707107 | -1.54931 | -1.18576198        |
| 2X4  | 7058   | 0.5025  | 19863.72 | 4.973067  | 0.707107 | -1.40718 | -1.3055333         |
| 2X5  | 5925   | 0.03167 | 264579   | 0.395428  | 0.707107 | -22.3273 | -0.08228107        |
| 2X6  | 6248   | 0.5394  | 16381.18 | 5.234277  | 0.707107 | -1.31091 | -1.40140231        |
| 2X7  | 5896   | 0.5071  | 16442.92 | 4.922749  | 0.707107 | -1.39441 | -1.31748445        |
| 2X8  | 5586   | 0.715   | 11048.67 | 6.656697  | 0.707107 | -0.98896 | -1.85762449        |
| 2X9  | 4124   | 0.4758  | 12257.71 | 4.479138  | 0.707107 | -1.48614 | -1.23616466        |
| 3X1  | 38400  | 0.1029  | 527753.2 | 1.35585   | 0.707107 | -6.87179 | -0.26734204        |
| 3X2  | 26800  | 0.08392 | 451631.6 | 1.092691  | 0.707107 | -8.42596 | -0.21803056        |
| 3X3  | 37930  | 0.7206  | 74439.52 | 8.083505  | 0.707107 | -0.98127 | -1.87217372        |
| 3X4  | 26110  | 0.03449 | 1070604  | 0.47885   | 0.707107 | -20.5018 | -0.08960765        |
| 4X1  | 39670  | 0.076   | 738182.3 | 1.026908  | 0.707107 | -9.30404 | -0.19745379        |
| 4X2  | 38670  | 0.6663  | 82076.6  | 7.539457  | 0.707107 | -1.06124 | -1.73109818        |
| 4X3  | 35190  | 0.04587 | 1084940  | 0.637457  | 0.707107 | -15.4154 | -0.11917376        |
| 5X1  | 61010  | 0.4427  | 194897.6 | 5.392188  | 0.707107 | -1.59726 | -1.15016834        |
| 5X2  | 61250  | 0.6296  | 137580.3 | 7.449404  | 0.707107 | -1.1231  | -1.63574878        |
| 5X3  | 56820  | 1.05    | 76529.16 | 11.8077   | 0.707107 | -0.67343 | <b>-2.72798002</b> |
| 6X1  | 41890  | 0.6105  | 97037.52 | 7.010282  | 0.707107 | -1.15824 | -1.58612553        |
| 6X2  | 31750  | 0.07332 | 612401.5 | 0.977     | 0.707107 | -9.64412 | -0.19049095        |
| 7X1  | 168200 | 0.3188  | 746144   | 4.311029  | 0.707107 | -2.21803 | -0.8282667         |
| 8X1  | 54720  | 0.4232  | 182858.6 | 5.12769   | 0.707107 | -1.67086 | -1.09950585        |
| 9X1  | 139800 | 0.05253 | 3763698  | 0.795352  | 0.707107 | -13.461  | -0.13647694        |

TABLE 5.3.7 : Amount of curvature of VB curve for Rice data.

| plot | Li    | K     | t0         |          | $h_{opt}$ | y1       | y2       | curvature  |
|------|-------|-------|------------|----------|-----------|----------|----------|------------|
| 1X1  | 24060 | 2.212 | -0.001112  | 75265.46 | 5.075189  | 0.707107 | -1.56412 | -1.1745372 |
| 1X2  | 16630 | 1.442 | -0.001668  | 33913.49 | 7.232429  | 0.707107 | -1.01965 | -1.8017172 |
| 1X3  | 13200 | 1.384 | 0.003369   | 25835.98 | 7.344065  | 0.707107 | -0.97864 | -1.8772227 |
| 1X4  | 885.8 | 2.423 | -0.0003071 | 3035.317 | 3.308843  | 0.707107 | -1.71332 | -1.072256  |
| 1X5  | 9560  | 1.914 | 0.000713   | 25877.05 | 5.309549  | 0.707107 | -1.3534  | -1.3574066 |
| 1X6  | 8990  | 1.502 | 0.006646   | 19096.1  | 6.569389  | 0.707107 | -1.06207 | -1.7297445 |
| 1X7  | 7425  | 2.531 | 0.0005997  | 26576.86 | 4.025806  | 0.707107 | -1.78969 | -1.0265019 |
| 1X8  | 7786  | 1.952 | 0.001384   | 21493.6  | 5.111789  | 0.707107 | -1.38027 | -1.3309817 |
| 1X9  | 6729  | 1.578 | 0.006585   | 15016.63 | 6.100954  | 0.707107 | -1.11581 | -1.6464361 |
| 2X1  | 11880 | 2.023 | 0.001398   | 33988.13 | 5.158969  | 0.707107 | -1.43048 | -1.284269  |
| 2X2  | 8907  | 2.343 | 0.001646   | 29513.37 | 4.39456   | 0.707107 | -1.65675 | -1.1088674 |
| 2X3  | 6563  | 2.2   | 0.0008845  | 20419.26 | 4.5119    | 0.707107 | -1.55563 | -1.1809437 |
| 2X4  | 7119  | 1.876 | 0.003532   | 18887.17 | 5.25206   | 0.707107 | -1.32653 | -1.384902  |
| 2X5  | 6651  | 2.971 | -1.113E-05 | 27945.03 | 3.445965  | 0.707107 | -2.10081 | -0.8744787 |
| 2X6  | 6216  | 1.809 | 0.004201   | 15902.47 | 5.352034  | 0.707107 | -1.27916 | -1.4361947 |
| 2X7  | 5883  | 1.961 | 0.00143    | 16315.16 | 4.94781   | 0.707107 | -1.38664 | -1.3248731 |
| 2X8  | 5554  | 1.393 | 0.00456    | 10941.38 | 6.681019  | 0.707107 | -0.985   | -1.8650942 |
| 2X9  | 4120  | 2.054 | 0.001529   | 11967.75 | 4.573083  | 0.707107 | -1.4524  | -1.2648862 |
| 3X1  | 10540 | 4.818 | -2.24      | 71816.2  | 0.080852  | 0.707107 | -3.40684 | -0.5392437 |
| 3X2  | 30570 | 19.16 | -2.534E-05 | 828334.9 | 0.711205  | 0.707107 | -13.5482 | -0.135599  |
| 3X3  | 38420 | 1.395 | -0.01006   | 75796.05 | 8.044278  | 0.707107 | -0.98641 | -1.8624202 |
| 3X4  | 23750 | 20.69 | -0.0003726 | 694926.9 | 0.649775  | 0.707107 | -14.63   | -0.1255716 |

| plot | Li     | K      | t0         |          | $h_{opt}$ | y1       | y2       | curvature  |
|------|--------|--------|------------|----------|-----------|----------|----------|------------|
| 4X1  | 37310  | 20.1   | 0.0003959  | 1060563  | 0.69066   | 0.707107 | -14.2128 | -0.1292575 |
| 4X2  | 39040  | 1.501  | -0.006317  | 82871.56 | 7.538685  | 0.707107 | -1.06137 | -1.7308969 |
| 4X3  | 35370  | 204.1  | -3.383E-06 | 10209232 | 0.07907   | 0.707107 | -144.32  | -0.0127294 |
| 5X1  | 61130  | 2.259  | -0.0009194 | 195292.5 | 5.391845  | 0.707107 | -1.59735 | -1.1501001 |
| 5X2  | 61640  | 1.585  | -0.003738  | 138167.8 | 7.463911  | 0.707107 | -1.12076 | -1.6391648 |
| 5X3  | 57490  | 0.9492 | -0.01105   | 77172.94 | 11.84504  | 0.707107 | -0.67119 | -2.737122  |
| 6X1  | 35120  | 3.138  | 0.0001175  | 155855.6 | 3.810406  | 0.707107 | -2.2189  | -0.8279402 |
| 6X2  | 31870  | 45.95  | -2.275E-05 | 2071012  | 0.316485  | 0.707107 | -32.4916 | -0.0565414 |
| 7X1  | 168200 | 3.137  | 0.00003353 | 746200.5 | 4.31076   | 0.707107 | -2.21819 | -0.8282041 |
| 8X1  | 44950  | 10.58  | 0.0004692  | 672559   | 1.268791  | 0.707107 | -7.48119 | -0.2455649 |
| 9X1  | 145200 | 44.45  | -1.175E-05 | 9127532  | 0.360546  | 0.707107 | -31.4309 | -0.0584494 |

TABLE 5.3.8 : Amount of curvature of Michaelis-menton curve for Rice data.

| plot | b      | c        | $h_{opt}$ | y1   | y2       | curvature |
|------|--------|----------|-----------|------|----------|-----------|
| 1X1  | 24430  | 0.1017   | 49.74337  | 1    | -0.04012 | -70.4916  |
| 1X2  | 17170  | 0.2052   | 59.15206  | 1    | -0.03369 | -83.9438  |
| 1X3  | 13500  | 0.1671   | 47.32869  | 1    | -0.04211 | -67.1692  |
| 1X4  | 11730  | 0.1758   | 45.23493  | 1    | -0.04404 | -64.2205  |
| 1X5  | 9559   | 0.06292  | 24.4616   | 1    | -0.08155 | -34.6829  |
| 1X6  | 8988   | 0.1059   | 30.74583  | 1    | -0.06483 | -43.6309  |
| 1X7  | 7260   | -0.04027 | ----      | ---- | ----     | ----      |
| 1X8  | 7806   | 0.06873  | 23.09388  | 1    | -0.08635 | -32.7569  |
| 1X9  | 6774   | 0.1186   | 28.22565  | 1    | -0.07056 | -40.0848  |
| 2X1  | 12010  | 0.07236  | 29.40719  | 1    | -0.06784 | -41.6904  |
| 2X2  | 8967   | 0.04856  | 20.81858  | 1    | -0.09584 | -29.5106  |
| 2X3  | 6765   | 0.1133   | 27.57198  | 1    | -0.07224 | -39.1529  |
| 2X4  | 7359   | 0.1498   | 33.05228  | 1    | -0.06024 | -46.9548  |
| 2X5  | 6910   | 0.09604  | 25.6651   | 1    | -0.07764 | -36.4318  |
| 2X6  | 6633   | 0.2394   | 39.60957  | 1    | -0.05019 | -56.355   |
| 2X7  | 6264   | 0.2118   | 36.2123   | 1    | -0.05491 | -51.5115  |
| 2X8  | 6538   | 0.5501   | 59.42117  | 1    | -0.03335 | -84.8122  |
| 2X9  | 4258   | 0.1446   | 24.66884  | 1    | -0.0806  | -35.0915  |
| 3X1  | 38490  | -0.00371 | ----      | ---- | ----     | ----      |
| 3X2  | 30130  | -0.02913 | ----      | ---- | ----     | ----      |
| 3X3  | 43870  | 0.4641   | 142.2246  | 1    | -0.01402 | -201.792  |
| 3X4  | 15060  | -0.4682  | ----      | ---- | ----     | ----      |
| 4X1  | 39400  | -0.02508 | ----      | ---- | ----     | ----      |
| 4X2  | 43990  | 0.4038   | 132.8747  | 1    | -0.01501 | -188.484  |
| 4X3  | 42480  | 0.2621   | 105.2557  | 1    | -0.01895 | -149.225  |
| 5X1  | 61720  | 0.06429  | 62.9276   | 1    | -0.03175 | -89.084   |
| 5X2  | 69370  | 0.3795   | 161.8731  | 1    | -0.01233 | -229.46   |
| 5X3  | 72390  | 1.005    | 268.7207  | 1    | -0.00741 | -381.45   |
| 6X1  | 43800  | 0.2414   | 102.5853  | 1    | -0.01945 | -145.419  |
| 6X2  | 28940  | -0.1479  | ----      | ---- | ----     | ----      |
| 7X1  | 167600 | 0.01082  | 42.57359  | 1    | -0.04697 | -60.2235  |
| 8X1  | 57310  | 0.1703   | 98.62187  | 1    | -0.02024 | -139.713  |
| 9X1  | 144400 | -0.01447 | ----      | ---- | ----     | ----      |

Thus using the three criteria i.e. Nugget to sill ratio (NSR), NSR/Range, maximum curvature value of the variogram models we have found optimum plot size and shapes for rice and jute data. These are summarized in the following table:

TABLE 5.3.9: Optimum plot sizes of Jute data for five different models:

| Model            | NSR   | NSR/Range | Curvature |
|------------------|-------|-----------|-----------|
| Michaelis-menton | 2 X 9 | 1 X 5     | 3 X 4     |
| Gaussian         | 2 X 4 | 7 X 1     | -----     |
| VB               | 1 X 5 | 2 X 9     | 3 X 5     |
| Exponential      | 1 X 5 | 1 X 9     | 3 X 4     |
| Spherical        | 1 X 9 | 1 X 9     | 3 X 4     |

TABLE 5.3.10 : Optimum plot sizes of Rice data for five different models:

| Model            | NSR   | NSR/Range | Curvature |
|------------------|-------|-----------|-----------|
| Michaelis-menton | 3 X 4 | 3 X 3     | 3 X 3     |
| Gaussian         | 3 X 4 | 3 X 4     | -----     |
| VB               | 3 X 1 | 3 X 1     | 5 X 3     |
| Exponential      | 3 X 4 | 3 X 4     | 5 X 3     |
| Spherical        | 4 X 1 | 4 X 1     | 7 X 1     |

## Chapter 6

### A CASE STUDY OF MERCER & HALL WHEAT GRAIN YIELD DATA.

6.1 INTRODUCTION: By now we have introduced a new concept of finding optimum plot size and shape using variogram analysis of the uniformity data. Here the average variogram curves are studied for different plot sizes and shapes. Fagroud *et al*(2002) studied the plot size and shape using the concept of nugget to sill ratio of variogram data. However their method is crude compared to our new suggested method as it takes care of the specific amount of curvature of the variogram curves fitted under different models.

6.2 MATERIAL AND METHOD: Mercer and Hall carried out uniformity trial on wheat yield at Rothamsted Experimental Station in 1910. A uniform area of one acre was harvested in separate plots each 1/500 acre in area. The dimension of each plot was 3.3m. (East-West) X 2.51 m. (North-South) i.e. 8.283 sq.m. The data given by Mercer and Hall (1911) consist of 20 X 25 lattice of plots with 20 rows of plots running East to West and 25 columns of plots running North to South. He studied both grain and straw yield. Here we consider only the wheat grain yield data as published in Cressie(1993). The object of their study was to determine the plot size that would “reduce the inevitable error within working limits”. As a matter of interest they concluded that 1/40 acre i.e. 103.54 sq.m., should give adequate precision.

6.3 RESULTS AND DISCUSSIONS: Data is first analysed using the Smith’s model of relating variance per unit area to the plot sizes. The fitted model shows that the heterogeneity coefficient  $b = 0.4570399$ . The analysis of the first row and first column indicates that the index of heterogeneity is more pronounced along the column than along the row direction. This is also reported by the Zhang *et al*(1994). For different plot sizes and shapes the following table shows how the variance per unit area and C.V. decreases with increase in plot size.

TABLE 6.3.1: Mercer & Hall wheat grain yield data.

| Plot size | Width | Length | No.of plots | Plot mean | Variance | Variance per unit area | C.V.     |
|-----------|-------|--------|-------------|-----------|----------|------------------------|----------|
| 1         | 1     | 1      | 500         | 393.982   | 2262.349 | 2262.349               | 12.07267 |
| 2         | 2     | 1      | 250         | 787.964   | 6549.59  | 1637.398               | 10.27072 |
| 2         | 1     | 2      | 240         | 790.2125  | 5511.632 | 1377.908               | 9.394987 |
| 3         | 3     | 1      | 150         | 1178.58   | 11629.64 | 1292.182               | 9.150063 |
| 3         | 1     | 3      | 160         | 1185.319  | 9914.214 | 1101.579               | 8.400285 |
| 4         | 4     | 1      | 125         | 1575.928  | 19526.45 | 1220.403               | 8.866971 |

| Plot size | Width | Length | No.of plots | Plot mean | Variance | Variance per unit area | C.V.     |
|-----------|-------|--------|-------------|-----------|----------|------------------------|----------|
| 4         | 2     | 2      | 120         | 1580.425  | 17110.05 | 1069.378               | 8.276596 |
| 4         | 1     | 4      | 120         | 1580.425  | 15088.13 | 943.0084               | 7.772198 |
| 5         | 5     | 1      | 100         | 1969.91   | 29524.04 | 1180.962               | 8.72251  |
| 5         | 1     | 5      | 100         | 1969.91   | 18497.62 | 739.9046               | 6.90417  |
| 6         | 6     | 1      | 75          | 2357.16   | 36887.79 | 1024.661               | 8.148023 |
| 6         | 3     | 2      | 72          | 2364.5    | 29131.83 | 809.2175               | 7.21846  |
| 6         | 2     | 3      | 80          | 2370.637  | 32581.06 | 905.0295               | 7.614081 |
| 6         | 1     | 6      | 80          | 2370.637  | 23734.89 | 659.3024               | 6.498729 |
| 7         | 7     | 1      | 50          | 2773.64   | 39645.47 | 809.0912               | 7.178715 |
| 7         | 1     | 7      | 60          | 2782.15   | 34488.61 | 703.8492               | 6.675093 |
| 8         | 8     | 1      | 50          | 3144.96   | 48033.3  | 750.5204               | 6.96877  |
| 8         | 4     | 2      | 60          | 3160.85   | 54769.9  | 855.7797               | 7.404011 |
| 8         | 2     | 4      | 60          | 3160.85   | 49942.78 | 780.356                | 7.070212 |
| 8         | 1     | 8      | 60          | 3160.85   | 36256.54 | 566.5085               | 6.02406  |
| 9         | 9     | 1      | 50          | 3535.74   | 64239.02 | 793.0743               | 7.168349 |
| 9         | 3     | 3      | 48          | 3546.75   | 53549.19 | 661.1011               | 6.52448  |
| 9         | 1     | 9      | 40          | 3594.3    | 27916.72 | 344.6508               | 4.648554 |
| 10        | 5     | 2      | 48          | 3951.063  | 78191.32 | 781.9132               | 7.077264 |
| 10        | 2     | 5      | 50          | 3939.82   | 61609.8  | 616.098                | 6.300115 |
| 12        | 6     | 2      | 36          | 4729      | 102277.9 | 710.2635               | 6.762724 |
| 12        | 4     | 3      | 40          | 4741.275  | 108584.2 | 754.0569               | 6.950054 |
| 12        | 3     | 4      | 36          | 4729      | 85859.2  | 596.2444               | 6.196181 |
| 12        | 2     | 6      | 40          | 4741.275  | 83059.7  | 576.8035               | 6.07855  |
| 14        | 7     | 2      | 24          | 5567.208  | 101764.5 | 519.2067               | 5.730081 |
| 14        | 2     | 7      | 30          | 5564.3    | 118021.2 | 602.1492               | 6.174042 |
| 15        | 5     | 3      | 32          | 5926.594  | 151451.1 | 673.116                | 6.566456 |
| 15        | 3     | 5      | 30          | 5892.9    | 92654.34 | 411.7971               | 5.165399 |
| 16        | 8     | 2      | 24          | 6310.708  | 128812.5 | 503.1739               | 5.687232 |
| 16        | 4     | 4      | 30          | 6321.7    | 168823.2 | 659.4655               | 6.499533 |
| 16        | 2     | 8      | 30          | 6321.7    | 122619.6 | 478.9828               | 5.539187 |
| 18        | 9     | 2      | 24          | 7093.5    | 183263.7 | 565.6285               | 6.035005 |
| 18        | 6     | 3      | 24          | 7093.5    | 192991.7 | 595.6533               | 6.193109 |
| 18        | 3     | 6      | 24          | 7093.5    | 147996.9 | 456.7805               | 5.423326 |
| 18        | 2     | 9      | 20          | 7188.6    | 88890.95 | 274.3548               | 4.147481 |
| 20        | 5     | 4      | 24          | 7902.125  | 238813.2 | 597.033                | 6.184225 |
| 20        | 4     | 5      | 25          | 7879.64   | 207941.3 | 519.8533               | 5.78714  |
| 21        | 7     | 3      | 16          | 8350.813  | 172776.3 | 391.7829               | 4.977523 |
| 21        | 3     | 7      | 18          | 8323.5    | 196994.4 | 446.6992               | 5.332378 |
| 24        | 8     | 3      | 16          | 9466.063  | 236309.3 | 410.2592               | 5.135362 |
| 24        | 6     | 4      | 18          | 9458      | 311433.4 | 540.683                | 5.900425 |
| 24        | 4     | 6      | 20          | 9482.55   | 276948.2 | 480.8129               | 5.549759 |
| 24        | 3     | 8      | 18          | 9458      | 178162.8 | 309.3105               | 4.462819 |
| 25        | 5     | 5      | 20          | 9849.55   | 283828.2 | 454.1252               | 5.408931 |
| 27        | 9     | 3      | 16          | 10640.25  | 345077.6 | 473.3575               | 5.520858 |
| 27        | 3     | 9      | 12          | 10737.92  | 165860.4 | 227.5176               | 3.792724 |
| 28        | 7     | 4      | 12          | 11134.42  | 271122.9 | 345.82                 | 4.676443 |

| Plot size | Width | Length | No.of plots | Plot mean | Variance | Variance per unit area | C.V.     |
|-----------|-------|--------|-------------|-----------|----------|------------------------|----------|
| 28        | 4     | 7      | 15          | 11128.6   | 426216   | 543.6429               | 5.866436 |
| 30        | 6     | 5      | 15          | 11785.8   | 341403.4 | 379.3372               | 4.957639 |
| 30        | 5     | 6      | 16          | 11853.19  | 397731.2 | 441.9236               | 5.320589 |
| 32        | 8     | 4      | 12          | 12621.42  | 390365.1 | 381.2159               | 4.950253 |
| 32        | 4     | 8      | 15          | 12643.4   | 403748.6 | 394.2857               | 5.025642 |
| 35        | 7     | 5      | 10          | 13868.2   | 178292   | 145.5445               | 3.044709 |
| 35        | 5     | 7      | 12          | 13910.75  | 587522.6 | 479.6103               | 5.510128 |
| 36        | 9     | 4      | 12          | 14187     | 575818.2 | 444.3042               | 5.348748 |
| 36        | 6     | 6      | 12          | 14187     | 564647.3 | 435.6846               | 5.29661  |
| 36        | 4     | 9      | 10          | 14377.2   | 305756.4 | 235.9232               | 3.846037 |
| 40        | 8     | 5      | 10          | 15724.8   | 352451.6 | 220.2822               | 3.775414 |
| 40        | 5     | 8      | 12          | 15804.25  | 560494.6 | 350.3091               | 4.737092 |
| 42        | 7     | 6      | 8           | 16701.63  | 482860.6 | 273.7305               | 4.160563 |
| 42        | 6     | 7      | 9           | 16647     | 787818   | 446.6089               | 5.331838 |
| 45        | 9     | 5      | 10          | 17678.7   | 626602.7 | 309.4334               | 4.477605 |
| 45        | 5     | 9      | 8           | 17971.5   | 409680   | 202.3111               | 3.561542 |
| 48        | 8     | 6      | 8           | 18932.13  | 792484.6 | 343.9603               | 4.702145 |
| 48        | 6     | 8      | 9           | 18916     | 660584   | 286.7118               | 4.296697 |
| 49        | 7     | 7      | 6           | 19602.67  | 298393.6 | 124.2789               | 2.786632 |
| 54        | 9     | 6      | 8           | 21280.5   | 1168376  | 400.6776               | 5.079366 |
| 54        | 6     | 9      | 6           | 21475.83  | 623596.8 | 213.8535               | 3.67707  |
| 56        | 8     | 7      | 6           | 22220.67  | 750009.6 | 239.1612               | 3.897412 |
| 56        | 7     | 8      | 6           | 22268.83  | 387718.4 | 123.6347               | 2.796152 |
| 63        | 9     | 7      | 6           | 24970.5   | 1487230  | 374.7116               | 4.883845 |
| 63        | 7     | 9      | 4           | 25193.25  | 393270.7 | 99.08558               | 2.48921  |
| 64        | 8     | 8      | 6           | 25242.83  | 710451.2 | 173.45                 | 3.339097 |
| 72        | 9     | 8      | 6           | 28374     | 1127955  | 217.584                | 3.743048 |
| 72        | 8     | 9      | 4           | 28629.75  | 875573.3 | 168.8992               | 3.268351 |
| 81        | 9     | 9      | 4           | 32213.75  | 1303589  | 198.6876               | 3.544289 |

TABLE 6.3.1A: Average values for same plot sizes but different shapes.

| Plot size | No.of plots | Plot mean | Variance | Variance per sq.m. | C.V.     |
|-----------|-------------|-----------|----------|--------------------|----------|
| 1         | 500         | 393.982   | 2262.349 | 2262.349           | 12.07267 |
| 2         | 245         | 789.0883  | 6030.611 | 1507.653           | 9.832854 |
| 3         | 155         | 1181.95   | 10771.93 | 1196.881           | 8.775174 |
| 4         | 122         | 1578.926  | 17241.54 | 1077.596           | 8.305255 |
| 5         | 100         | 1969.91   | 24010.83 | 960.4333           | 7.81334  |
| 6         | 76.8        | 2365.734  | 30583.89 | 849.5526           | 7.369823 |
| 7         | 55          | 2777.895  | 37067.04 | 756.4702           | 6.926904 |
| 8         | 57.5        | 3156.878  | 47250.63 | 738.2912           | 6.866763 |
| 9         | 46          | 3558.93   | 48568.31 | 599.6087           | 6.113794 |
| 10        | 49          | 3945.442  | 69900.56 | 699.0056           | 6.68869  |
| 12        | 38          | 4735.138  | 94945.25 | 659.3421           | 6.496877 |
| 14        | 27          | 5565.754  | 109892.9 | 560.678            | 5.952062 |
| 15        | 31          | 5909.747  | 122052.7 | 542.4566           | 5.865928 |

| Plot size | No. of plots | Plot mean | Variance | Variance per sq.m. | C.V.     |
|-----------|--------------|-----------|----------|--------------------|----------|
| 16        | 28           | 6318.036  | 140085.1 | 547.2074           | 5.908651 |
| 18        | 23           | 7117.275  | 153285.8 | 473.1043           | 5.44973  |
| 20        | 24.5         | 7890.883  | 223377.3 | 558.4432           | 5.985683 |
| 21        | 17           | 8337.157  | 184885.4 | 419.2411           | 5.154951 |
| 24        | 18           | 9466.153  | 250713.4 | 435.2664           | 5.262091 |
| 25        | 20           | 9849.55   | 283828.2 | 454.1252           | 5.408931 |
| 27        | 14           | 10689.09  | 255469   | 350.4376           | 4.656791 |
| 28        | 13.5         | 11131.51  | 348669.5 | 444.7315           | 5.27144  |
| 30        | 15.5         | 11819.5   | 369567.3 | 410.6304           | 5.139114 |
| 32        | 13.5         | 12632.41  | 397056.9 | 387.7508           | 4.987948 |
| 35        | 11           | 13889.48  | 382907.3 | 312.5774           | 4.277419 |
| 36        | 11.3         | 14250.4   | 482074   | 371.9707           | 4.830465 |
| 40        | 11           | 15764.53  | 456473.1 | 285.2957           | 4.256253 |
| 42        | 8.5          | 16674.32  | 635339.3 | 360.1697           | 4.746201 |
| 45        | 9            | 17825.1   | 518141.4 | 255.8723           | 4.019574 |
| 48        | 8.5          | 18924.07  | 726534.3 | 315.3361           | 4.499421 |
| 49        | 6            | 19602.67  | 298393.6 | 124.2789           | 2.786632 |
| 54        | 7            | 21378.17  | 895986.4 | 307.2656           | 4.378218 |
| 56        | 6            | 22244.75  | 568864   | 181.398            | 3.346782 |
| 63        | 5            | 25081.88  | 940250.4 | 236.8986           | 3.686528 |
| 64        | 6            | 25242.83  | 710451.2 | 173.45             | 3.339097 |
| 72        | 5            | 28501.88  | 1001764  | 193.2416           | 3.5057   |
| 81        | 4            | 32213.75  | 1303589  | 198.6876           | 3.544289 |

The relation  $y = a x^{-b}$  in estimated form was  $y = 12.41195 x^{-0.2852526}$  with  $\phi = 0.976363$ , thus indicating a good fit. It is found that  $x_{opt} = 2.311197$  units when units plots were 3.3 m. x 2.51 m. Model 3 i.e.  $y = a' .x_1^{b_1} .x_2^{b_2}$  applied to C. V. data resulted in  $y = 12.41203 x_1^{-0.227} .x_2^{-0.3434}$ , which too was a good fit since  $\phi = 0.982$ . The relative magnitude of  $b_1$  and  $b_2$  again indicate the C.V values to expectedly fall at a higher rate as the plot size was increased along length than along width of the wheat field. For attaining  $x_2 > x_1$  with  $x_1 x_2 = 2.311197$  it is sufficient to evaluate conditional maxima of  $x_2$  at different  $x_1$ ,s which be possibly due to  $b_2 > b_1$ . The equation  $x_{02} = 2.603391 x_1^{-0.169}$  gave an excellent fit to the underlying relationship between  $x_{02}$  &  $x_1$ . its solution provided  $x_{1opt} = .403109$  unit  $x_{2opt} = 5.733429$  units. Accordingly optimum plot size is 19.14sq. mt. with 1.33026 m. along the width and 14.391 m. along the length of the wheat field. The above mentioned data is again analysed for finding different variogram values for different lags and also for different plot sizes and shapes. Here in the following table we present only the robust variogram values for the basic plot size.

TABLE 6.3.2: Robust variogram values for basic plot size average over same lag distance.

| LAG   | AV-ve   | AV+ve   | Average | LAG   | AV-ve   | AV+ve   | Average |
|-------|---------|---------|---------|-------|---------|---------|---------|
| 1     | 2632.37 | 2632.37 | 2632.37 | 8.602 | 5300.65 | 4442.58 | 4871.61 |
| 1.414 | 3638.12 | 3349.26 | 3493.69 | 8.944 | 5212.14 | 4558.18 | 4885.16 |
| 2     | 3111.44 | 3111.44 | 3111.44 | 9     | 4206.07 | 4206.07 | 4206.07 |
| 2.236 | 4033.18 | 3518.14 | 3775.66 | 9.055 | 4479.2  | 4331.42 | 4405.31 |
| 2.828 | 4304.04 | 3919.42 | 4111.73 | 9.22  | 4435.49 | 4469.49 | 4452.49 |
| 3     | 3106.62 | 3106.62 | 3106.62 | 9.434 | 4762.81 | 5041.57 | 4902.19 |
| 3.162 | 3853.99 | 3754.68 | 3804.33 | 9.487 | 4360.61 | 4270.95 | 4315.78 |
| 3.606 | 3891.22 | 3596.62 | 3743.92 | 9.849 | 4740.63 | 4209.41 | 4475.02 |
| 4     | 3538.74 | 3538.74 | 3538.74 | 9.899 | 4459.5  | 4418.51 | 4439.01 |
| 4.123 | 4130.9  | 4074.23 | 4102.56 | 10    | 4324.84 | 5058.19 | 4691.51 |
| 4.243 | 3472.8  | 3399.89 | 3436.34 | 10.05 | 4689.96 | 5012.51 | 4851.23 |
| 4.472 | 4679.13 | 3888.93 | 4284.03 | 10.2  | 4295.23 | 4866.86 | 4581.05 |
| 5     | 3999.37 | 3842.75 | 3921.06 | 10.3  | 4034.9  | 4886.85 | 4460.88 |
| 5.099 | 4477.63 | 3994.64 | 4236.13 | 10.44 | 4548.38 | 4916.96 | 4732.67 |
| 5.385 | 4762.64 | 4122.37 | 4442.5  | 10.63 | 3748.48 | 4722.54 | 4235.51 |
| 5.657 | 4772.83 | 4010.12 | 4391.47 | 10.77 | 4612.23 | 5024.61 | 4818.42 |
| 5.831 | 4339.92 | 3991.92 | 4165.92 | 10.82 | 3834.33 | 5160.09 | 4497.21 |
| 6     | 3824.31 | 3824.31 | 3824.31 | 11    | 5214.65 | 5214.65 | 5214.65 |
| 6.083 | 4303.86 | 3887.66 | 4095.76 | 11.05 | 5080.37 | 5252.22 | 5166.29 |
| 6.325 | 4852.01 | 3762    | 4307.01 | 11.18 | 4695.72 | 4991.2  | 4843.46 |
| 6.403 | 5019.91 | 4239.83 | 4629.87 | 11.31 | 3807.52 | 4530.09 | 4168.81 |
| 6.708 | 4262.33 | 3661.54 | 3961.94 | 11.4  | 4174.64 | 4703.79 | 4439.21 |
| 7     | 4283.22 | 4283.22 | 4283.22 | 11.66 | 3840.39 | 5602.72 | 4721.55 |
| 7.071 | 4939.01 | 4387.29 | 4663.15 | 11.71 | 5352.14 | 4956.73 | 5154.43 |
| 7.211 | 4851.03 | 3694.34 | 4272.69 | 12.04 | 3351.17 | 5035.98 | 4193.58 |
| 7.28  | 4779.85 | 4217.33 | 4498.59 | 12.08 | 4728.49 | 5747.08 | 5237.79 |
| 7.616 | 4637.96 | 3915.67 | 4276.82 | 12.21 | 3859.29 | 5644.99 | 4752.14 |
| 7.81  | 5075.93 | 4600.5  | 4838.21 | 12.53 | 4027.06 | 5648.92 | 4837.99 |
| 8     | 4360.08 | 4360.08 | 4360.08 | 12.73 | 3401.14 | 4713.59 | 4057.36 |
| 8.062 | 5019.8  | 4267.12 | 4643.46 | 12.81 | 4672.86 | 5649.8  | 5161.33 |
| 8.246 | 4872.12 | 4906.9  | 4889.51 | 13.04 | 3864.88 | 5896.47 | 4880.67 |
| 8.485 | 4796.28 | 3914.4  | 4355.34 | 13.45 | 4353.07 | 5247.73 | 4800.4  |
| 8.544 | 4613.43 | 4601.32 | 4607.37 | 13.6  | 4607.16 | 5475.81 | 5041.49 |

Now different number of units along row and column directions are used to construct larger plots with different plot shapes. For each size and shape we find the variogram values and fit a number of models like spherical, exponential, Gaussian, Michaelis-menton and VB. From the fit for each model we find the variogram parameters like range, nugget and sill. The fit for each model are given in the following:

Mercer and Hall (1 X 1) Spherical model  $y=a+b*(1.5*(x/c)-0.5*(x/c)^3)$  Rsq.= 0.645465

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 2.347e+3 | 2.071e+2 | 8.823e+0 | 0.9286223    |
| b         | 2.443e+3 | 2.364e+2 | 9.674e+0 | 0.9229586    |
| c         | 1.085e+1 | 6.093e-1 | 5.618e+0 | 0.2312960    |

|  |           |          |          |              |
|--|-----------|----------|----------|--------------|
| (1 X 1) Exponential model $y = a - b \cdot \exp(-x/c)$ Rsq.= 0.781267                          |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| a  | 4.646e+3  | 6.283e+1 | 1.352e+0 | 0.5217601    |
| b  | 3.992e+3  | 3.072e+2 | 7.696e+0 | 0.4043345    |
| c  | 2.118e+0  | 2.428e-1 | 1.146e+1 | 0.6447663    |
| (1 X 1) Gaussian model $y = a - b / \exp(x/c)^2$ Rsq.= 0.781271                                |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| a  | 4.647e+3  | 6.295e+1 | 1.355e+0 | 0.5234602    |
| b  | 3.990e+3  | 3.070e+2 | 7.692e+0 | 0.4050133    |
| c  | 4.241e+0  | 4.872e-1 | 1.149e+1 | 0.6460648    |
| (1 X 1) Michaelis-menton model $y = a - b / (1+x/c)$ Rsq.= 0.826949                            |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| a  | 5.136e+3  | 1.066e+2 | 2.075e+0 | 0.8685361    |
| b  | 5.019e+3  | 3.061e+2 | 6.100e+0 | 0.6475390    |
| c  | 1.156e+0  | 2.062e-1 | 1.784e+1 | 0.8829620    |
| (1 X 1) VB model $y = li \cdot (1 - \exp(-k \cdot (t-t_0)))$ Rsq.= 0.78129                     |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| li   | 4.646e+3  | 6.260e+1 | 1.348e+0 | 0.4557491    |
| k  | 4.730e-1  | 5.507e-2 | 1.164e+1 | 0.7125638    |
| t0   | -3.192e-1 | 1.873e-1 | 5.869e+1 | 0.5612791    |
| (3 X 1) Spherical model $y = a + b \cdot (1.5 \cdot (x/c) - 0.5 \cdot (x/c)^3)$ Rsq.= 0.163940 |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| a  | 4.057e+3  | 7.760e+2 | 1.913e+1 | 0.8943563    |
| b  | 2.223e+3  | 1.545e+3 | 6.951e+1 | 0.9377237    |
| c  | 1.322e+1  | 1.680e+1 | 1.270e+2 | 0.9614503    |
| (6 X 1) Exponential model $y = a - b \cdot \exp(-x/c)$ Rsq.= 0.877393                          |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| a  | 2.713e+4  | 1.298e+3 | 4.784e+0 | 0.2222222    |
| b  | 2.339e+4  | 3.671e+3 | 1.569e+1 | 0.1250000    |
| c  | 2.087e-2  | 4.948e+5 | 2.371e+9 | 0.1250000    |
| (7 X 2) Spherical model $y = a + b \cdot (1.5 \cdot (x/c) - 0.5 \cdot (x/c)^3)$ Rsq.= 0.245716 |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| a  | 7.796e+2  | 1.515e+3 | 1.943e+2 | 0.7575758    |
| b  | 1.718e+3  | 2.141e+3 | 1.246e+2 | 0.7372188    |
| c  | 2.591e+0  | 8.182e-1 | 3.158e+1 | 0.1574018    |
| (7 X 2) Gaussian model $y = a - b / \exp(x/c)^2$ Rsq.= 0.578916                                |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| a  | 2.361e+3  | 7.625e+2 | 3.230e+1 | 0.4000145    |
| b  | 2.437e+3  | 1.525e+3 | 6.256e+1 | 0.2500045    |
| c  | 8.253e-2  | 5.776e+2 | 6.998e+5 | 0.2500114    |
| (7 X 2) Michaelis-menton model $y = a - b / (1+x/c)$ Rsq.= 0.637873                            |           |          |          |              |
| Parameter  | Value     | StdErr   | CV(%)    | Dependencies |
| a  | 1.696e+3  | 7.971e+2 | 4.699e+1 | 0.5796912    |
| b  | 1.716e+3  | 1.347e+3 | 7.848e+1 | 0.5401640    |
| c  | -4.147e-1 | 4.254e-1 | 1.026e+2 | 0.7335319    |

(4 X 3) Spherical model  $y=a+b*(1.5*(x/c)-0.5*(x/c)^3)$  Rsq.= 0.9622942

| Parameter | Value     | StdErr    | CV(%)    | Dependencies |
|-----------|-----------|-----------|----------|--------------|
| a         | -6.036e+1 | 1.760e+2  | 2.916e+2 | 0.8122625    |
| b         | 9.063e+5  | 3.263e+10 | 3.601e+6 | 1.0000000    |
| c         | 1.947e+3  | 7.014e+7  | 3.603e+6 | 1.0000000    |

(4 X 3) Exponential model  $y = a - b*exp(-x/c)$  Rsq.= 0.962307

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 5.366e+6 | 1.079e+4 | 2.011e-1 | 0.9999500    |
| b         | 5.366e+6 | 1.079e+4 | 2.011e-1 | 0.9999500    |
| c         | 7.680e+3 | 8.784e+2 | 1.144e+1 | 0.7391650    |

(4 X 3) Michaelis-menton model  $y = a - b / (1+x/c)$  Rsq.= 0.962301

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 9.177e+6 | 1.079e+4 | 1.176e-1 | 0.9999500    |
| b         | 9.177e+6 | 1.079e+4 | 1.176e-1 | 0.9999500    |
| c         | 1.313e+4 | 1.106e+3 | 8.423e+0 | 0.7391696    |

(3 X 6) Gaussian model  $y = a - b / exp(x/c)^2$  Rsq.= 0.93373

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 1.561e+3 | 2.468e+2 | 1.581e+1 | 0.5018041    |
| b         | 1.510e+3 | 4.270e+2 | 2.827e+1 | 0.3341371    |
| c         | 1.356e-2 | 4.998e+3 | 3.686e+7 | 0.3357385    |

(1 X 7) Exponential model  $y = a - b*exp(-x/c)$  Rsq.= 0.757976

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| a         | 1.083e+3 | 2.974e+2 | 2.747e+1 | 0.9519928    |
| b         | 9.719e+2 | 2.850e+2 | 2.933e+1 | 0.7865196    |
| c         | 3.397e+0 | 2.667e+0 | 7.850e+1 | 0.9134872    |

(1 X 7) VB model  $y = li * (1-exp(-k * (t-t0)))$  Rsq.= 0.757993

| Parameter | Value     | StdErr   | CV(%)    | Dependencies |
|-----------|-----------|----------|----------|--------------|
| li        | 1.086e+3  | 3.035e+2 | 2.796e+1 | 0.9030766    |
| k         | 2.919e-1  | 2.398e-1 | 8.215e+1 | 0.9334464    |
| t0        | -3.718e-1 | 7.581e-1 | 2.039e+2 | 0.6389446    |

(3 X 5) VB model  $y = li * (1-exp(-k * (t-t0)))$  Rsq.= 0.85441

| Parameter | Value    | StdErr   | CV(%)    | Dependencies |
|-----------|----------|----------|----------|--------------|
| li        | 7.380e+4 | 4.778e+6 | 6.474e+3 | 0.9999869    |
| k         | 1.965e-2 | 1.321e+0 | 6.723e+3 | 0.9999869    |
| t0        | 6.277e-2 | 5.427e-1 | 8.646e+2 | 0.6894852    |

.....  
Using the variogram parameters found after fitting we compute the nugget to sill ratios for different plot sizes and shapes and also for different models. The values of NSR and NSR/range are shown in the following tables:

Table 6.3.3: Nugget to Sill ratios under spherical model.

| M&Hall | a    | b    | NSR         | c     | NSR/range   |
|--------|------|------|-------------|-------|-------------|
| 1X1    | 2347 | 2443 | 0.489979123 | 10.85 | 0.045159366 |
| 2X1    | 1505 | 2195 | 0.406756757 | 9.259 | 0.04393096  |
| 3X1    | 4057 | 2223 | 0.646019108 | 13.22 | 0.048866801 |
| 4X1    | 1054 | 1843 | 0.363824646 | 9.662 | 0.037655211 |

| M&Hall | a     | b      | NSR         | c     | NSR/range    |
|--------|-------|--------|-------------|-------|--------------|
| 5X1    | 1117  | 1727   | 0.392756681 | 10.62 | 0.036982738  |
| 6X1    | 14190 | 18960  | 0.428054299 | 6.874 | 0.062271501  |
| 7X1    | 1619  | 1342   | 0.546774738 | 6.932 | 0.07887691   |
| 8X1    | 13440 | 20220  | 0.399286988 | 6.993 | 0.057098096  |
| 9X1    | 31440 | 44130  | 0.41603811  | 7.125 | 0.058391314  |
| 1X2    | 1505  | 2194   | 0.406866721 | 9.259 | 0.043942836  |
| 2X2    | 455.8 | 1871   | 0.195891353 | 5.092 | 0.038470415  |
| 3X2    | 1182  | 4071   | 0.225014278 | 5.401 | 0.041661596  |
| 4X2    | 295.7 | 1758   | 0.143984029 | 4.916 | 0.029288859  |
| 5X2    | 292.6 | 1850   | 0.136563054 | 5.512 | 0.02477559   |
| 6X2    | 2908  | 26300  | 0.099561764 | 2.107 | 0.047252854  |
| 7X2    | 779.6 | 1718   | 0.312139654 | 2.591 | 0.120470727  |
| 8X2    | 2952  | 34200  | 0.079457364 | 2.85  | 0.027879777  |
| 9X2    | 7777  | 75360  | 0.093544391 | 2.92  | 0.03203575   |
| 1X3    | 914.5 | 1210   | 0.430454225 | 6.348 | 0.067809424  |
| 2X3    | 47.19 | 1757   | 0.026155782 | 3.332 | 0.007849874  |
| 3X3    | 201.9 | 3225   | 0.058916222 | 2.536 | 0.023231949  |
| 4X3    | -60.4 | 906300 | -6.6605E-05 | 1947  | -3.4209E-08  |
| 5X3    | -6.44 | 559600 | -1.1508E-05 | 1351  | -8.5184E-09  |
| 1X4    | 967.7 | 821.3  | 0.540916713 | 5.904 | 0.091618684  |
| 2X4    | 167.6 | 1383   | 0.108087192 | 3.011 | 0.03589744   |
| 3X4    | 188.8 | 3193   | 0.055828257 | 2.02  | 0.027637751  |
| 4X4    | -33.5 | 1499   | -0.02288003 | 2.462 | -0.00929327  |
| 5X4    | -10.5 | 1931   | -0.00548303 | 3.544 | -0.001547131 |
| 1X5    | 471.9 | 558.9  | 0.457799767 | 7.787 | 0.058790262  |
| 2X5    | 109.8 | 615.6  | 0.151364764 | 2.972 | 0.050930271  |
| 3X5    | -88.7 | 401100 | -0.00022112 | 421.6 | -5.24469E-07 |
| 1X6    | 502.7 | 748.9  | 0.401645893 | 7.802 | 0.051479863  |
| 2X6    | 120.1 | 882.9  | 0.119740778 | 2.64  | 0.045356355  |
| 3X6    | 67.29 | 1675   | 0.038621584 | 1.523 | 0.025358887  |
| 1X7    | 245.7 | 1272   | 0.161889702 | 16.46 | 0.00983534   |
| 2X7    | 29.25 | 519.5  | 0.053302961 | 2.037 | 0.026167384  |
| 1X8    | 233.2 | 801    | 0.2254883   | 11.29 | 0.019972392  |
| 2X8    | 18.07 | 610.3  | 0.028756943 | 1.905 | 0.015095508  |
| 1X9    | 127.7 | 436.5  | 0.226338178 | 5.297 | 0.042729503  |
| 2X9    | 27.77 | 439.9  | 0.059379477 | 2.128 | 0.02790389   |

Nugget-Sill / Range ratio (Mercer & Hall)

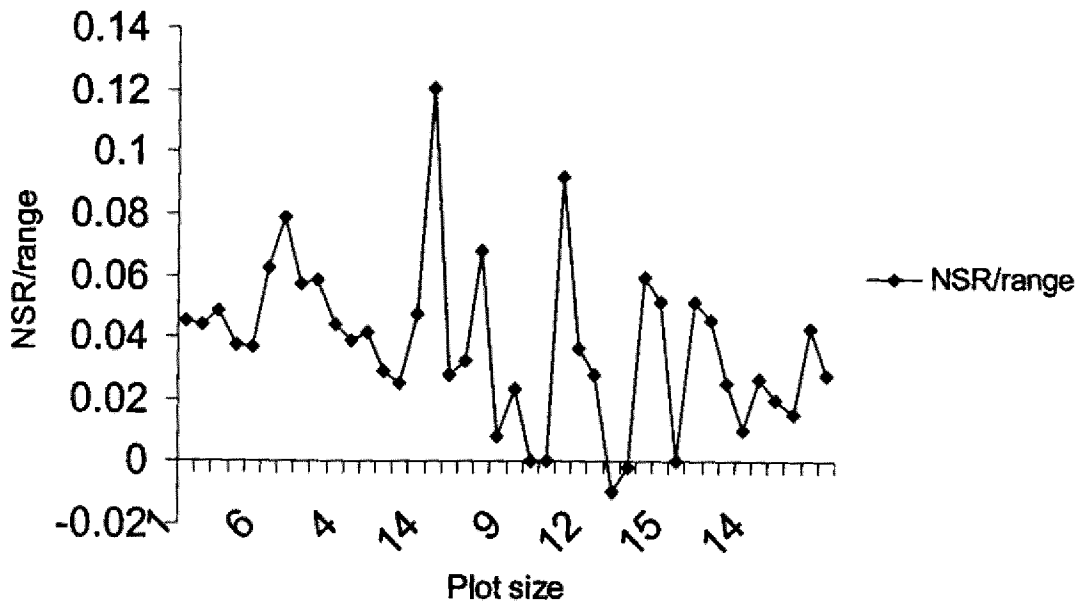


Table 6.3.4: Nugget to Sill ratios under exponential model.

| M&Hall | a     | b      | NSR         | c        | NSR/range          |
|--------|-------|--------|-------------|----------|--------------------|
| 1X1    | 4646  | 3992   | 0.140766251 | 2.118    | 0.066461875        |
| 2X1    | 3586  | 3280   | 0.085331846 | 2.036    | 0.041911516        |
| 3X1    | 5626  | 5584   | 0.007465339 | 0.6303   | 0.011844105        |
| 4X1    | 2741  | 2500   | 0.087924115 | 2.006    | 0.043830566        |
| 5X1    | 2618  | 2408   | 0.080213904 | 1.831    | 0.043808795        |
| 6X1    | 27130 | 23390  | 0.137854773 | 0.02087  | <b>6.605403609</b> |
| 7X1    | 2888  | 2882   | 0.002077562 | 0.104    | 0.019976561        |
| 8X1    | 29110 | 28520  | 0.020267949 | 0.03766  | 0.538182399        |
| 9X1    | 65910 | 64490  | 0.02154453  | 0.07356  | 0.292883774        |
| 1X2    | 3585  | 3281   | 0.084797768 | 2.033    | 0.041710658        |
| 2X2    | 2369  | 2279   | 0.037990713 | 1.689    | 0.022493022        |
| 3X2    | 5190  | 4853   | 0.064932563 | 1.658    | 0.039163186        |
| 4X2    | 2089  | 2072   | 0.008137865 | 1.719    | 0.004734069        |
| 5X2    | 2249  | 2189   | 0.026678524 | 2.197    | 0.012143161        |
| 6X2    | 23830 | 23790  | 0.001678556 | 0.03955  | 0.042441377        |
| 7X2    | 2331  | 2317   | 0.006006006 | 0.005829 | 1.030366445        |
| 8X2    | 28480 | 28490  | -0.00035112 | 0.3381   | -0.00103852        |
| 9X2    | 64530 | 64530  | 0           | 0.285    | 0                  |
| 1X3    | 1972  | 1994   | -0.01115619 | 0.9062   | -0.012310954       |
| 2X3    | 1758  | 1792   | -0.01934016 | 1.178    | -0.016417792       |
| 3X3    | 3347  | 3338   | 0.002688975 | 0.8092   | 0.003323004        |
| 4X3    | 5E+06 | 5E+06  | 0           | 7680     | 0                  |
| 5X3    | 8E+05 | 810100 | 0           | 1302     | 0                  |
| 1X4    | 1665  | 1682   | -0.01021021 | 0.5812   | -0.017567464       |

| M&Hall | a     | b     | NSR         | c        | NSR/range    |
|--------|-------|-------|-------------|----------|--------------|
| 2X4    | 1432  | 1448  | -0.01117318 | 0.7296   | -0.015314123 |
| 3X4    | 3225  | 3215  | 0.003100775 | 0.482    | 0.006433144  |
| 4X4    | 2989  | 3009  | -0.0066912  | 3.079    | -0.002173173 |
| 5X4    | 5396  | 5403  | -0.00129726 | 6.326    | -0.000205068 |
| 1X5    | 925.2 | 916   | 0.009943796 | 0.6453   | 0.015409571  |
| 2X5    | 655.6 | 655.3 | 0.000457596 | 0.5558   | 0.000823311  |
| 3X5    | 2E+06 | 2E+06 | 0           | 1348     | 0            |
| 1X6    | 1087  | 1076  | 0.010119595 | 0.8031   | 0.012600666  |
| 2X6    | 862.4 | 865.5 | -0.00359462 | 0.4324   | -0.008313181 |
| 3X6    | 1529  | 1510  | 0.012426422 | 0.05845  | 0.212599187  |
| 1X7    | 1083  | 971.9 | 0.102585411 | 3.397    | 0.030198826  |
| 2X7    | 422.7 | 422.9 | -0.00047315 | 0.08611  | -0.005494702 |
| 1X8    | 819.8 | 771.4 | 0.05903879  | 1.815    | 0.032528259  |
| 2X8    | 437.9 | 443   | -0.01164649 | 0.004273 | -2.725601365 |
| 1X9    | 494.9 | 506.9 | -0.02424732 | 0.9047   | -0.026801506 |
| 2X9    | 382.7 | 382.7 | 0           | 0.07044  | 0            |

Table 6.3.5: Nugget to Sill ratios under Gaussian model.

| M&Hall | a     | b       | NSR         | c       | NSR/range    |
|--------|-------|---------|-------------|---------|--------------|
| 1X1    | 4647  | 3990    | 0.141381536 | 4.241   | 0.03333684   |
| 2X1    | 3586  | 3280    | 0.085331846 | 4.071   | 0.020960905  |
| 3X1    | 5626  | 5583    | 0.007643086 | 1.263   | 0.006051533  |
| 4X1    | 2740  | 2501    | 0.087226277 | 4.002   | 0.021795672  |
| 5X1    | 2618  | 2407    | 0.080595875 | 3.667   | 0.021978695  |
| 6X1    | 29050 | 28950   | 0.003442341 | 0.05731 | 0.060065273  |
| 7X1    | 2824  | 2651    | 0.061260623 | 0.1818  | 0.336967124  |
| 8X1    | 29500 | 29490   | 0.000338983 | 0.03955 | 0.008571     |
| 9X1    | 66790 | 66640   | 0.002245845 | 0.08566 | 0.026218132  |
| 1X2    | 3586  | 3280    | 0.085331846 | 4.07    | 0.020966056  |
| 2X2    | 2369  | 2280    | 0.037568594 | 3.382   | 0.011108396  |
| 3X2    | 5188  | 4852    | 0.064764842 | 3.31    | 0.019566418  |
| 4X2    | 2090  | 2072    | 0.00861244  | 3.442   | 0.002502162  |
| 5X2    | 2251  | 2190    | 0.027099067 | 4.4     | 0.006158879  |
| 6X2    | 25140 | 25500   | -0.01431981 | 0.0918  | -0.155989206 |
| 7X2    | 2361  | 2437    | -0.03218975 | 0.08253 | -0.390036958 |
| 8X2    | 28480 | 28490   | -0.00035112 | 0.6763  | -0.000519183 |
| 9X2    | 64530 | 64530   | 0           | 0.5699  | 0            |
| 1X3    | 1972  | 1994    | -0.01115619 | 1.812   | -0.006156836 |
| 2X3    | 1759  | 1792    | -0.01876066 | 2.366   | -0.007929273 |
| 3X3    | 3348  | 3340    | 0.002389486 | 1.621   | 0.001474082  |
| 4X3    | 5E+06 | 5367000 | 0           | 15360   | 0            |
| 5X3    | 8E+05 | 810100  | 0           | 2605    | 0            |
| 1X4    | 1665  | 1682    | -0.01021021 | 1.16    | -0.008801905 |
| 2X4    | 1433  | 1448    | -0.01046755 | 1.463   | -0.007154853 |
| 3X4    | 3235  | 3224    | 0.003400309 | 0.9864  | 0.003447191  |
| 4X4    | 2990  | 3009    | -0.00635452 | 6.158   | -0.001031912 |
| M&Hall | a     | b       | NSR         | c       | NSR/range    |

| M&Hall | a     | b       | NSR         | c       | NSR/range          |
|--------|-------|---------|-------------|---------|--------------------|
| 5X4    | 5396  | 5403    | -0.00129726 | 12.65   | -0.00010255        |
| 1X5    | 924.2 | 916.7   | 0.008115127 | 1.262   | 0.00643037         |
| 2X5    | 655.6 | 655.3   | 0.000457596 | 1.112   | 0.000411507        |
| 3X5    | 2E+06 | 1925000 | 0           | 2696    | 0                  |
| 1X6    | 1088  | 1075    | 0.011948529 | 1.627   | 0.007343903        |
| 2X6    | 864.1 | 866.7   | -0.00300891 | 0.8948  | -0.003362663       |
| 3X6    | 1561  | 1510    | 0.032671365 | 0.01356 | <b>2.409392663</b> |
| 1X7    | 1084  | 972.5   | 0.102859779 | 6.811   | 0.015102008        |
| 2X7    | 404.7 | 405.9   | -0.00296516 | 0.09755 | -0.030396303       |
| 1X8    | 819.7 | 771.4   | 0.058923997 | 3.628   | 0.016241454        |
| 2X8    | 470.5 | 481.4   | -0.02316684 | 0.1267  | -0.182848017       |
| 1X9    | 494.1 | 507.1   | -0.02631046 | 1.777   | -0.014806113       |
| 2X9    | 373.4 | 373.4   | 0           | 0.09996 | 0                  |

Table 6.3.6: Nugget to Sill ratios under Michaelis-menton model.

| M&Hall | a     | b     | NSR                | c        | NSR/range          |
|--------|-------|-------|--------------------|----------|--------------------|
| 1X1    | 5136  | 5019  | <b>0.022780374</b> | 1.156    | 0.019706206        |
| 2X1    | 4079  | 4034  | 0.011032116        | 1.323    | 0.008338712        |
| 3X1    | 5869  | 5865  | 0.000681547        | 0.2511   | 0.002714246        |
| 4X1    | 3158  | 3104  | 0.01709943         | 1.403    | 0.012187762        |
| 5X1    | 3009  | 2950  | 0.019607843        | 1.299    | 0.015094567        |
| 6X1    | 29160 | 29160 | 0                  | -0.01141 | 0                  |
| 7X1    | 2578  | 2577  | 0.000387898        | -0.2224  | -0.001744144       |
| 8X1    | 29610 | 29610 | 0                  | -0.00075 | 0                  |
| 9X1    | 67080 | 67080 | 0                  | -0.0027  | 0                  |
| 1X2    | 4080  | 4034  | 0.01127451         | 1.324    | 0.008515491        |
| 2X2    | 2919  | 2894  | 0.008564577        | 1.49     | 0.005748038        |
| 3X2    | 6269  | 6150  | 0.018982294        | 1.349    | 0.014071382        |
| 4X2    | 2763  | 2763  | 0                  | 1.86     | 0                  |
| 5X2    | 3026  | 3002  | 0.007931262        | 2.45     | 0.00323725         |
| 6X2    | 20520 | 20520 | 0                  | -0.2527  | 0                  |
| 7X2    | 1696  | 1716  | -0.01179245        | -0.4147  | <b>0.028436105</b> |
| 8X2    | 29050 | 29050 | 0                  | 0.06748  | 0                  |
| 9X2    | 66690 | 66680 | 0.000149948        | 0.07648  | 0.001960611        |
| 1X3    | 2107  | 2123  | -0.00759374        | 0.4308   | -0.017627055       |
| 2X3    | 2176  | 2197  | -0.00965074        | 1.085    | -0.008894687       |
| 3X3    | 3979  | 3977  | 0.000502639        | 0.6354   | 0.000791059        |
| 4X3    | 9E+06 | 9E+06 | 0                  | 13130    | 0                  |
| 5X3    | 2E+06 | 2E+06 | 0                  | 3018     | 0                  |
| 1X4    | 1692  | 1694  | -0.00118203        | 0.1195   | -0.00989149        |
| 2X4    | 1617  | 1623  | -0.00371058        | 0.4675   | -0.007937059       |
| 3X4    | 3681  | 3678  | 0.000814996        | 0.31     | 0.002629019        |
| 4X4    | 5420  | 5437  | -0.00313653        | 5.558    | -0.000564327       |
| 5X4    | 10200 | 10210 | -0.00098039        | 11.94    | -8.21099E-05       |
| 1X5    | 1010  | 1004  | 0.005940594        | 0.4176   | 0.01422556         |
| 2X5    | 716.7 | 716.8 | -0.00013953        | 0.2873   | -0.000485654       |
| M&Hall | a     | b     | NSR                | c        | NSR/range          |

| M&Hall | a     | b     | NSR         | c        | NSR/range    |
|--------|-------|-------|-------------|----------|--------------|
| 3X5    | 4E+06 | 4E+06 | 0           | 3126     | 0            |
| 1X6    | 1220  | 1215  | 0.004098361 | 0.5597   | 0.007322424  |
| 2X6    | 870.8 | 871.1 | -0.00034451 | 0.0655   | -0.005259707 |
| 3X6    | 1187  | 1185  | 0.00168492  | -0.3312  | -0.005087319 |
| 1X7    | 1245  | 1203  | 0.03373494  | 2.39     | 0.014115038  |
| 2X7    | 390.1 | 390.3 | -0.00051269 | -0.1657  | 0.00309408   |
| 1X8    | 975.6 | 959.1 | 0.016912669 | 1.449    | 0.011671959  |
| 2X8    | 367.8 | 369.4 | -0.00435019 | -0.3002  | 0.014490974  |
| 1X9    | 534.2 | 539.6 | -0.01010857 | 0.4878   | -0.020722783 |
| 2X9    | 371.3 | 371.3 | 0           | -0.05098 | 0            |

Table 6.3.7: Nugget to Sill ratios under VB model.

| M&HALL | VB       | K       | t0         | nugget   | NSR         | NSR/range    |
|--------|----------|---------|------------|----------|-------------|--------------|
| plot   | sill(Li) |         |            |          |             |              |
| 1X1    | 4646     | 0.473   | -0.3192    | 651.0741 | 0.14013648  | 0.296271628  |
| 2X1    | 3586     | 0.4915  | -0.1807    | 304.7537 | 0.084984295 | 0.172908027  |
| 3X1    | 5626     | 1.58    | -0.004993  | 44.20857 | 0.007857904 | 0.004973357  |
| 4X1    | 2742     | 0.4975  | -0.1862    | 242.5941 | 0.088473398 | 0.177835975  |
| 5X1    | 2617     | 0.5467  | -0.1522    | 208.9413 | 0.079840027 | 0.146039924  |
| 6X1    | 29260    | 12.24   | 0.0002228  | -79.903  | -0.00273079 | -0.000223104 |
| 7X1    | 2770     | 12.74   | 0.0006481  | -22.966  | -0.00829098 | -0.000650783 |
| 8X1    | 29620    | 17.42   | 0.0001094  | -56.5021 | -0.00190757 | -0.000109504 |
| 9X1    | 67140    | 18.91   | 0.00006441 | -81.8259 | -0.00121874 | -6.44492E-05 |
| 1X2    | 3585     | 0.4924  | -0.1789    | 302.2939 | 0.084321868 | 0.171246685  |
| 2X2    | 2370     | 0.5907  | -0.06583   | 90.39046 | 0.038139434 | 0.064566505  |
| 3X2    | 5191     | 0.6028  | -0.1115    | 337.4317 | 0.065003226 | 0.107835478  |
| 4X2    | 2090     | 0.5811  | -0.0149    | 18.01792 | 0.008621014 | 0.014835681  |
| 5X2    | 2250     | 0.4546  | -0.05967   | 60.2131  | 0.026761377 | 0.058867965  |
| 6X2    | 24450    | 28.51   | 0.00001444 | -10.0678 | -0.00041177 | -1.4443E-05  |
| 7X2    | 2224     | 9.869   | -0.0002238 | 4.906689 | 0.002206245 | 0.000223553  |
| 8X2    | 28480    | 2.957   | 0.00001332 | -1.12177 | -3.9388E-05 | -1.33203E-05 |
| 9X2    | 64530    | 3.51    | -9.968E-06 | 2.257715 | 3.49871E-05 | 9.96783E-06  |
| 1X3    | 1972     | 1.104   | 0.01043    | -22.8383 | -0.01158127 | -0.01049028  |
| 2X3    | 1759     | 0.8439  | 0.02192    | -32.8413 | -0.01867044 | -0.022123997 |
| 3X3    | 3348     | 1.234   | -0.002086  | 8.607085 | 0.002570814 | 0.002083317  |
| 4X3    | 26750    | 0.02672 | 0.09494    | -67.9455 | -0.00254002 | -0.095060524 |
| 5X3    | 29850    | 0.02146 | 0.02236    | -14.3268 | -0.00047996 | -0.022365366 |
| 1X4    | 1666     | 1.695   | 0.005441   | -15.4357 | -0.00926515 | -0.005466167 |
| 2X4    | 1433     | 1.364   | 0.007807   | -15.3412 | -0.01070565 | -0.007848715 |
| 3X4    | 3235     | 2.031   | -0.001727  | 11.32701 | 0.003501393 | 0.001723975  |
| 4X4    | 2990     | 0.3248  | 0.01957    | -19.066  | -0.00637658 | -0.019632329 |
| 5X4    | 5402     | 0.1579  | 0.008253   | -7.0442  | -0.001304   | -0.00825838  |
| 1X5    | 925.1    | 1.554   | -0.006247  | 8.93727  | 0.009660869 | 0.006216775  |
| 2X5    | 655.6    | 1.799   | -0.0002148 | 0.253291 | 0.000386351 | 0.000214759  |
| 3X5    | 73800    | 0.01965 | 0.06277    | -91.0833 | -0.00123419 | -0.062808727 |
| 1X6    | 1088     | 1.233   | -0.009343  | 12.46175 | 0.011453819 | 0.009289391  |
| M&HALL | VB       |         |            |          |             |              |

| M&HALL | VB       |        |            |          |             |                    |
|--------|----------|--------|------------|----------|-------------|--------------------|
| plot   | sill(Li) | K      | t0         | nugget   | NSR         | NSR/range          |
| 2X6    | 863.6    | 2.251  | 0.001388   | -2.70244 | -0.00312927 | -0.001390171       |
| 3X6    | 1581     | 37.58  | 0.00005162 | -3.06993 | -0.00194176 | -5.16701E-05       |
| 1X7    | 1086     | 0.2919 | -0.3718    | 111.6914 | 0.102846603 | <b>0.352335055</b> |
| 2X7    | 434.9    | 88.74  | 0.00001443 | -0.55725 | -0.00128134 | -1.44392E-05       |
| 1X8    | 820.6    | 0.5478 | -0.1126    | 49.08702 | 0.059818446 | 0.109197602        |
| 2X8    | 454      | 22.14  | 0.00004002 | -0.40244 | -0.00088644 | -4.00377E-05       |
| 1X9    | 494.8    | 1.106  | 0.02183    | -12.0918 | -0.02443781 | -0.022095665       |
| 2X9    | 383.2    | 80.11  | 4.591E-06  | -0.14096 | -0.00036785 | -4.59184E-06       |

The following tables present the maximum curvature values for different plot sizes and shapes and also for different models.

TABLE 6.3.8:

| M&H  | SPHERICAL |       |          |          |          |           |                   |
|------|-----------|-------|----------|----------|----------|-----------|-------------------|
| plot | b         | c     | h        | y1       | y2       | curvature |                   |
| 1X1  | 2443      | 10.85 | 21987.05 | 26506.57 | -2E+09   | -152093   | -5.385E+22        |
| 2X1  | 2195      | 9.259 | 19755.04 | 20323.52 | -1.7E+09 | -168602   | -2.983E+22        |
| 3X1  | 2223      | 13.22 | 20007.09 | 29388.1  | -1.2E+09 | -84827.7  | -2.283E+22        |
| 4X1  | 1843      | 9.662 | 16587.06 | 17807.08 | -9.7E+08 | -109154   | -8.409E+21        |
| 5X1  | 1727      | 10.62 | 15543.07 | 18340.77 | -7.3E+08 | -79333.7  | -4.854E+21        |
| 6X1  | 18960     | 6.874 | 170640   | 130331   | -1.5E+12 | -2.3E+07  | -1.441E+29        |
| 7X1  | 1342      | 6.932 | 12078.04 | 9302.753 | -5.2E+08 | -112437   | -1.272E+21        |
| 8X1  | 20220     | 6.993 | 181980   | 141398.5 | -1.8E+12 | -2.5E+07  | -2.223E+29        |
| 9X1  | 44130     | 7.125 | 397170   | 314426.3 | -1.8E+13 | -1.2E+08  | -5.146E+31        |
| 1X2  | 2194      | 9.259 | 19746.04 | 20314.26 | -1.7E+09 | -168448   | -2.973E+22        |
| 2X2  | 1871      | 5.092 | 16839.02 | 9527.135 | -1.9E+09 | -405035   | -1.773E+22        |
| 3X2  | 4071      | 5.401 | 36639.01 | 21987.47 | -1.9E+10 | -1704414  | -3.86E+24         |
| 4X2  | 1758      | 4.916 | 15822.02 | 8642.331 | -1.7E+09 | -383650   | -1.188E+22        |
| 5X2  | 1850      | 5.512 | 16650.02 | 10197.2  | -1.7E+09 | -337945   | -1.514E+22        |
| 6X2  | 26300     | 2.107 | 236700   | 55414.1  | -1.3E+13 | -4.7E+08  | -4.647E+30        |
| 7X2  | 1718      | 2.591 | 15462    | 4451.338 | -2.9E+09 | -1318964  | -1.918E+22        |
| 8X2  | 34200     | 2.85  | 307800   | 97470    | -2.1E+13 | -4.3E+08  | -2.16E+31         |
| 9X2  | 75360     | 2.92  | 678240   | 220051.2 | -2.2E+14 | -2E+09    | -5.318E+33        |
| 1X3  | 1210      | 6.348 | 10890.04 | 7681.088 | -4.2E+08 | -108998   | -6.73E+20         |
| 2X3  | 1757      | 3.332 | 15813.01 | 5854.325 | -2.4E+09 | -834171   | -1.745E+22        |
| 3X3  | 3225      | 2.536 | 29025    | 8178.6   | -2E+10   | -4851569  | -1.61E+24         |
| 4X3  | 906300    | 1947  | 8156705  | 1.76E+09 | -5.7E+14 | -650030   | <b>-2.902E+38</b> |
| 5X3  | 559600    | 1351  | 5036404  | 7.56E+08 | -1.9E+14 | -514714   | -1.431E+37        |
| 1X4  | 821.3     | 5.904 | 7391.747 | 4848.964 | -1.4E+08 | -58054.1  | -4.803E+19        |
| 2X4  | 1383      | 3.011 | 12447.01 | 4164.214 | -1.3E+09 | -632913   | -3.616E+21        |
| 3X4  | 3193      | 2.02  | 28737    | 6449.86  | -2.4E+10 | -7495772  | -1.884E+24        |
| 4X4  | 1499      | 2.462 | 13491    | 3690.538 | -2.1E+09 | -1112112  | -7.771E+21        |
| 5X4  | 1931      | 3.544 | 17379.01 | 6843.465 | -3E+09   | -890632   | -3.178E+22        |
| 1X5  | 558.9     | 7.787 | 5030.221 | 4352.186 | -3.4E+07 | -15454.4  | -2.461E+18        |
| 2X5  | 615.6     | 2.972 | 5540.416 | 1829.565 | -1.2E+08 | -128713   | -1.268E+19        |
| 3X5  | 401100    | 421.6 | 3609900  | 1.69E+08 | -2.3E+14 | -2715347  | -4.457E+36        |
| 1X6  | 748.9     | 7.802 | 6740.19  | 5842.941 | -8.1E+07 | -27641.3  | -1.905E+19        |
| 2X6  | 882.9     | 2.64  | 7946.109 | 2330.857 | -3.9E+08 | -335534   | -1.782E+20        |
| 3X6  | 1675      | 1.523 | 15075    | 2551.025 | -4.6E+09 | -3628700  | -2.732E+22        |
| 1X7  | 1272      | 16.46 | 11448.24 | 20937.25 | -1.9E+08 | -17915.9  | -3.683E+20        |

M&H SPHERICAL

M&H SPHERICAL

| plot | b     | c     |          | h        | y1       | y2       | curvature  |
|------|-------|-------|----------|----------|----------|----------|------------|
| 1X8  | 801   | 11.29 | 7209.177 | 9043.357 | -6.8E+07 | -15100.9 | -2.108E+19 |
| 2X8  | 610.3 | 1.905 | 5492.707 | 1162.622 | -1.8E+08 | -307906  | -1.862E+19 |
| 1X9  | 436.5 | 5.297 | 3928.571 | 2312.153 | -2.4E+07 | -20371.9 | -6.412E+17 |
| 2X9  | 439.9 | 2.128 | 3959.111 | 936.108  | -6E+07   | -128199  | -1.685E+18 |

TABLE 6.3.9

M&H EXPONENTIAL

| plot | b      | c        |          | h        | y1       | y2       | curvature |
|------|--------|----------|----------|----------|----------|----------|-----------|
| 1X1  | 3992   | 2.118    | 2665.505 | 16.7071  | 0.707107 | -0.33386 | -5.50273  |
| 2X1  | 3280   | 2.036    | 2278.301 | 15.74069 | 0.707107 | -0.3473  | -5.28968  |
| 3X1  | 5584   | 0.6303   | 12528.9  | 5.947381 | 0.707107 | -1.12186 | -1.63757  |
| 4X1  | 2500   | 2.006    | 1762.48  | 14.9938  | 0.707107 | -0.3525  | -5.21174  |
| 5X1  | 2408   | 1.831    | 1859.872 | 13.78425 | 0.707107 | -0.38619 | -4.75708  |
| 6X1  | 23390  | 0.02087  | 1584976  | 0.297942 | 0.707107 | -33.8815 | -0.05422  |
| 7X1  | 2882   | 0.104    | 39190.03 | 1.099922 | 0.707107 | -6.7991  | -0.2702   |
| 8X1  | 28520  | 0.03766  | 1070987  | 0.522875 | 0.707107 | -18.7761 | -0.09784  |
| 9X1  | 64490  | 0.07356  | 1239840  | 1.032083 | 0.707107 | -9.61265 | -0.19111  |
| 1X2  | 3281   | 2.033    | 2282.358 | 15.72112 | 0.707107 | -0.34781 | -5.28189  |
| 2X2  | 2279   | 1.689    | 1908.225 | 12.75859 | 0.707107 | -0.41865 | -4.38815  |
| 3X2  | 4853   | 1.658    | 4139.432 | 13.80834 | 0.707107 | -0.42648 | -4.30761  |
| 4X2  | 2072   | 1.719    | 1704.625 | 12.79125 | 0.707107 | -0.41135 | -4.46609  |
| 5X2  | 2189   | 2.197    | 1409.064 | 15.92975 | 0.707107 | -0.32185 | -5.70797  |
| 6X2  | 23790  | 0.03955  | 850673.6 | 0.540007 | 0.707107 | -17.8788 | -0.10275  |
| 7X2  | 2317   | 0.005829 | 562143.2 | 0.077173 | 0.707107 | -121.308 | -0.01514  |
| 8X2  | 28490  | 0.3381   | 119168.7 | 3.951813 | 0.707107 | -2.09141 | -0.87841  |
| 9X2  | 64530  | 0.285    | 320207.7 | 3.612867 | 0.707107 | -2.48108 | -0.74045  |
| 1X3  | 1994   | 0.9062   | 3111.832 | 7.288537 | 0.707107 | -0.7803  | -2.35438  |
| 2X3  | 1792   | 1.178    | 2151.333 | 9.039787 | 0.707107 | -0.60026 | -3.06053  |
| 3X3  | 3338   | 0.8092   | 5833.718 | 7.016905 | 0.707107 | -0.87383 | -2.10236  |
| 4X3  | 5E+06  | 7680     | 988.1081 | 52959.68 | 0.707107 | -9.2E-05 | -19953.2  |
| 5X3  | 810100 | 1302     | 879.9189 | 8827.338 | 0.707107 | -0.00054 | -3382.7   |
| 1X4  | 1682   | 0.5812   | 4092.752 | 4.833825 | 0.707107 | -1.21663 | -1.51     |
| 2X4  | 1448   | 0.7296   | 2806.718 | 5.792857 | 0.707107 | -0.96917 | -1.89556  |
| 3X4  | 3215   | 0.482    | 9432.981 | 4.411248 | 0.707107 | -1.46703 | -1.25227  |
| 4X4  | 3009   | 3.079    | 1382.062 | 22.26527 | 0.707107 | -0.22965 | -7.99948  |
| 5X4  | 5403   | 6.326    | 1207.872 | 44.89319 | 0.707107 | -0.11178 | -16.4354  |
| 1X5  | 916    | 0.6453   | 2007.469 | 4.907268 | 0.707107 | -1.09578 | -1.67654  |
| 2X5  | 655.3  | 0.5558   | 1667.388 | 4.123488 | 0.707107 | -1.27223 | -1.44401  |
| 3X5  | 2E+06  | 1348     | 2019.556 | 10259.13 | 0.707107 | -0.00052 | -3502.21  |
| 1X6  | 1076   | 0.8031   | 1894.775 | 6.06088  | 0.707107 | -0.88047 | -2.08652  |
| 2X6  | 865.5  | 0.4324   | 2830.717 | 3.436839 | 0.707107 | -1.63531 | -1.12341  |
| 3X6  | 1510   | 0.05845  | 36534.86 | 0.614077 | 0.707107 | -12.0976 | -0.15186  |
| 1X7  | 971.9  | 3.397    | 404.6141 | 20.39197 | 0.707107 | -0.20816 | -8.82566  |
| 2X7  | 422.9  | 0.08611  | 6945.429 | 0.761715 | 0.707107 | -8.21167 | -0.22372  |
| 1X8  | 771.4  | 1.815    | 601.0602 | 11.61363 | 0.707107 | -0.38959 | -4.71551  |
| 2X8  | 443    | 0.004273 | 146617.5 | 0.05083  | 0.707107 | -165.482 | -0.0111   |
| 1X9  | 506.9  | 0.9047   | 792.3785 | 6.038908 | 0.707107 | -0.78159 | -2.35048  |

2X9 382.7 0.07044 7683.412 0.630214 0.707107 -10.0384 -0.18301

TABLE 6.3.10

| M&H  | Michaelis-menton |          |          |       |          |                   |
|------|------------------|----------|----------|-------|----------|-------------------|
| plot | b                | c        | h+ve     | y1    | y2       | curvature         |
| 1X1  | 5019             | 1.156    | 75.01462 | 1     | -0.02626 | -107.72153        |
| 2X1  | 4034             | 1.323    | 71.73165 | 1     | -0.02738 | -103.31488        |
| 3X1  | 5865             | 0.2511   | 38.12469 | 1     | -0.05212 | -54.271567        |
| 4X1  | 3104             | 1.403    | 64.58876 | 1     | -0.03031 | -93.326438        |
| 5X1  | 2950             | 1.299    | 60.60455 | 1     | -0.03231 | -87.544846        |
| 6X1  | 29160            | -0.01141 | _____    | _____ | _____    | _____             |
| 7X1  | 2577             | -0.2224  | _____    | _____ | _____    | _____             |
| 8X1  | 29610            | -0.00075 | _____    | _____ | _____    | _____             |
| 9X1  | 67080            | -0.0027  | _____    | _____ | _____    | _____             |
| 1X2  | 4034             | 1.324    | 71.75826 | 1     | -0.02737 | -103.35392        |
| 2X2  | 2894             | 1.49     | 64.17628 | 1     | -0.03046 | -92.86614         |
| 3X2  | 6150             | 1.349    | 89.7353  | 1     | -0.02196 | -128.81265        |
| 4X2  | 2763             | 1.86     | 69.82807 | 1     | -0.0279  | -101.38225        |
| 5X2  | 3002             | 2.45     | 83.31071 | 1     | -0.02332 | -121.28396        |
| 6X2  | 20520            | -0.2527  | _____    | _____ | _____    | _____             |
| 7X2  | 1716             | -0.4147  | _____    | _____ | _____    | _____             |
| 8X2  | 29050            | 0.06748  | 44.20773 | 1     | -0.04517 | -62.614599        |
| 9X2  | 66680            | 0.07648  | 71.33561 | 1     | -0.02801 | -100.99194        |
| 1X3  | 2123             | 0.4308   | 29.81136 | 1     | -0.06613 | -42.768877        |
| 2X3  | 2197             | 1.085    | 47.73861 | 1     | -0.04096 | -69.047013        |
| 3X3  | 3977             | 0.6354   | 49.63373 | 1     | -0.03979 | -71.091291        |
| 4X3  | 9177000          | 13130    | 333992.5 | 1     | -5.8E-06 | <b>-490905.31</b> |
| 5X3  | 1877000          | 3018     | 72246.77 | 1     | -2.7E-05 | -106440.46        |
| 1X4  | 1694             | 0.1195   | 14.1084  | 1     | -0.14057 | -20.121282        |
| 2X4  | 1623             | 0.4675   | 27.07796 | 1     | -0.07261 | -38.955167        |
| 3X4  | 3678             | 0.31     | 33.45655 | 1     | -0.05923 | -47.753115        |
| 4X4  | 5437             | 5.558    | 168.2777 | 1     | -0.01151 | -245.84079        |
| 5X4  | 10210            | 11.94    | 337.2124 | 1     | -0.00573 | -493.77606        |
| 1X5  | 1004             | 0.4176   | 20.05849 | 1     | -0.09767 | -28.957569        |
| 2X5  | 716.8            | 0.2873   | 14.06319 | 1     | -0.13937 | -20.294661        |
| 3X5  | 4465000          | 3126     | 115016.2 | 1     | -1.7E-05 | -167078.36        |
| 1X6  | 1215             | 0.5597   | 25.51779 | 1     | -0.07669 | -36.87914         |
| 2X6  | 871.1            | 0.0655   | 7.488112 | 1     | -0.26477 | -10.68242         |
| 3X6  | 1185             | -0.3312  | _____    | _____ | _____    | _____             |
| 1X7  | 1203             | 2.39     | 51.23061 | 1     | -0.0373  | -75.830996        |
| 2X7  | 390.3            | -0.1657  | _____    | _____ | _____    | _____             |
| 1X8  | 959.1            | 1.449    | 35.83016 | 1     | -0.05365 | -52.720696        |
| 2X8  | 369.4            | -0.3002  | _____    | _____ | _____    | _____             |
| 1X9  | 539.6            | 0.4878   | 15.73616 | 1     | -0.12327 | -22.944144        |
| 2X9  | 371.3            | -0.05098 | _____    | _____ | _____    | _____             |

TABLE 6.3.11

| M&H plot | VB model Li | K       | t0         | h        | y1       | y2       | curvature |
|----------|-------------|---------|------------|----------|----------|----------|-----------|
| 1X1      | 4646        | 0.473   | -0.3192    | 16.68223 | 0.707107 | -0.33446 | -5.492762 |
| 2X1      | 3586        | 0.4915  | -0.1807    | 15.73196 | 0.707107 | -0.34754 | -5.286015 |
| 3X1      | 5626        | 1.58    | -0.004993  | 5.969154 | 0.707107 | -1.11723 | -1.644352 |
| 4X1      | 2742        | 0.4975  | -0.1862    | 15.01954 | 0.707107 | -0.35179 | -5.222264 |
| 5X1      | 2617        | 0.5467  | -0.1522    | 13.77226 | 0.707107 | -0.38658 | -4.752289 |
| 6X1      | 29260       | 12.24   | 0.0002228  | 1.073365 | 0.707107 | -8.65499 | -0.212261 |
| 7X1      | 2770        | 12.74   | 0.0006481  | 0.849779 | 0.707107 | -9.00854 | -0.203931 |
| 8X1      | 29620       | 17.42   | 0.0001094  | 0.775104 | 0.707107 | -12.3178 | -0.149143 |
| 9X1      | 67140       | 18.91   | 0.00006441 | 0.761609 | 0.707107 | -13.3714 | -0.137392 |
| 1X2      | 3585        | 0.4924  | -0.1789    | 15.70783 | 0.707107 | -0.34818 | -5.276353 |
| 2X2      | 2370        | 0.5907  | -0.06583   | 12.78464 | 0.707107 | -0.41769 | -4.398301 |
| 3X2      | 5191        | 0.6028  | -0.1115    | 13.81532 | 0.707107 | -0.42624 | -4.310014 |
| 4X2      | 2090        | 0.5811  | -0.0149    | 12.80331 | 0.707107 | -0.4109  | -4.470962 |
| 5X2      | 2250        | 0.4546  | -0.05967   | 15.94764 | 0.707107 | -0.32145 | -5.715082 |
| 6X2      | 24450       | 28.51   | 0.00001444 | 0.484098 | 0.707107 | -20.1596 | -0.091129 |
| 7X2      | 2224        | 9.869   | -0.0002238 | 1.047809 | 0.707107 | -6.97844 | -0.263256 |
| 8X2      | 28480       | 2.957   | 0.00001332 | 3.952569 | 0.707107 | -2.09091 | -0.878619 |
| 9X2      | 64530       | 3.51    | -9.968E-06 | 3.611692 | 0.707107 | -2.48194 | -0.740193 |
| 1X3      | 1972        | 1.104   | 0.01043    | 7.28608  | 0.707107 | -0.78065 | -2.35333  |
| 2X3      | 1759        | 0.8439  | 0.02192    | 9.086209 | 0.707107 | -0.59673 | -3.078654 |
| 3X3      | 3348        | 1.234   | -0.002086  | 7.026239 | 0.707107 | -0.87257 | -2.10541  |
| 4X3      | 26750       | 0.02672 | 0.09494    | 259.0216 | 0.707107 | -0.01889 | -97.23339 |
| 5X3      | 29850       | 0.02146 | 0.02236    | 317.308  | 0.707107 | -0.01517 | -121.066  |
| 1X4      | 1666        | 1.695   | 0.005441   | 4.897734 | 0.707107 | -1.19855 | -1.532788 |
| 2X4      | 1433        | 1.364   | 0.007807   | 5.817573 | 0.707107 | -0.96449 | -1.904748 |
| 3X4      | 3235        | 2.031   | -0.001727  | 4.496986 | 0.707107 | -1.43613 | -1.27921  |
| 4X4      | 2990        | 0.3248  | 0.01957    | 22.2642  | 0.707107 | -0.22967 | -7.999003 |
| 5X4      | 5402        | 0.1579  | 0.008253   | 44.94369 | 0.707107 | -0.11165 | -16.45393 |
| 1X5      | 925.1       | 1.554   | -0.006247  | 4.895495 | 0.707107 | -1.09884 | -1.671864 |
| 2X5      | 655.6       | 1.799   | -0.0002148 | 4.123941 | 0.707107 | -1.27209 | -1.444178 |
| 3X5      | 73800       | 0.01965 | 0.06277    | 388.1549 | 0.707107 | -0.01389 | -132.2176 |
| 1X6      | 1088        | 1.233   | -0.009343  | 6.112409 | 0.707107 | -0.87186 | -2.107118 |
| 2X6      | 863.6       | 2.251   | 0.001388   | 3.519406 | 0.707107 | -1.5917  | -1.154188 |
| 3X6      | 1581        | 37.58   | 0.00005162 | 0.301777 | 0.707107 | -26.5731 | -0.069135 |
| 1X7      | 1086        | 0.2919  | -0.3718    | 20.54456 | 0.707107 | -0.2064  | -8.900569 |
| 2X7      | 434.9       | 88.74   | 0.00001443 | 0.122929 | 0.707107 | -62.7486 | -0.029277 |
| 1X8      | 820.6       | 0.5478  | -0.1126    | 11.67047 | 0.707107 | -0.38735 | -4.742746 |
| 2X8      | 454         | 22.14   | 0.00004002 | 0.431931 | 0.707107 | -15.6553 | -0.117348 |
| 1X9      | 494.8       | 1.106   | 0.02183    | 6.035824 | 0.707107 | -0.78206 | -2.349074 |
| 2X9      | 383.2       | 80.11   | 4.591E-06  | 0.133303 | 0.707107 | -56.6463 | -0.032431 |
| 8X1      | 745.6       | 2.748   | 0.001286   | 2.902173 | 0.707107 | -1.94313 | -0.945443 |
| 9X1      | 7767        | 15.74   | 4.832E-06  | 0.766232 | 0.707107 | -11.1299 | -0.165062 |

Thus using the three criteria i.e. Nugget to sill ratio (NSR), NSR/Range, maximum curvature value of the variogram models we have found optimum plot size and shapes (i.e. number of units

to be taken along row and column directions) for Mercer and Hall wheat grain yield data. These are summarized in the following table:

TABLE 6.3.12: Plot sizes found using the method of NSR and curvature.

| Model            | NSR   | NSR/Range | Curvature |
|------------------|-------|-----------|-----------|
| Michaelis-menton | 1 X 1 | 7 X 2     | 4 X 3     |
| Gaussian         | 1 X 1 | 3 X 6     | -----     |
| VB               | 1 X 1 | 1 X 7     | 4 X 3     |
| Exponential      | 1 X 1 | 6 X 1     | 4 X 3     |
| Spherical        | 3 X 1 | 7 X 2     | 3 X 5     |

## Chapter 7

### SUMMARY AND CONCLUSION

The study reveals the existence of structural heterogeneity due to which the observations vary among themselves even if other factors are controlled so that they do not cause any variability in the observations. The presence of structured heterogeneity of soil induces error in the treatment comparisons. It is known that the classical experimental design is based on the three concepts of randomization, replication and local control. Randomisation endeavors to neutralize the effects of spatial correlation and yields valid tests for the hypothesis of equal treatment effects. Here we have tried to identify and estimate the covariance and spatial correlation structure. If the correlation is present the analysis based on appropriate correlation structure is more efficient than one based on independence. The works on spatial modeling proves the need of obtaining the *a priori* information on structured heterogeneity of soil before conducting the field experiment and, also, it emphasizes the need of obtaining *a posteriori* information before analysis of the field experiment observations for inferring on the treatment comparisons more precisely. Again the distribution of several soil properties may be spatially structured. It indicates that not only on the basis of plot yield but also on the basis of soil properties heterogeneity structure and thereby the optimum plot size and shape can be studied more precisely. Hence there is further scope of studying the nature of spatial dependence on the basis of various soil properties viz. soil P<sup>H</sup>, amount of macro and micro nutrients present in the soil, which ultimately play an important role in determining the crop yield from each plot.

The Smith's (1938) method of determining optimum plot size is based on minimizing the cost per unit of information. Following the method cost aspect has been given importance along with the average estimate of heterogeneity of the field as another determining criteria. The value of  $X_{opt} =$

$\frac{b.k_1}{(1-b).k_2}$  indicates that as the heterogeneity of the field increases, optimum plot size also

increases. Again with the increase in the fixed cost ( $k_1$ ) (in proportion to the variable cost ( $k_2$ )) the optimum plot size also increases accordingly. However, if the data related to the cost aspect are not available and there exist a random fertility structure in the field, still we can search for optimum plot size by observing the graph of C.V. vs. plot size using the general equation of  $y = a.x^{-b}$ . Here C.V. values are used to compare the nature of relative variation in two or more different types of situations. Optimum plot size is found by maximizing the radius of curvature

i.e. the point when there is no further appreciable decrease in C.V. value with the increase in plot size. But the associated cost for experimentation goes up with the increase in plot size. Hence it can be said that if an experimenter primarily faces with the cost constraint Smith's optimum plot size can take care of his problem. Otherwise, it is better to go for other methods (described as above and also as below) in order to determine optimum plot size. However if there are bidirectional heterogeneity operating in the field the above mentioned general equation is modified as  $y = a' x_1^{-b_1} x_2^{-b_2}$ . The bidirectional fertility coefficients namely,  $b_1$  and  $b_2$  are then found by using least squares technique and finally optimum plot dimensions have been determined. Optimum block size has been studied by searching for minimum value of within block C.V. and highest blocking efficiency individually when blocks run along row and column directions. Thus we can also find the optimum plot and block dimensions. In the foregoing discussion the assumption of independence of the plot observations holds true. But as mentioned earlier that observations from field plots are often found to be spatially correlated. If the analysis of field plot observations show presence of spatial dependence the above mentioned methods become limited in terms of their validity. Here determination of optimum plot size by using the spatial correlation structure appears to be a better choice. It is well known that spatial dependence can be studied using the variogram analysis based on plot observations. Here optimum plot size and shape is determined by using the criteria of independence of the observations. Using the estimated values (obtained by using nonlinear estimation) of the variogram parameters, the nugget/sill ratio (NSR) is used as a criterion indicating the extent to which the experimental errors between plots were randomly distributed in space. The smaller the NSR, the less the plot configuration meets the condition that experimental errors can be considered to be random. So the largest NSR represents the configuration which best meets the underlying hypothesis of classical ANOVA techniques. We have also given a new approach to determine optimum plot size whereby we find the point  $h_{opt}$ . The plot size which shows maximum radius of curvature at  $h_{opt}$  is the optimum one.

## BIBLIOGRAPHY

1. Abraham, T.P. and Vachhani, M.V. (1964). "Investigations on Field Experimental Techniques with Rice Crops, I. Size and Shape of Plots and Blocks in Field Experiments with Transplanted Rice Crop". *Indian Jour. Of Agri. Sci.*
2. Abramowitz, M. and Stegun, I.A. (1964). *Handbook of Mathematical Functions*: Dover, New York, 1046p.
3. Batchelor, L.D., and Reed, H.S. (1918). "Relation of the Variability of Fruit Trees to the Accuracy of Field Trials." *Jour. Of Agri. Res.* XII, no.5, 245-283.
4. Bhatti, A.U., Mulla, D.J., Koehler, F.E., and Gurmani, A.H. (1991). "Identifying and removing spatial correlation from yield experiments." *Soil Sci. Soc. Am. J.*, 55, November-December, 1523-1528.
5. Carleton, M.A. (1909) "Limitations in Field Experiments." *Proc. 30-th Ann. Meeting Soc. Prom. Agr. Sci.*, 55-61.
6. Clark, I. (1976). "Some Practical Computational Aspects of Mine Planning, in *Advanced Geostatistics in the Mining Industry*", Eds.: M. Guarascio, M. David, and C. Huijbregts, Reidel, Dordrecht, 461p.
7. Coombs, G.E., and Grantham, J. (1916). "Field Experiments and the Interpretation of Their Results." *Agr. Bul. Fed. Malay States*, 4, no.7, 206-216, 1 fig.
8. Cressie, N.A.C. (1993). *Statistics for Spatial Data*. John Wiley & Sons, Inc.
9. David, M. (1976). "The Practice of Kriging, in *Advanced Geostatistics in the Mining Industry*", Eds.: M. Guarascio, M. David, and C. Huijbregts, Reidel, Dordrecht, 461p.
10. Davis, Michael W.D. and David, Michael. (1978). "The Numerical Calculation of Integrals of an Isotropic Variogram Function on Hypercubes" *Math. Geol.*, 10, No. 3, 311-314.
11. Emerson, J.D. and Hoaglin, D.C.(1983). "Analysis of Two Way Tables by Medians. In *Understanding Robust and Exploratory Data Analysis*, D.C.Hoaglin, F. Mosteller, and J.W. Tukey, eds. Wiley, New York, 166-210.
12. Ersboll, A.K. (1996). "Spatial experimental design." p. 112-125. In J.M.C. Ocerin *et al.*(ed.) III HaRMA meeting; Cordoba: Design of experiments and statistical education in agriculture. European Community, Brussels.

13. Federer, W. T. (1955). *Experimental Design*. Macmillan, New York.
14. Fagroud, M. and Meirvenne, M. Van (2002). "Accounting for Soil Spatial Autocorrelation in the Design of Experimental Trials." *Soil Sci. Soc. Am. J.*, **66**, July-August, 1134-1142.
15. Goovaerts, P. (1998). "Geostatistical tools for characterizing the spatial variability of microbiological and physiochemical soil properties." *Biol. Fertil. Soils*. **27**, 615-634.
16. Grondona, M.O. and Cressie, N. (1991). "Using Spatial Considerations in the Analysis of Experiments." *Technometrics* **33**, no. 4, 381-392.
17. Hall, A.D. (1909) "The Experimental Error in Field Trials." *Jour. Bd. Agr. [London]*, **16**, no.5, 365-370.
18. Hall, A.D. and Russel, E.J. (1911) "Field Trials and Their Interpretation." *Jour. Bd. Agr. [London]*, Sup. 7, 5-14, 2 fig.
19. Harris, J.A. (1912) "On the Significance of Variety Tests." *Science*, n.s., **36**, no.923, 318-320.
20. Harris, J.A. (1913a) "An Illustration of the Influence of Substratum Heterogeneity upon Experimental Results." *Science*, n.s., **38**, no.975, 345-346.
21. Harris, J.A. (1913b) "Supplementary Note on the Significance of Variety Tests." *Science*, n.s., **37**, no.952, 493-494.
22. Harris, J.A. (1915). "On a Criterion of Substratum Homogeneity (or Heterogeneity) in Field Experiments." *Amer. Nat.* **49**, 430-454.
23. Holtsmark, G., and Larsen, B.R. (1906) "UBER DIE FEHLER, WELCHE BEI FELDVERSUCHEN DURCH DIE UNGLEICHARTIG KEIT DES BODENS BEDINGT WERDEN." *Landw. Vers. Stat.*, Bd. 65, Heft ½, 1-22.
24. Journel, A.G. and Huijbregts, C.J. (1978). *Mining Geostatistics*. Academic Press, London.
25. Krylov, V.I. (1962). *Approximate Calculation of Integrals*. Macmillan, New York, 357p.
26. Lyon, T.L. (1912) "Some Experiments to Estimate Errors in Field Plot Tests." *Proc. Amer. Soc. Agron.*, **3**, 1911, 89-114, 5 fig.
27. Matheron, G.(1963b). "Principles of Geostatistics." *Economic Geology*, **58**, 1246-1266.
28. Matheron, G.(1971). "The Theory of Regionalised Variables and its Applications" *Les Cahiers du CMM Fasc.*, No. 5, ENSMP, Paris, France, 211p.

29. McCuen, R.H. and Snyder, W.M. (1986). *Hydrologic Modeling: Statistical Methods and Applications*. Prentice-Hall, Englewood Cliffs, New Jersey, 508p.
30. Mercer, W.B., and Hall, A.D. (1911) "The Experimental Error of Field Trials" *Jour. Agr. Sci.*, 4, pt. 2, 107-132, 10 fig.
31. Mitchell, H.H., and Grindley, H.S. (1913). "The Element of Uncertainty in the Interpretation of Feeding experiments." *Ill. Agr. Exp. Sta. Bul.* 165, 459-579, 8 fig. Bibliography, 578-579.
32. Modjeska, J.S. and Rawlings, J.O. (1983). "Spatial Correlation Analysis of Uniformity Data". *Biometrics* 39, 373-384.
33. Montgomery, E.G. (1912). "Variation in Yield and Method of Arranging Plots to Secure Comparative Results." *Nebr. Agr. Exp. Sta. 25<sup>th</sup> Ann. Rpt.*, [1911]/12, 164-180, 4 fig.
34. Montgomery, E.G. (1913). "Experiments in Wheat Breeding: Experimental Error in the Nursery and Variation in Nitrogen and Yield." *U.S. Dept. Agr. Bur. Plant Indus. Bul.* 269, 61 p., 22 fig., 4 pl.
35. Olmstead, L.B. (1914). "Some Applications of the Method of Least Squares to Agricultural experiments." *Jour. Amer. Soc. Agron.*, 6, no.4/5, 190-204, 1 fig.
36. Pickering, S.U. (1911). "Experimental Error in Horticultural Work." *Jour. Bd. Agr.* [London], Sup. 7, 38-47.
37. Pritchard, F.J. (1916). "The Use of Checks and Repeated Plantings in Varietal Tests." *Jour. Amer. Soc. Agron.*, 8, no.2, 65-81, 3 fig.
38. Rendu, J.M. (1978). *An Introduction to Geostatistical Methods of Mineral Evaluation*: South African Institute of Mining & Metallurgy, Johannesburg, 84p.
39. Sasmal, B.C. and Katyal, V. (1980). "Note on the Size and Shape of Plots and Blocks in Field Experiments with Tossa Jute." *Indian Jour. Of Agri. Sci.* 50(10):791-793
40. Sethi, A.S. (1985). "A Modified Approach to Determine the Optimum Size and Shape of Plots in Field Experiments on Maize Grown on Terraced Land." *Indian Jour. Of Agril. Sci.* 55(1):48-51
41. Smith, H.F. (1938). "An Empirical Law Describing Heterogeneity in the Yields of Agricultural Crops." *Journal of Agricultural Sciences, Cambridge* 28:1-29.

43. Strond, A.H. and Secrest, D. (1966). *Gaussian Quadrature Formulas*: Prentice-Hall, Englewood cliffs, New Jersey, 374p.
44. Surface, F.M., and Pearl, Raymond (1916). "A Method of Correcting for Soil Heterogeneity in Variety Tests." *Jour. Agr. Research*, **5**, no.22, 1039-1050, 4 fig. Literature cited, p.1050.
45. Weber, C.R. and Horner, T.W. (1957). "Estimates of Cost and Optimum Plot Size and Shape for Measuring Yield and Chemical Characters in Soybeans." *Agron. J.* **49**, 444-449.
46. Webster, R. and Burgess, T.M. (1984). "Sampling and Bulking Strategies for Estimating Soil Properties in Small Regions." *J. Soil Sci.*, **35**, 127-140.
47. Wood, T.B. (1911). "The Interpretation of Experimental Results." *Jour. Bd. Agr. [London]*, Sup. **7**, 15-37, 2 fig.
48. Wood, T.B. and Stratton, F.J.M. (1910). "The Interpretation of Experimental Results." *Jour. Agr. Sci.*, **3**, pt. 4, 417-440, 10 fig.
49. Zhang, R, Warrick, A.W. and Myers, D.E. (1990). "Variance as a Function of Sample Support Size." *Math. Geol.*, **22**, no.1, 107-121.
50. Zhang, R, Warrick, A.W. and Myers, D.E. (1994). "Heterogeneity, Plot Shape Effect and Optimum Plot Size." *Geoderma*, **62**, no. , 183-197.

## **APPENDIX**

```

REM Program to find v(x), vx, c.v. and heterogeneity for all
REM plot sizes and shapes
DIM Y(36, 30), V(200), PD(200), VV(200), S(200)
CLS
INPUT "GIVE NAME OF DATA FILE : ", DF$
INPUT "GIVE NAME OF OUTPUT FILE : ", OF$
OPEN "I", #1, DF$
OPEN "O", #2, OF$
INPUT "GIVE NO. OF ROWS & COLUMNS", R, C
P = R * C: G = 0: SS = 0
FOR I = 1 TO R
FOR J = 1 TO C
INPUT #1, Y(I, J)

```

```

G = G + Y(I, J): SS = SS + Y(I, J) ^ 2
NEXT J
NEXT I
N = 1: CF = G ^ 2 / P: VV(N) = (SS - CF) / (P - 1)
M = G / P: S(N) = 1: W = 1: L = 1
V(N) = VV(N): PD(N) = P
VV1 = SQR(VV(N))
CV = (VV1 / M) * 100
PRINT #2, "PLOT          No.of PLOT      VARIANCE"
PRINT #2, "SIZE WIDTH LENGTH PLOTS MEAN VARIANCE /SQ.MT. C.V."
PRINT #2, S(N), W, L, PD(N), M, VV(N), V(N), CV
FOR L = 1 TO 9
  REM IF C / L <> C \ L GOTO 10
  FOR W = 1 TO 9
    IF (L = 1 AND W = 1) THEN GOTO 8
    REM IF R / W <> R \ W GOTO 8
    REM IF L * W > 36 THEN GOTO 8
    CN = 1: YM = 0: TT = 0: N = N + 1: SM = 0: GT = 0
    S(N) = L * W: PD(N) = (R \ W) * (C \ L): PJ = 1: PK = 1
    FOR I = 1 TO PD(N)
      T = 0
      FOR J = PJ TO PJ + W - 1
        FOR K = PK TO PK + L - 1
          PRINT "I J K : ", I, J, K
          T = T + Y(J, K)
        NEXT K
      NEXT J
      YM = YM + (T / S(N)) ^ 2: TT = TT + T ^ 2: PJ = PJ + W: SM = SM + T / S(N)
      GT = GT + T
      IF I = (R \ W) * CN THEN
        CN = CN + 1: PK = PK + L: PJ = 1: PRINT "PJ,PK,W : ", PJ, PK, W
      END IF
    NEXT I
    SM = SM / PD(N): VR = YM / PD(N) - SM ^ 2: CF = GT ^ 2 / (PD(N) * S(N))
    VV(N) = S(N) * (TT / S(N) - CF) / (PD(N) - 1): V(N) = VV(N) / (S(N) ^ 2)
    GT = GT / PD(N): CVT = (SQR(VV(N)) / GT) * 100
    5 PRINT #2, S(N), W, L, PD(N), GT, VV(N), V(N), CVT
    8 NEXT W
    10 NEXT L
  FOR I = 1 TO N
    FOR J = I + 1 TO N
      IF S(I) > S(J) THEN
        TEMP = S(I): TEM = VV(I): T = V(I)
        S(I) = S(J): VV(I) = VV(J): V(I) = V(J)
        S(J) = TEMP: VV(J) = TEM: V(J) = T
      END IF
    NEXT J
  NEXT I

```

```

NEXT J
NEXT I
FOR I = 1 TO N
PRINT S(I); VV(I); V(I)
NEXT I
INPUT BB
K = 0: CO = LOG(V(1)): NS = 0: DS = 0: S(0) = 0: VX = VV(1)
PRINT #2, "Plot size   Var/unit area"
FOR I = 1 TO N
IF S(I) = S(I - 1) GOTO 20
T = VV(I): CT = 1: LS = LOG(VV(I)): TOT = V(I): MIN = V(I): VX = V(I)
FOR J = I + 1 TO N
IF S(I) = S(J) THEN
CT = CT + 1: T = T + VV(J): TOT = TOT + V(J): LS = LS + LOG(VV(J))
IF V(J) < MIN THEN
MIN = V(J)
END IF
END IF
NEXT J
IF VV(I) > VV(I + 1) THEN
KAM = VV(I + 1): JADA = VV(I)
ELSE
KAM = VV(I): JADA = VV(I + 1)
END IF
IF CT = 2 THEN
F = JADA / KAM: PRINT "F"; PD(N); "d.f. calc."; F: INPUT A$
IF A$ = "Y" OR A$ = "y" THEN
PRINT #2, "For plot size"; S(I); "calculated F "; PD(N); ", "; PD(N); "d.f. is "; F
YV = LOG(MIN) - CO: VX = MIN
ELSE
VX = TOT / CT: YV = LOG(VX) - CO
END IF
END IF
IF CT > 2 THEN
X2 = 2.3026 * PD(N) * (CT * LOG(T / CT) - LS) / (1 + ((CT + 1) / (3 * CT * PD(N))))
DF = CT - 1
PRINT "X^2"; DF; "d.f. calc.="; X2: INPUT A$
IF A$ = "Y" OR A$ = "y" THEN
PRINT #2, "For plot size"; S(I); "calculated X2"; DF; "d.f. is "; X2
YV = LOG(MIN) - CO: VX = MIN
ELSE
VX = TOT / CT: YV = LOG(VX) - CO
END IF
END IF
PRINT #2, S(I), VX
SZ = LOG(S(I))

```

```

NS = NS + CT * SZ * YV: DS = DS + CT * SZ ^ 2
20 NEXT I
PRINT "NS = "; NS
B = -NS / DS
PRINT "Smith's index of soil heterogeneity= "; B
PRINT #2, "Smith's index of soil heterogeneity= "; B
CLOSE #1, #2
END

```

```

REM Program to find optimum plot size and shape by the method of maximum curvature.
DIM Y(36, 30), V(100), PD(100), VV(100), S(100), RW(100), CL(100), CV(100)
CLS
INPUT "GIVE NAME OF DATA FILE : ", DF$
INPUT "GIVE NAME OF OUTPUT FILE : ", OF$
OPEN "I", #1, DF$
OPEN "O", #2, OF$
INPUT "GIVE NO. OF DATA", N
FOR I = 1 TO N
INPUT #1, S(I), RW(I), CL(I), CV(I)
PRINT #2, S(I), RW(I), CL(I), CV(I)
NEXT I
SX = 0: SY = 0: SSX = 0: SXY = 0: ACV = 0: SX1 = 0: SX2 = 0: S1Y = 0: S2Y = 0
S12 = 0: SS1 = 0: SS2 = 0
FOR I = 1 TO N
LS = LOG(S(I)): LCV = LOG(CV(I)): LR = LOG(RW(I)): LC = LOG(CL(I))
SX = SX + LS: SY = SY + LCV: SX1 = SX1 + LR: SX2 = SX2 + LC: S1Y = S1Y + LR * LCV
S2Y = S2Y + LC * LCV: S12 = S12 + LR * LC: SSX = SSX + LS ^ 2: SXY = SXY + LS *
LCV
ACV = ACV + LCV: SS1 = SS1 + LR ^ 2: SS2 = SS2 + LC ^ 2
NEXT I
ACV = ACV / N: SX = SX / N: SY = SY / N: SX1 = SX1 / N: SX2 = SX2 / N
COV1Y = (S1Y / N - SX1 * SY): COV2Y = (S2Y / N - SX2 * SY): COV12 = S12 / N - SX1 *
SX2
V1 = SS1 / N - SX1 ^ 2: V2 = SS2 / N - SX2 ^ 2: B = -(SXY / N - SX * SY) / (SSX / N - SX ^ 2)
A = EXP(SY + B * SX): XO = ((A * B) ^ 2 * (1 + 2 * B) / (2 + B)) ^ (1 / (2 + 2 * B))
B2 = (COV1Y * COV12 - V1 * COV2Y) / (V1 * V2 - COV12 ^ 2)
B1 = -(COV1Y + B2 * COV12) / V1: A1 = EXP(SY + B1 * SX1 + B2 * SX2)
RSS = 0: RSS1 = 0: VCV = 0
FOR I = 1 TO N
RSS = RSS + (CV(I) - A / S(I) ^ B) ^ 2: RSS1 = RSS1 + (CV(I) - A1 / ((RW(I) ^ B1) * (CL(I) ^
B2))) ^ 2
VCV = VCV + (CV(I) - ACV) ^ 2
NEXT I
FIT = 1 - RSS / VCV: FIT1 = 1 - RSS1 / VCV
PRINT #2, "A,B,Xopt,FIT= ", A; B; XO; FIT
PRINT #2, "A,B1,B2,FIT= ", A1; B1; B2; FIT1

```

```

PRINT #2, "Fixed x1 conditional maxima x02 Fixed x2 Conditional maxima x01"
SR = 0: SX2 = 0: SSR = 0: SSX2 = 0: SRX2 = 0
FOR I = 1 TO N
X20 = ((B2 * A1 / (RW(I)) ^ (B1)) ^ 2 * (1 + 2 * B2) / (2 + B2)) ^ (1 / (2 + 2 * B2))
X10 = ((B1 * A1 / (CL(I)) ^ (B2)) ^ 2 * (1 + 2 * B1) / (2 + B1)) ^ (1 / (2 + 2 * B1))
LR = LOG(RW(I)): LX2 = LOG(X20): LX1 = LOG(X10)
SR = SR + LR: SX2 = SX2 + LX2: SSR = SSR + LR ^ 2: SSX2 = SSX2 + LX2 ^ 2: SRX2 =
SRX2 + LR * LX2
PRINT #2, RW(I); X20; CL(I); X10
NEXT I
SR = SR / N: SX2 = SX2 / N: B = -(SRX2 / N - SR * SX2) / (SSR / N - SR ^ 2)
A = EXP(SX2 + B * SR)
X10 = ((A * B) ^ 2 * (1 + 2 * B) / (2 + B)) ^ (1 / (2 + 2 * B)): X20 = XO / X10
PRINT #2, "A,B,X10,X20=", A; B; X10; X20
CLOSE #1, #2
END

```

```

REM Program to find within block C.V., R.E., B.E. for different plot sizes and shapes
REM and block size when blocks run row direction.
DIM Y(36, 22), TY(36, 22)
CLS
INPUT "GIVE NAME OF DATA FILE : ", DF$
INPUT "GIVE NAME OF OUTPUT FILES FOR CV, RE, BE : ", OF1$, OF2$, OF3$
OPEN "I", #1, DF$
OPEN "O", #2, OF1$
OPEN "O", #3, OF2$
OPEN "O", #4, OF3$
INPUT "GIVE NO. OF ROWS & COLUMNS", R, C
P = R * C: G = 0: SS = 0
FOR I = 1 TO R
FOR J = 1 TO C
INPUT #1, Y(I, J)
G = G + Y(I, J): SS = SS + Y(I, J) ^ 2
NEXT J
NEXT I
N = 1: CF = G ^ 2 / P: VV = (SS - CF) / (P - 1)
M = G / P: S = 1: W = 1: L = 1
V = VV: PD = P
VV1 = SQR(VV)
CV = (VV1 / M) * 100
PRINT #2, "TABLE: C.V. for different plots when blocks run row(E->W) direction"
PRINT #2, " "
PRINT #3, "TABLE: Relative Efficiencies for different plots when blocks run row(E->W)
direction"
PRINT #3, " "

```

```

PRINT #4, "TABLE: Blocking Efficiencies for different plots when blocks run row(E->W)
direction"
PRINT #4, " "
FOR LG = 3 TO 12
PRINT #2, " "
PRINT #3, " "
PRINT #4, " "
PRINT #2, LG; "plot blocks: "
PRINT #2, "row      no. of units along column(N->S) direction"
PRINT #2, "E->W 1      2      3      4      5      6      7      8
9"
PRINT #3, LG; "plot blocks: "
PRINT #3, "row      no. of units along column(N->S) direction"
PRINT #3, "E->W 1      2      3      4      5      6      7      8
9"
PRINT #4, LG; "plot blocks: "
PRINT #4, "row      no. of units along column(N->S) direction"
PRINT #4, "E->W 1      2      3      4      5      6      7      8
9"
FOR W = 1 TO 9
PRINT #2, W;
PRINT #3, W;
PRINT #4, W;
FOR L = 1 TO 9
IF (L = 1 AND W = 1) THEN
FOR I = 1 TO R
FOR J = 1 TO C
TY(I, J) = Y(I, J)
NEXT J
NEXT I
GOTO 5
END IF
CN = 1: MT = 0: TT = 0: N = N + 1: RN = 1
S = L * W: PD = (R \ W) * (C \ L): PJ = 1: PK = 1
FOR I = 1 TO PD
T = 0
FOR J = PJ TO PJ + W - 1
FOR K = PK TO PK + L - 1
PRINT "I J K : ", I; J; K
T = T + Y(J, K)
NEXT K
NEXT J
T = T / S: PJ = PJ + W: TY(RN, CN) = T
RN = RN + 1
IF I = (R \ W) * CN THEN
RN = 1: CN = CN + 1: PK = PK + L: PJ = 1: PRINT "PJ,PK,W : ", PJ; PK; W

```

```

END IF
NEXT I
5 REM **PRINT #2, S(N); W; L; PD(N); VV(N); V(N); CV
REM Block sum of squares(blocks run in row direction)
RT = R \ W: CT = C \ L
IF LG > RT THEN
GOTO 8
END IF
PJ = 1: NR = 0: BB = 0: T = 0: SS = 0
FOR K = 1 TO CT
7 IF (PJ + LG - 1) > RT THEN
PJ = 1
GOTO 20
END IF
B = 0
FOR J = PJ TO PJ + LG - 1
B = B + TY(J, K): SS = SS + TY(J, K) ^ 2
NEXT J
B = B / LG: BB = BB + B ^ 2: T = T + B: NR = NR + 1
PJ = PJ + LG
GOTO 7
20 NEXT K
IF NR = 1 THEN
GOTO 8
END IF
T = T / NR: VB = BB / NR - T ^ 2: V = SS / (NR * LG) - T ^ 2
VAR = V - VB
PRINT "L,W,T,NR,BB, VAR= ", L, W, T, NR, BB, VAR
CV = (SQR(VAR) / T) * 100
PRINT #2, " ";
PRINT #2, USING "#####.##"; CV;
IF L = 1 AND W = 1 THEN
V1 = VAR: R1 = NR
END IF
RE = (V1 / R1) / (VAR / NR)
PRINT #3, " ";
PRINT #3, USING "#####.##"; RE;
BE = V / VAR
PRINT #4, " ";
PRINT #4, USING "#####.##"; BE;
8 NEXT L
PRINT #2, " "
PRINT #3, " "
PRINT #4, " "
10 NEXT W
PRINT #2, " "

```

```

PRINT #2, " "
PRINT #3, " "
PRINT #3, " "
PRINT #4, " "
PRINT #4, " "
25 NEXT LG
CLOSE #1, #2, #3, #4
END

```

```

REM Program to find diagonal and off diagonal spatial correlation, M.S.E., S.T.M.S.E.
REM and Cost per unit of information matrix for uniformity data.
DIM Y(36, 18), K1(20, 20), K2(20, 20), KM(20, 20), COVP(18, 9), COVN(18, 9), COV(18, 9)
DIM ROP(18, 9), RON(18, 9), MC(18, 9), MSE(18, 9), STMSE(18, 9)
CLS
INPUT "GIVE NAME OF DATA FILE : ", DF$
INPUT "GIVE NAME OF OUTPUT FILE : ", OF$
OPEN "I", #1, DF$
OPEN "O", #2, OF$
INPUT "GIVE NO. OF ROWS & COLUMNS:- ", R, C
FOR I = 1 TO R
FOR J = 1 TO C
INPUT #1, Y(I, J)
NEXT J
NEXT I
M = R / 2 - 1: N = C / 2 - 1
REM Module to compute KM
FOR I = 0 TO M
FOR J = 0 TO M
K1(I, J) = 0: K2(I, J) = I + 1
NEXT J
NEXT I
FOR I = 0 TO M
K1(I, 0) = I + 1
NEXT I
FOR I = 1 TO M
FOR J = 1 TO I
K1(I, J) = 2 * (I - J + 1)
NEXT J
NEXT I
FOR I = 0 TO M
FOR J = 0 TO M
KM(I, J) = K1(I, J) / K2(I, J)
NEXT J
NEXT I
FOR I = 0 TO M
FOR J = 0 TO M

```

```

PRINT USING "###.###"; KM(I, J);
NEXT J
PRINT " "
INPUT A$
NEXT I
REM Module for computing Cov+, Cov-, R+, R-
FOR L = 0 TO M
FOR K = 0 TO N
SPP = 0: SPN = 0: SP1 = 0: SN1 = 0: SP2 = 0: SN2 = 0: SSP1 = 0
SSP2 = 0: SSN1 = 0: SSN2 = 0
FOR I = 1 TO (R - L)
FOR J = 1 TO (C - K)
SPP = SPP + Y(I, J) * Y(I + L, J + K): SPN = SPN + Y(I, J + K) * Y(I + L, J)
SP1 = SP1 + Y(I, J): SN1 = SN1 + Y(I, J + K)
SP2 = SP2 + Y(I + L, J + K): SN2 = SN2 + Y(I + L, J)
SSP1 = SSP1 + Y(I, J) ^ 2: SSN1 = SSN1 + Y(I, J + K) ^ 2
SSP2 = SSP2 + Y(I + L, J + K) ^ 2: SSN2 = SSN2 + Y(I + L, J) ^ 2
NEXT J
NEXT I
COVP(L, K) = (SPP - SP1 * SP2 / ((R - L) * (C - K))) / ((R - L) * (C - K) - 1)
COVN(L, K) = (SPN - SN1 * SN2 / ((R - L) * (C - K))) / ((R - L) * (C - K) - 1)
COV(L, K) = (COVP(L, K) + COVN(L, K)) / 2
VP1 = (SSP1 - SP1 ^ 2 / ((R - L) * (C - K))) / ((R - L) * (C - K) - 1)
VP2 = (SSP2 - SP2 ^ 2 / ((R - L) * (C - K))) / ((R - L) * (C - K) - 1)
VN1 = (SSN1 - SN1 ^ 2 / ((R - L) * (C - K))) / ((R - L) * (C - K) - 1)
VN2 = (SSN2 - SN2 ^ 2 / ((R - L) * (C - K))) / ((R - L) * (C - K) - 1)
VP = (VP1 * VP2) ^ .5: VN = (VN1 * VN2) ^ .5
ROP(L, K) = COVP(L, K) / VP: RON(L, K) = COVN(L, K) / VN
PRINT "*****"
PRINT "OOOO"
NEXT K
NEXT L
PRINT #2, "Spatial correlation left=>R-(l,k) right=>R+(l,k)"
PRINT #2, "-----"
PRINT #2, "          K          "
PRINT #2, " 1  -----"
PRINT #2, " ";
FOR K = -(C / 2) + 1 TO C / 2 - 1
PRINT #2, K;
NEXT K
PRINT #2, " "
PRINT #2, "-----"
FOR L = 0 TO (R / 2 - 1)
PRINT #2, L;
FOR K = (C / 2 - 1) TO 0 STEP -1
PRINT #2, USING "#####.###"; RON(L, K);

```

```

NEXT K
FOR K = 1 TO (C / 2 - 1)
PRINT #2, USING "#####.###"; ROP(L, K);
NEXT K
PRINT #2, " "
NEXT L
PRINT #2, "Average Spatial correlation R(1,k)"
PRINT #2, "-----"
PRINT #2, "          K          "
PRINT #2, " 1  -----"
PRINT #2, " ";
FOR K = 0 TO C / 2 - 1
PRINT #2, K;
NEXT K
PRINT #2, " "
PRINT #2, "-----"
FOR L = 0 TO (R / 2 - 1)
PRINT #2, L;
PRINT #2, USING "#####.###"; RON(L, 0);
FOR K = 1 TO (C / 2 - 1)
ROA = (RON(L, K) + ROP(L, K)) / 2
PRINT #2, USING "#####.###"; ROA;
NEXT K
PRINT #2, " "
NEXT L
REM Module to find product KM*COV
FOR L = 0 TO (R / 2 - 1)
FOR K = 0 TO (C / 2 - 1)
S = 0
FOR I = 0 TO (R / 2 - 1)
S = S + KM(L, I) * COV(I, K)
NEXT I
MC(L, K) = S
NEXT K
NEXT L
REM Module to compute KN
FOR I = 0 TO N
FOR J = 0 TO N
K1(I, J) = 0; K2(I, J) = I + 1
NEXT J
NEXT I
FOR I = 0 TO N
K1(I, 0) = I + 1
NEXT I
FOR I = 1 TO N
FOR J = 1 TO I

```

```

K1(I, J) = 2 * (I - J + 1)
NEXT J
NEXT I
FOR I = 0 TO N
FOR J = 0 TO N
KM(I, J) = K1(I, J) / K2(I, J)
NEXT J
NEXT I
FOR I = 0 TO N
FOR J = I TO N
T = KM(I, J): KM(I, J) = KM(J, I): KM(J, I) = T
PRINT USING "##.##"; KM(I, J);
NEXT J
PRINT " "
INPUT A$
NEXT I
REM Module to compute MSE & STMSE
FOR L = 0 TO (R / 2 - 1)
FOR K = 0 TO (C / 2 - 1)
S = 0
FOR I = 0 TO (C / 2 - 1)
S = S + MC(L, I) * KM(I, K)
NEXT I
MSE(L, K) = S: STMSE(L, K) = S / MSE(0, 0)
NEXT K
NEXT L
PRINT #2, "    MSE for plots a x c units"
PRINT #2, "-----"
PRINT #2, "    Number of unit plots, c    "
PRINT #2, " a  -----"
PRINT #2, "    ";
FOR K = 1 TO C / 2
PRINT #2, K;
NEXT K
PRINT #2, " "
PRINT #2, "-----"
FOR L = 0 TO R / 2 - 1
PRINT #2, L + 1;
FOR K = 0 TO (C / 2 - 1)
PRINT #2, USING "#####.##"; MSE(L, K);
NEXT K
PRINT #2, " "
NEXT L
PRINT #2, "Standardised MSE for plots a x c units"
PRINT #2, "-----"
PRINT #2, "    Number of unit plots, c    "

```

```

PRINT #2, " a -----"
PRINT #2, " ";
FOR K = 1 TO C / 2
PRINT #2, K;
NEXT K
PRINT #2, " "
PRINT #2, "-----"
FOR L = 0 TO R / 2 - 1
PRINT #2, L + 1;
FOR K = 0 TO (C / 2 - 1)
PRINT #2, USING "##.###"; STMSE(L, K);
NEXT K
PRINT #2, " "
NEXT L
INPUT "GIVE COSTS K1, K2: ", C1, C2
PRINT #2, "Cost per unit of information for plots a x c units"
PRINT #2, "-----"
PRINT #2, "   Number of unit plots, c   "
PRINT #2, " a -----"
PRINT #2, " ";
FOR K = 1 TO C / 2
PRINT #2, K;
NEXT K
PRINT #2, " "
PRINT #2, "-----"
FOR L = 0 TO R / 2 - 1
PRINT #2, L + 1;
FOR K = 0 TO (C / 2 - 1)
COSTPI = (C1 + C2 * (L + 1) * (K + 1)) * MSE(L, K) / ((L + 1) * (K + 1))
PRINT #2, USING "#####.###"; COSTPI;
NEXT K
PRINT #2, " "
NEXT L
END

```